

**Texas A&M University**  
**Department of Electrical and Computer Engineering**

**ECEN 720 – High-Speed Links**

**Spring 2025**

**Exam #2**

**Instructor: Sam Palermo**

- Please write your name in the space provided below
- Please verify that there are 7 pages in your exam
- Good Luck!

Problem	Score	Max Score
1		35
2		35
3		30
<b>Total</b>		<b>100</b>

Name: SAM PALERMO

UIN: \_\_\_\_\_

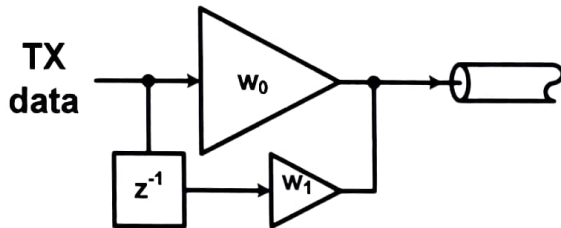
**TABLE 13-1.  $Q_{\text{BER}}$  as a Function of the Bit Error Rate**

BER	$Q_{\text{BER}}$	BER	$Q_{\text{BER}}$	BER	$Q_{\text{BER}}$
$1 \times 10^{-3}$	6.180	$1 \times 10^{-10}$	12.723	$1 \times 10^{-17}$	16.987
$1 \times 10^{-4}$	7.438	$1 \times 10^{-11}$	13.412	$1 \times 10^{-18}$	17.514
$1 \times 10^{-5}$	8.530	$1 \times 10^{-12}$	14.069	$1 \times 10^{-19}$	18.026
$1 \times 10^{-6}$	9.507	$1 \times 10^{-13}$	14.698	$1 \times 10^{-20}$	18.524
$1 \times 10^{-7}$	10.399	$1 \times 10^{-14}$	15.301	$1 \times 10^{-21}$	19.010
$1 \times 10^{-8}$	11.224	$1 \times 10^{-15}$	15.882	$1 \times 10^{-22}$	19.484
$1 \times 10^{-9}$	11.996	$1 \times 10^{-16}$	16.444	$7.7 \times 10^{-24}$	20.000

## Problem 1 (35 points)

## TX FIR Equalization

- a) Give the equalizer coefficients to realize 12dB of frequency peaking at the Nyquist frequency (relative to the DC response) for 50Gb/s PAM4 modulation. Assume that  $|W_0| + |W_1| = 1$ .
- b) Sketch the equalizer magnitude response out to the Nyquist frequency. Label the magnitude value in dB at low frequencies and at the Nyquist frequency.



Response at Nyquist Frequency  
is  $W_0 - W_1$

Response at DC is  $W_0 + W_1$

$$W_0 = \frac{5}{8}$$

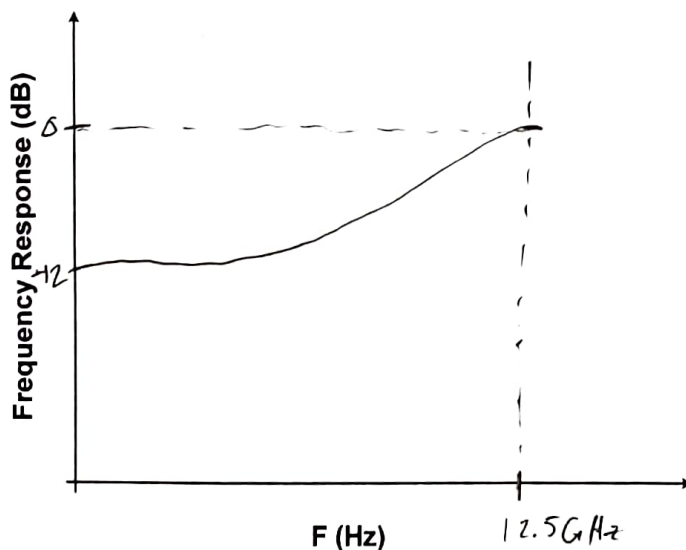
$$W_1 = -\frac{3}{8}$$

For 12dB peaking relative to DC:  $\frac{W_0 - W_1}{W_0 + W_1} = 4$

Peak Power constraint:  $|W_0| + |W_1| = 1$ , this should occur @  
Nyquist frequency data.

$$W_0 - W_1 = 1 \quad W_0 + W_1 = \frac{1}{4}$$

$$\Rightarrow W_0 = \frac{5}{8}, W_1 = -\frac{3}{8}$$

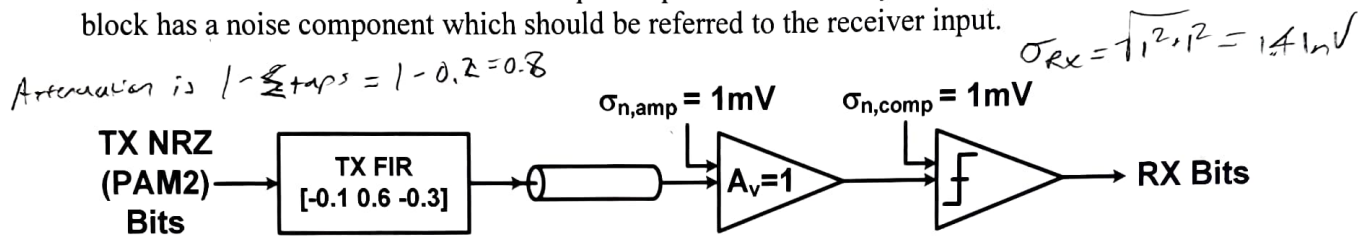


## Problem 2 (35 points)

This problem compares the voltage noise budgeting of a serial link system with PAM2 and PAM4 modulation. Here we will conservatively assume that all distributions combine in a worst-case manner.

**PAM2 System**

The system consists of a transmitter with a 3-tap FIR filter which sends NRZ (PAM2) bits over a channel to a receiver modeled as a simple amplifier followed by a comparator. Each receiver block has a noise component which should be referred to the receiver input.



Complete the following noise budget table assuming a TX peak differential swing of  $1V_{ppd}$  and a target  $BER=10^{-12}$ . You can refer to the  $Q_{BER}$  table on page 2 if needed. (10 points)

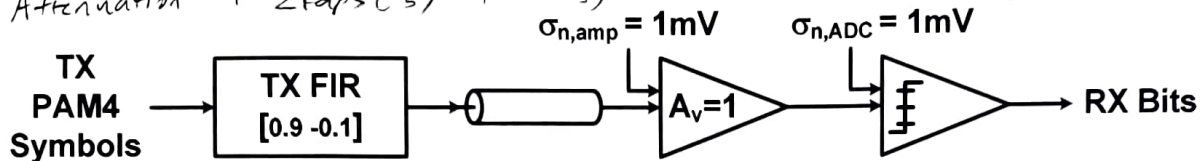
Parameter	$K_n$	RMS	Value ( $BER=10^{-12}$ )
Peak Differential Swing, $V_{swing}$			1V
RX Offset + Sensitivity			5mV
Power Supply Noise			5mV
Residual ISI	0.05		= 50mV
Crosstalk	0.05		= 50mV
Random Noise		= 1.41mV	= 19.9mV
Attenuation (TX FIR)	= 0.8		= 800mV
Total Noise			= 929.9mV
Differential Eye Height Margin			= 70.1mV

**PAM4 System**

The system consists of a transmitter with a 2-tap FIR filter which sends PAM4 symbols over a channel to a receiver modeled as a simple amplifier followed by a 2-bit ADC. Each receiver block has a noise component which should be referred to the receiver input.

$$\text{Attenuation} = 1 - \sum \text{taps} \left(\frac{1}{3}\right) = 1 - 0.8\left(\frac{1}{3}\right) = 0.733$$

$$\sigma_{Kx} = \sqrt{1^2 + 1^2} = 1.41 \text{ mV}$$



Complete the following noise budget table assuming a TX peak differential swing of  $1V_{ppd}$  and a target  $BER=10^{-12}$ . You can refer to the  $Q_{BER}$  table on page 2 if needed. (10 points)

Parameter	$K_n$	RMS	Value ( $BER=10^{-12}$ )
Peak Differential Swing, $V_{swing}$			1V
RX Offset + Sensitivity			5mV
Power Supply Noise			5mV
Residual ISI (compute from max. transition)	0.05		= 50mV
Crosstalk (compute from max. transition)	0.05		= 50mV
Random Noise		= 1.41mV	= 19.9mV
Attenuation (TX FIR and modulation)	= 0.733		= 733mV
Total Noise			= 862.9mV
Differential Eye Height Margin			= 137.1mV

What is the minimum peak differential swing,  $V_{swing}$ , for a  $BER=10^{-12}$ , i.e. as the differential eye height margin goes to zero for both the PAM2 and PAM4 systems? (10 points)

$$V_{swing} (1 - \sum K_n) \geq \text{Fixed Noise}$$

$$V_{swing} \geq \frac{\text{Fixed Noise}}{1 - \sum K_n}$$

$$\text{PAM2: } V_{swing} \geq \frac{29.9 \text{ mV}}{1 - 0.9} = 299 \text{ mV}$$

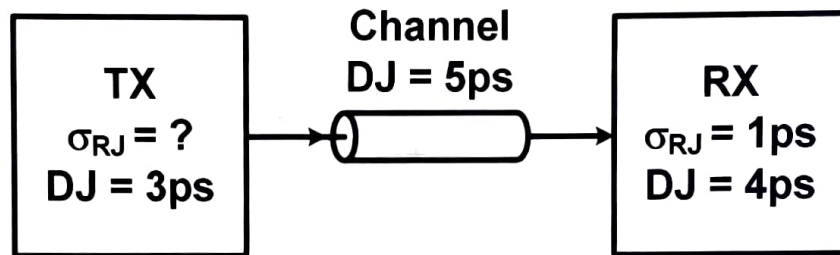
$$\text{PAM4: } V_{swing} \geq \frac{29.9 \text{ mV}}{1 - 0.833} = 179 \text{ mV}$$

$$\text{Min. } V_{swing} (\text{PAM2}) = 299 \text{ mV}$$

$$\text{Min. } V_{swing} (\text{PAM4}) = 179 \text{ mV}$$

## Problem 3 (30 points)

This problem involves designing a TX PLL loop bandwidth to satisfy a system jitter budget, given the following jitter components from the TX, channel, and RX. What is the maximum TX random rms jitter,  $\sigma_{RJ,TX}$ , for a  $BER=10^{-12}$  at a 25Gb/s data rate? Assume that the only source of random noise in the TX PLL below is from the VCO, which has  $\kappa = 10^{-8} \sqrt{s}$ , and that the jitter  $\sigma$  of interest is closed-loop and referenced to an ideal clock. What is the necessary TX PLL loop bandwidth to satisfy the system jitter budget?



$$\Delta J_{tot} + Q\sigma_{j,tot} = \frac{1}{DR}$$

$$\sigma_{j,tot} = \frac{\frac{1}{DR} - \Delta J_{tot}}{Q} = \frac{40ps - 12ps}{14.069} = 1.99ps$$

$$\sigma_{j,tot} = \sqrt{\sigma_{TX}^2 + \sigma_{RX}^2} \Rightarrow \sigma_{TX} = \sqrt{\sigma_{j,tot}^2 - \sigma_{RX}^2} = \sqrt{1.99ps^2 - 1ps^2} = 1.72ps$$

$$\sigma_x = K \sqrt{\frac{1}{2\pi f_{PLL}}}$$

$$f_{PLL} = \frac{K^2}{2\pi\sigma^2} = \frac{(10^{-8}\sqrt{s})^2}{2\pi(1.72ps)^2} = 5.38MHz$$

$$\text{Max } \sigma_{RJ,TX} \text{ (w/ } DR=25Gb/s) = 1.72ps$$

$$\text{PLL Loop Bandwidth (Hz)} = 5.38MHz$$