

ECEN689: Special Topics in High-Speed Links Circuits and Systems Spring 2010

Lecture 18: RX FIR & CTLE Equalization



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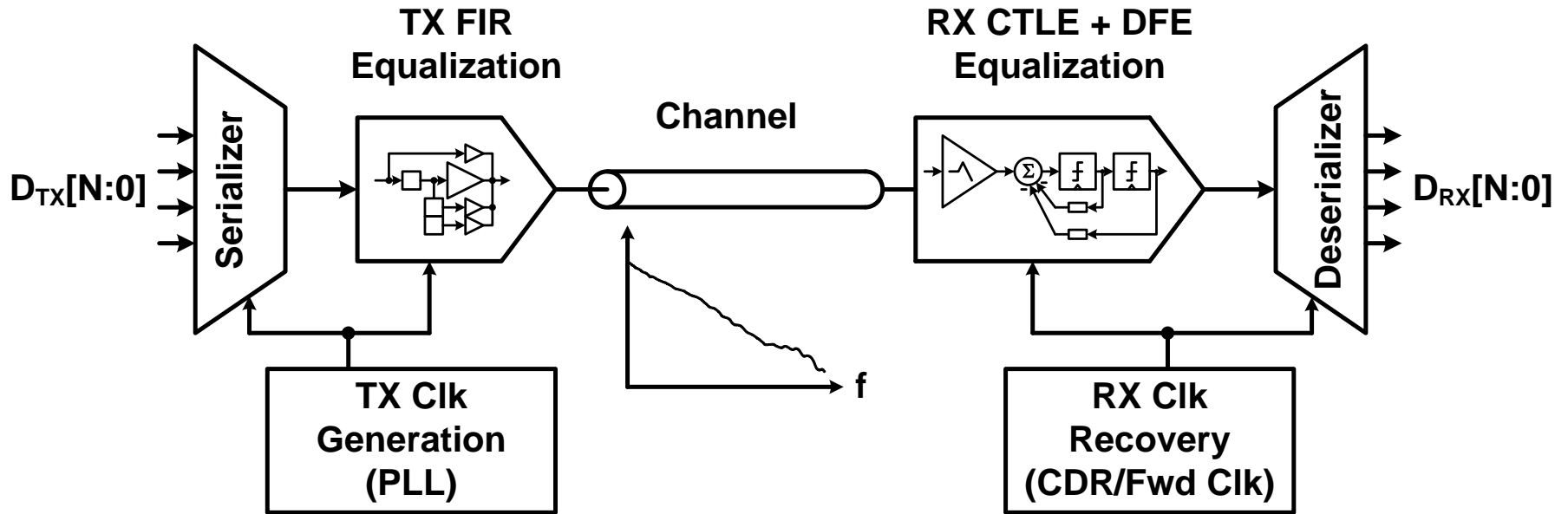
Announcements

- HW5 now due Friday (in class)
 - Any issues?
- Reading
 - Hanumolu equalization overview paper

Agenda

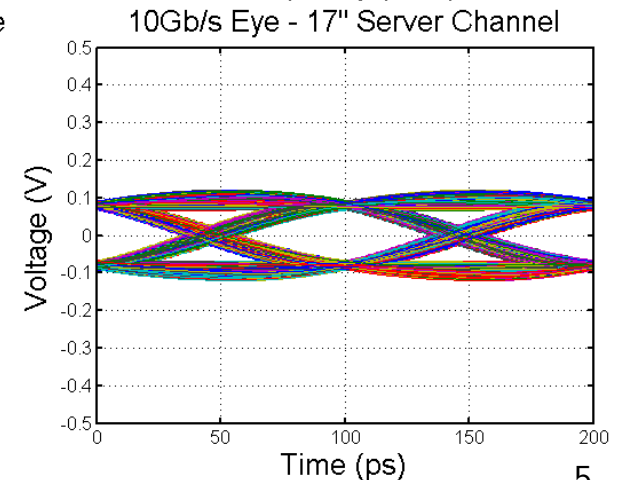
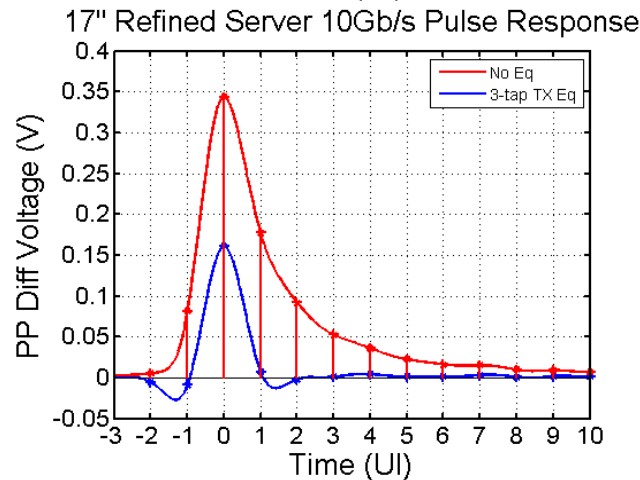
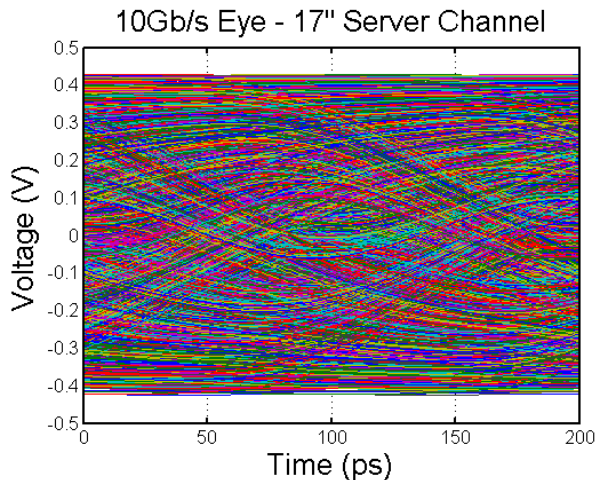
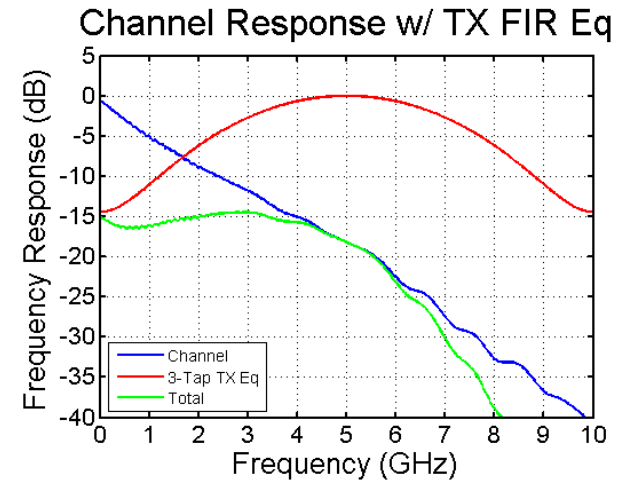
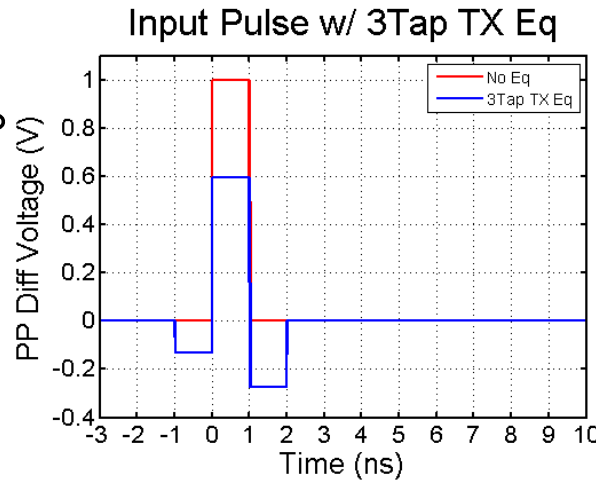
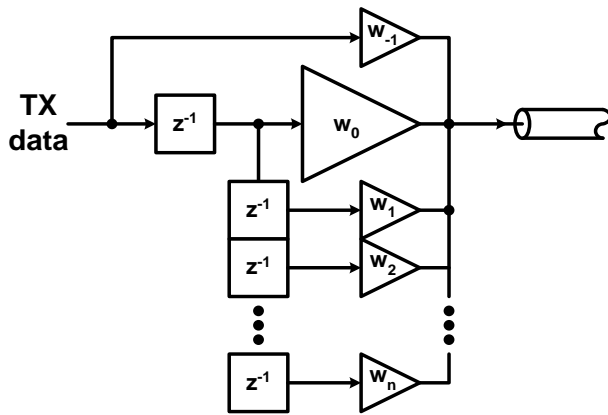
- RX FIR Equalization
- RX CTLE Equalization

Link with Equalization



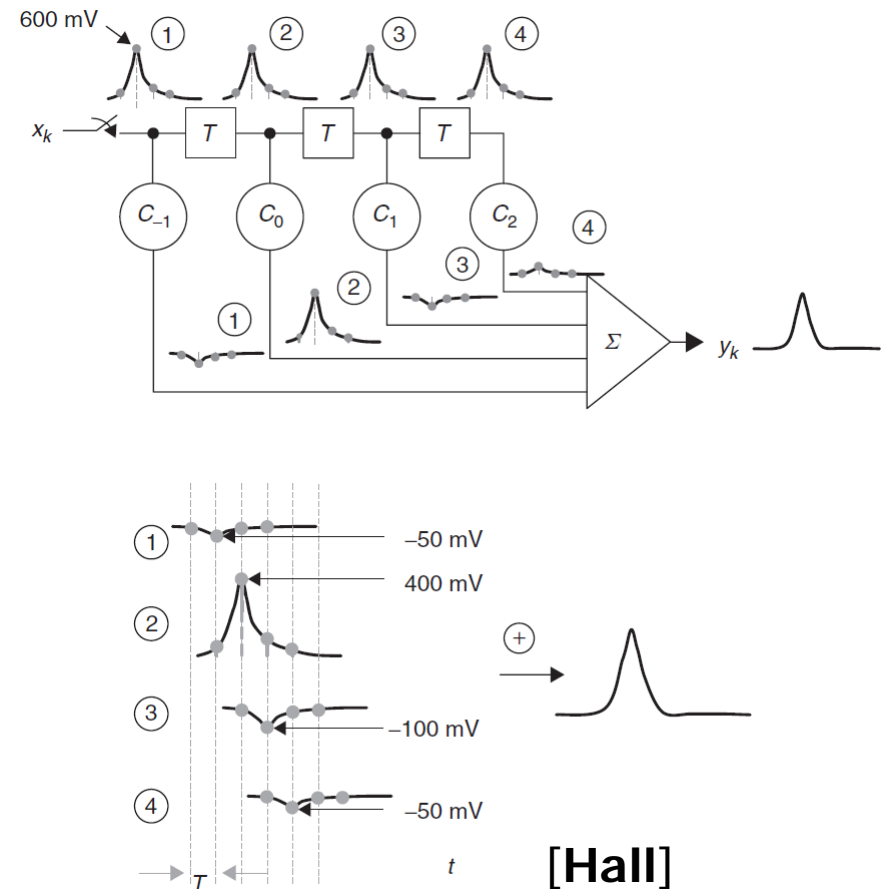
TX FIR Equalization

- TX FIR filter pre-distorts transmitted pulse in order to invert channel distortion at the cost of attenuated transmit signal (de-emphasis)



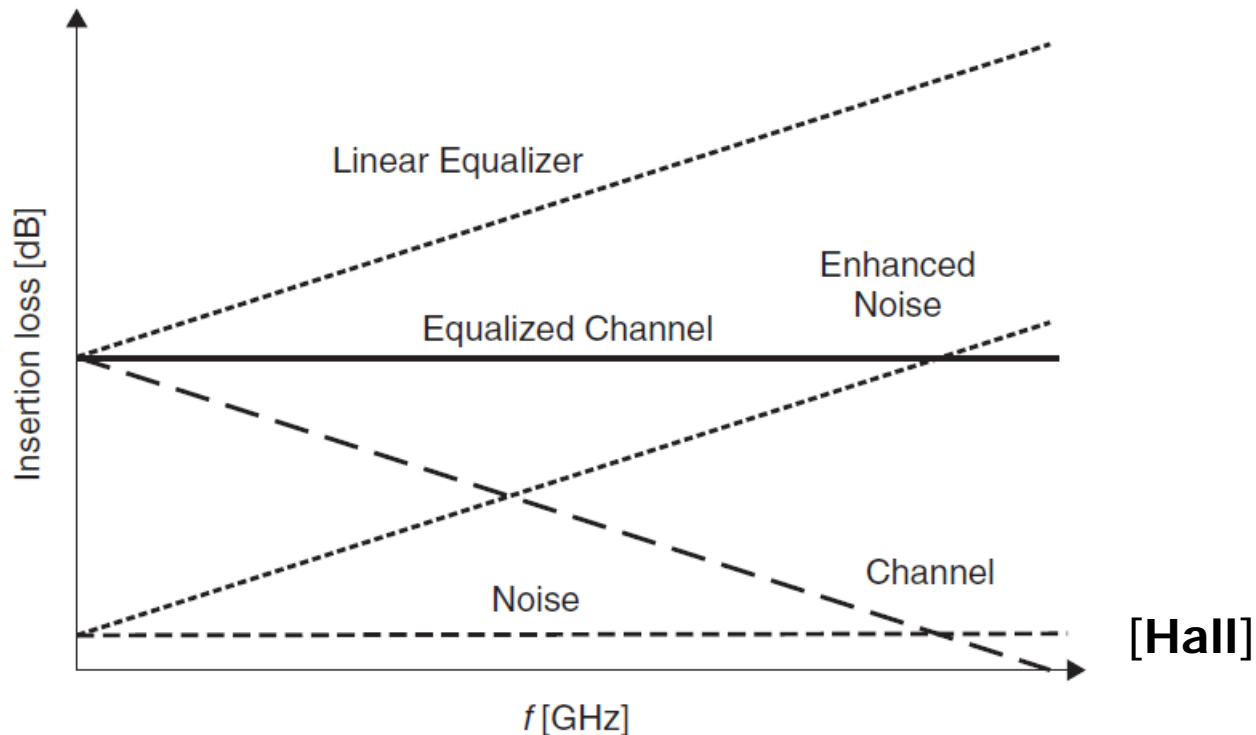
RX FIR Equalization

- Delay analog input signal and multiply by equalization coefficients
- Pros
 - With sufficient dynamic range, can amplify high frequency content (rather than attenuate low frequencies)
 - Can cancel ISI in pre-cursor and beyond filter span
 - Filter tap coefficients can be adaptively tuned without any back-channel
- Cons
 - Amplifies noise/crosstalk
 - Implementation of analog delays
 - Tap precision



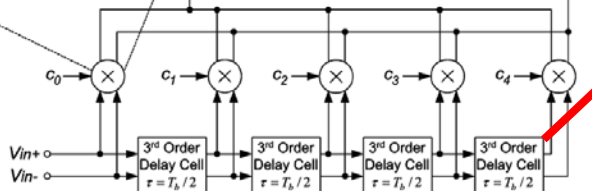
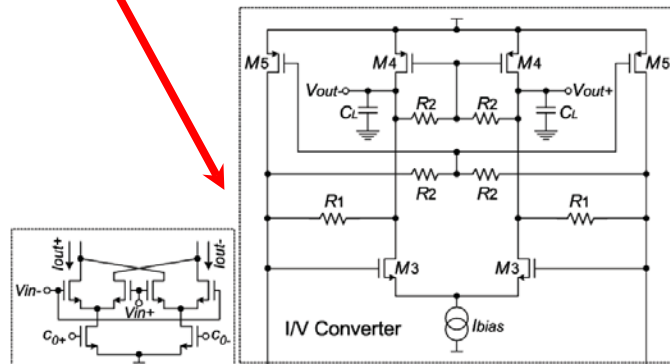
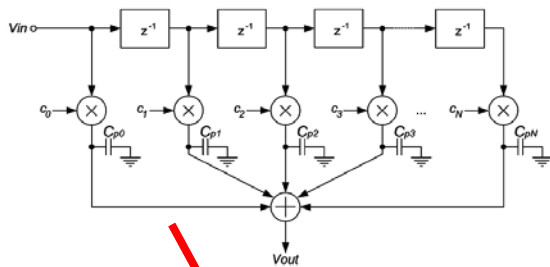
RX Equalization Noise Enhancement

- Linear RX equalizers don't discriminate between signal, noise, and cross-talk
 - While signal-to-distortion (ISI) ratio is improved, SNR remains unchanged

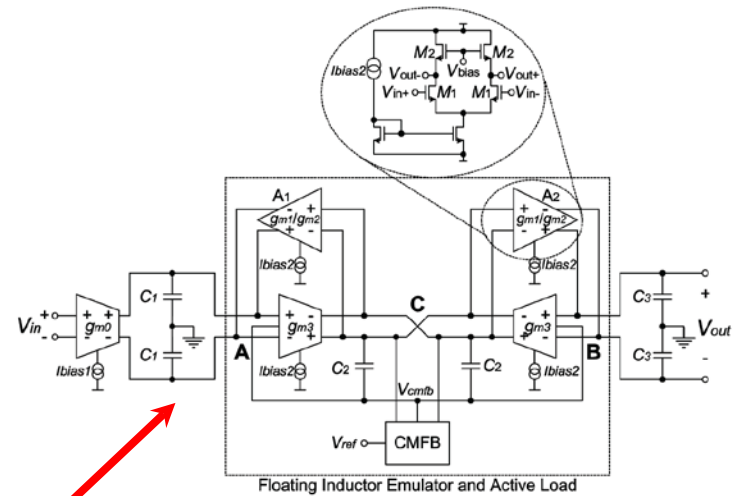


Analog RX FIR Equalization Example

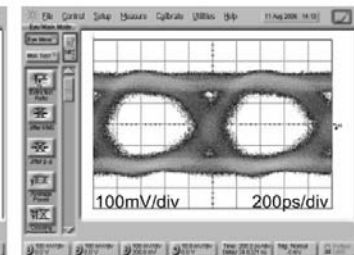
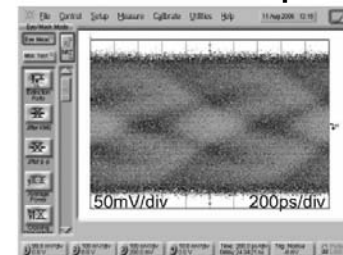
- 5-tap equalizer with tap spacing of $T_b/2$



3rd-order delay cell



1Gb/s experimental results

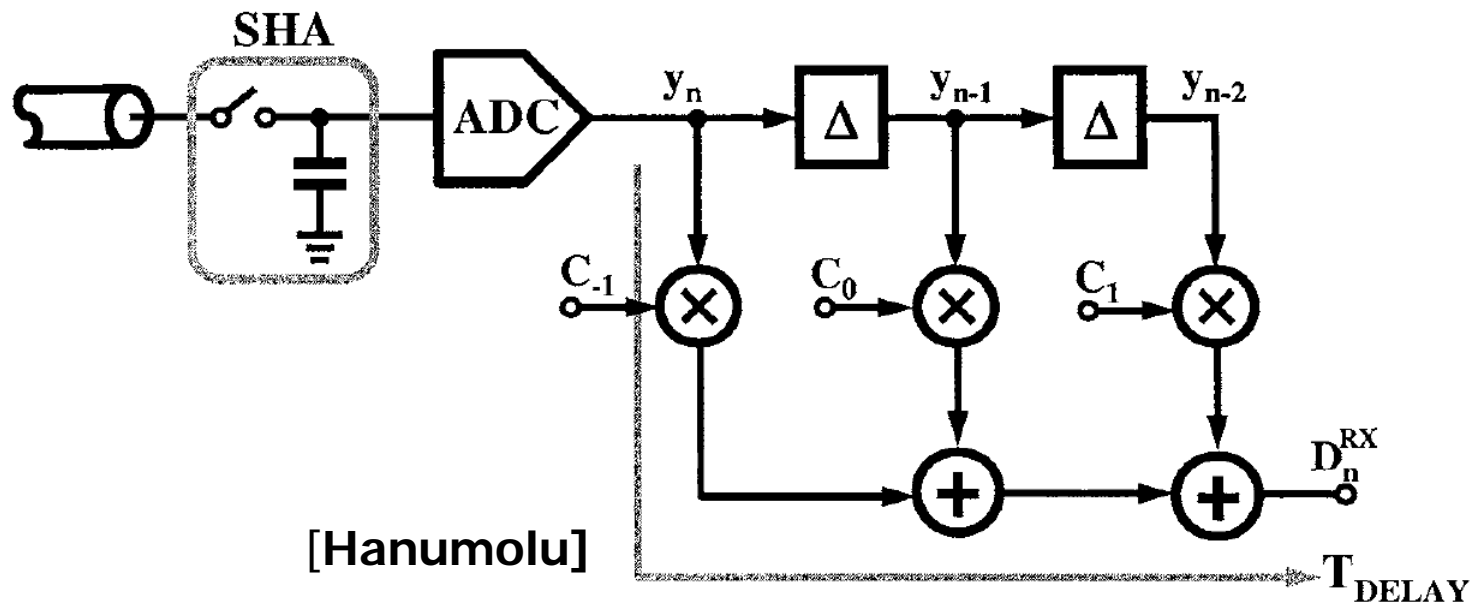


Before Equalizer: 23meters

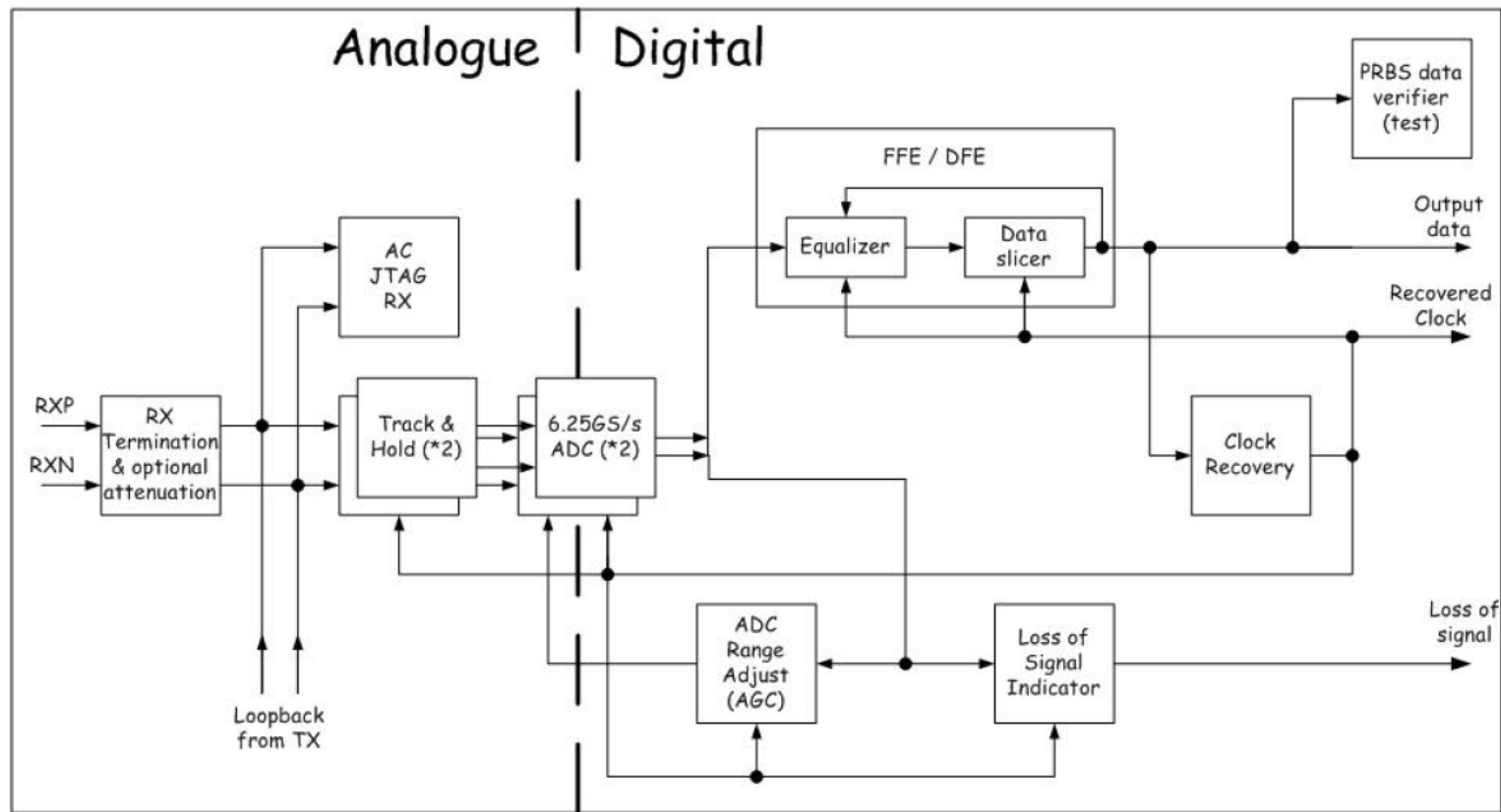
After Equalizer: 23meters

Digital RX FIR Equalization

- Digitize the input signal with high-speed low/medium resolution ADC and perform equalization in digital domain
 - Digital delays, multipliers, adders
 - Limited to ADC resolution
- Power can be high due to very fast ADC



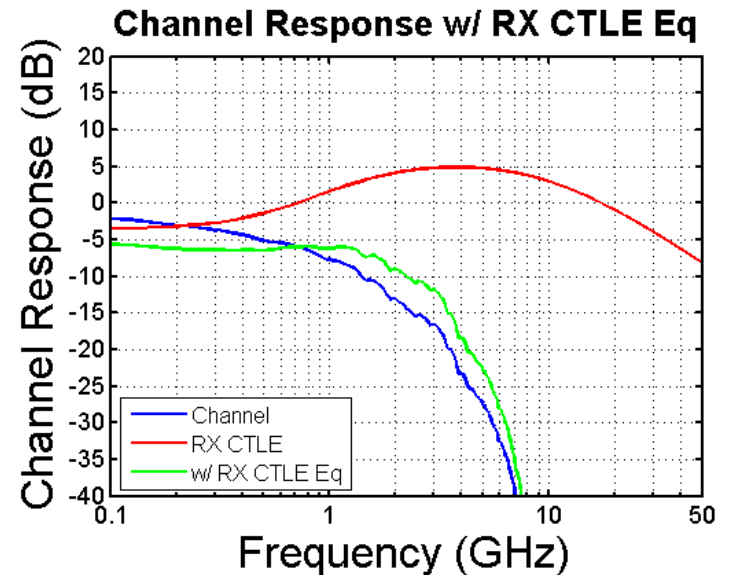
Digital RX FIR Equalization Example



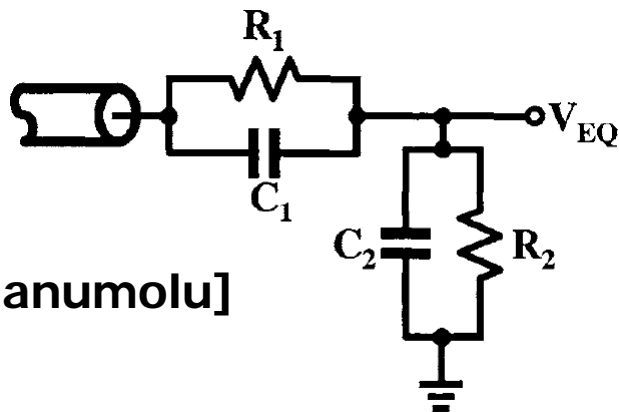
- 12.5GS/s 4.5-bit Flash ADC in 65nm CMOS [Harwood ISSCC 2007]
- 2-tap FFE & 5-tap DFE
- XCVR power (inc. TX) = 330mW, Analog = 245mW, Digital = 85mW

RX Continuous-Time Linear Equalizer (CTLE)

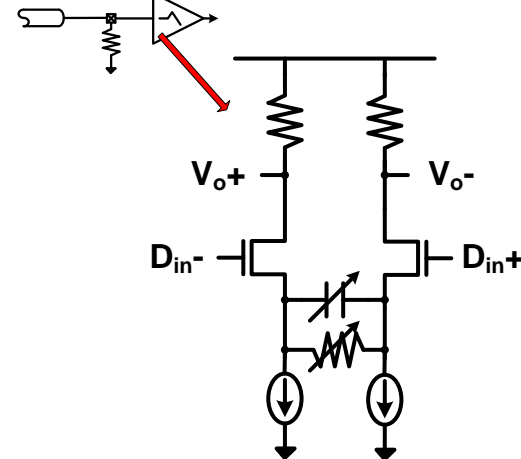
- Passive R-C (or L) can implement high-pass transfer function to compensate for channel loss
- Cancel both precursor and long-tail ISI
- Can be purely passive or combined with an amplifier to provide gain



Passive CTLE

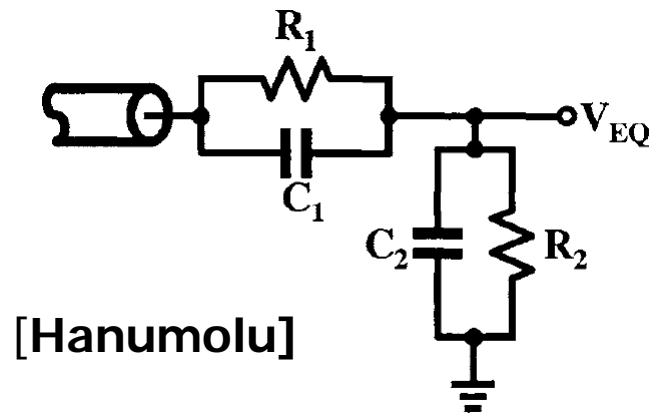


Active CTLE



Passive CTLE

- Passive structures offer excellent linearity, but no gain at Nyquist frequency



$$H(s) = \frac{R_2}{R_1 + R_2} \frac{1 + R_1 C_1 s}{1 + \frac{R_1 R_2}{R_1 + R_2} (C_1 + C_2) s}$$

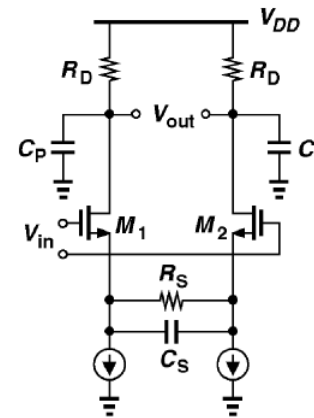
$$\omega_z = \frac{1}{R_1 C_1}, \quad \omega_p = \frac{1}{\frac{R_1 R_2}{R_1 + R_2} (C_1 + C_2)}$$

$$\text{DC gain} = \frac{R_2}{R_1 + R_2}, \quad \text{HF gain} = \frac{C_1}{C_1 + C_2}$$

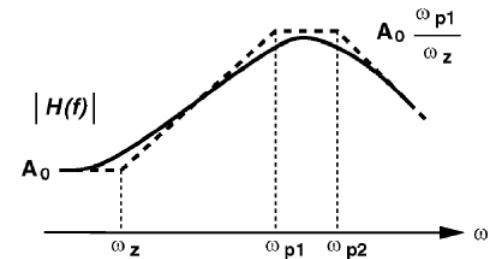
$$\text{Peaking} = \frac{\text{HF gain}}{\text{DC gain}} = \frac{\omega_p}{\omega_z} = \frac{R_1 + R_2}{R_2} \frac{C_1}{C_1 + C_2}$$

Active CTLE

- Input amplifier with RC degeneration can provide frequency peaking with gain at Nyquist frequency
- Potentially limited by gain-bandwidth of amplifier
- Amplifier must be designed for input linear range
 - Often TX eq. provides some low frequency attenuation
- Sensitive to PVT variations and can be hard to tune
- Generally limited to 1st-order compensation



[Gondi JSSC 2007]



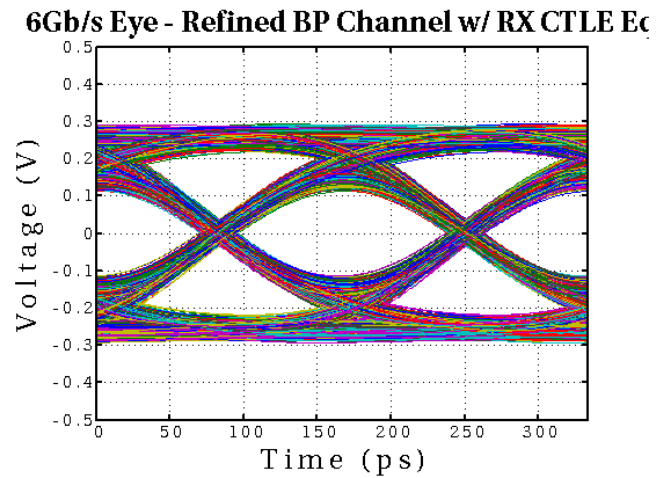
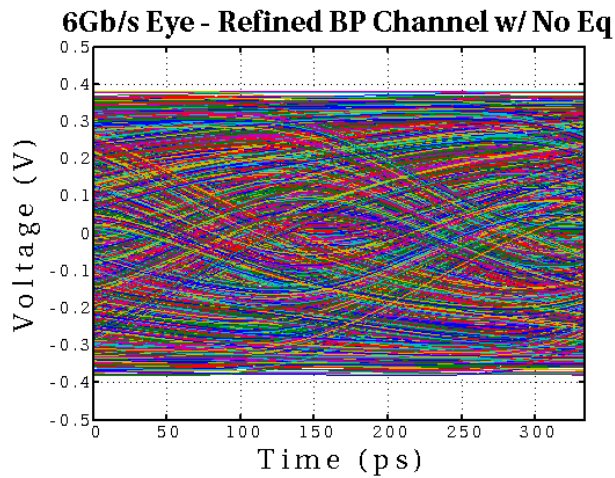
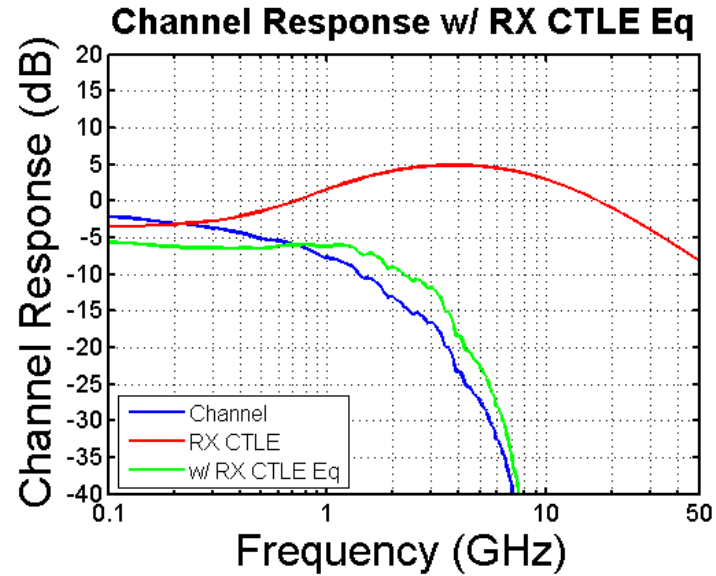
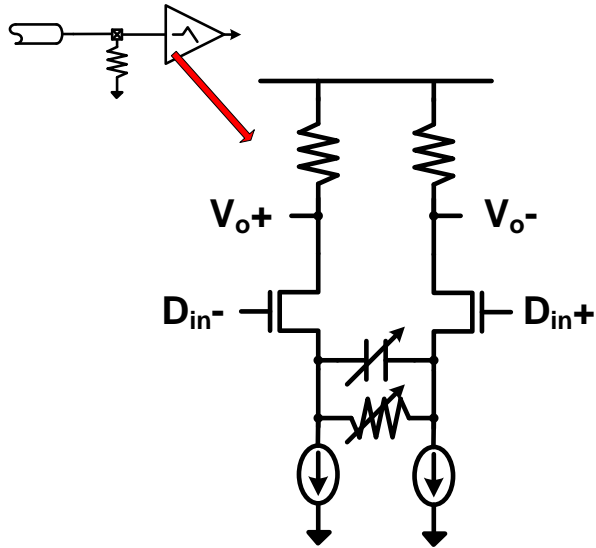
$$H(s) = \frac{g_m}{C_p} \frac{s + \frac{1}{R_S C_S}}{\left(s + \frac{1 + g_m R_S / 2}{R_S C_S} \right) \left(s + \frac{1}{R_D C_p} \right)}$$

$$\omega_z = \frac{1}{R_S C_S}, \quad \omega_{p1} = \frac{1 + g_m R_S / 2}{R_S C_S}, \quad \omega_{p2} = \frac{1}{R_D C_p}$$

$$\text{DC gain} = \frac{g_m R_D}{1 + g_m R_S / 2}, \quad \text{Ideal peak gain} = g_m R_D$$

$$\text{Ideal Peaking} = \frac{\text{Ideal peak gain}}{\text{DC gain}} = \frac{\omega_{p1}}{\omega_z} = 1 + g_m R_S / 2$$

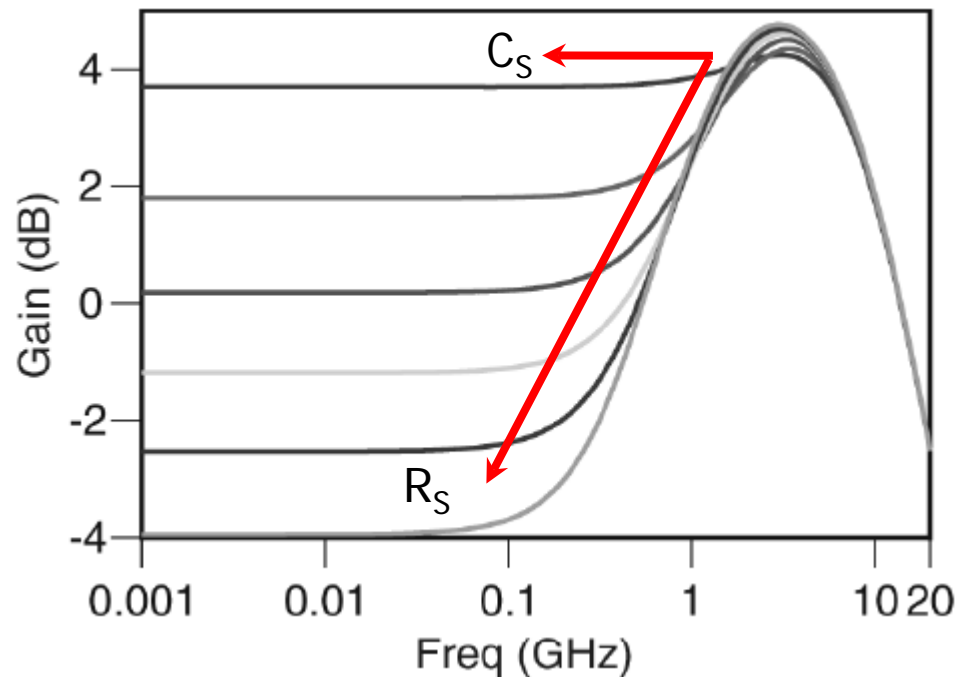
Active CTLE Example



Active CTLE Tuning

- Tune degeneration resistor and capacitor to adjust zero frequency and 1st pole which sets peaking and DC gain

$$\omega_z = \frac{1}{R_S C_S}, \quad \omega_{p1} = \frac{1 + g_m R_S / 2}{R_S C_S}$$



Next Time

- RX DFE
- Alternate/Future Approaches