

**Texas A&M University**  
**Department of Electrical and Computer Engineering**

**ECEN 620 – Network Theory (Broadband Circuit Design)**

**Fall 2023**

**Exam #2**

**Instructor: Sam Palermo**

- Please write your name in the space provided below
- Please verify that there are 4 pages in your exam
- You may use one double-sided page of notes and equations for the exam
- Good Luck!

Problem	Score	Max Score
1		50
2		50
<b>Total</b>		<b>100</b>

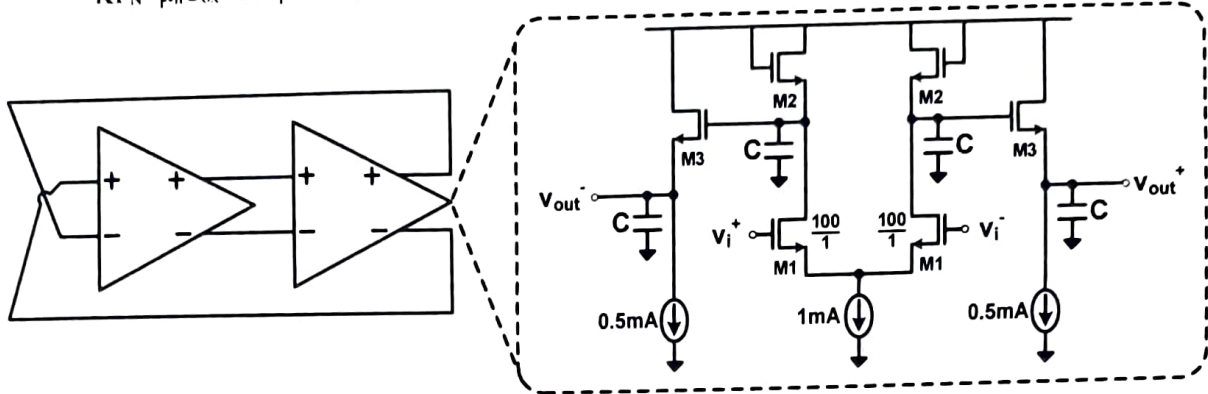
Name: SAM PALERMO

UIN: \_\_\_\_\_

Problem 1 (50 points)

A differential ring oscillator is shown below. Assume that all transistors are operating in saturation with  $r_o = \infty$  and you can ignore any transistor device capacitors. Assume that  $C = 100\text{fF}$  and use the following NMOS parameters

$$K_{PN} = \mu_n C_{ox} = 600 \mu\text{A}/\text{V}^2, V_{TN} = 0.35\text{V}, \lambda_N = 0\text{V}^{-1}$$



- Assume that for M2 and M3 that  $W_2/L_2 = W_3/L_3$ . Determine the sizes (W/L) of M2 and M3 to achieve oscillation.
- What is the oscillation frequency?

a. Each oscillator cell:

$$\left[ \frac{g_{m1}}{g_{m2}} \right] \left[ \frac{1}{1 + \frac{sC}{g_{m2}}} \right]$$

$$H(s) = \left[ \frac{g_{m1}}{g_{m2}} \right]^2 \left[ \frac{1}{1 + \frac{sC}{g_{m3}}} \right]^2$$

$$\begin{aligned}
 \omega_{osc} &= \frac{g_{mL}}{C} \\
 &= \frac{\sqrt{K_{PN}} \left(\frac{W}{L}\right)_2 2I_0}{C} \\
 &= \frac{\sqrt{(600 \mu)(25)(2)(0.5\text{mA})}}{100\text{fF}} \\
 &= 38.76 \text{ rad/s} = 6.17 \text{ GHz}
 \end{aligned}$$

To oscillate each cell should contribute a phase shift of

$$\frac{360^\circ - 180^\circ}{2} = 90^\circ$$

Since  $\left(\frac{W}{L}\right)_2 = \left(\frac{W}{L}\right)_3$  and  $I_2 = I_3 \Rightarrow g_{m2} = g_{m3}$ . Thus, each cell has

2 poles that are both at  $-\frac{g_{m2}}{C}$

$\Rightarrow$  Circuit will oscillate when each pole gives  $45^\circ$ , which is  $W_2/L_2 = W_3/L_3 = \frac{25}{1}$

$$\omega_{osc} = \omega_p = \frac{g_{m2}}{C}$$

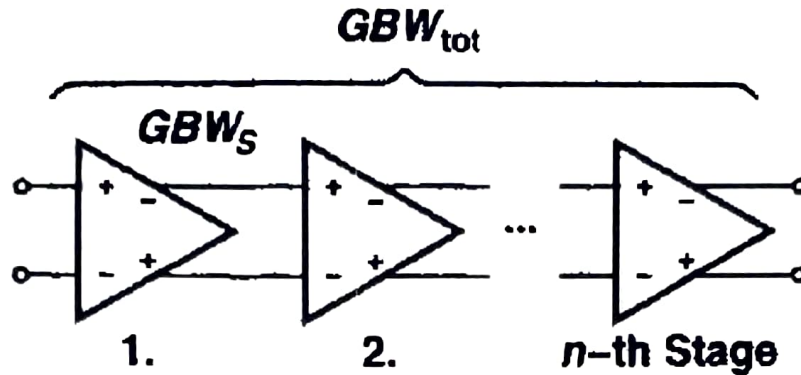
$$f_{osc} = 6.17 \text{ GHz}$$

At  $\omega_{osc}$ , the gain is  $\frac{g_{m1}}{g_{m2}} \left(\frac{1}{\sqrt{2}}\right) \left(\frac{1}{\sqrt{2}}\right) = \frac{g_{m1}}{2g_{m2}}$  which needs to equal 1,

$$\frac{g_{m1}}{2g_{m2}} = \frac{\sqrt{K_{PN}} \left(\frac{W}{L}\right)_1 2I_0}{2\sqrt{K_{PN}} \left(\frac{W}{L}\right)_2 2I_0} = \frac{1}{2} \sqrt{\frac{\left(\frac{W}{L}\right)_1}{\left(\frac{W}{L}\right)_2}} = 1 \Rightarrow \left(\frac{W}{L}\right)_2 = \frac{\left(\frac{W}{L}\right)_1}{4} = \frac{25}{1}$$

Problem 2 (50 points)

Assume that the limiting amplifier below consists of cascaded identical single-pole amplifier stages, with gain  $A_{vs}$  and bandwidth  $\omega_{3dBs}$ .



- a) Design the limiting amplifier to achieve a 34dB total gain and 20GHz total bandwidth with the minimum per-stage gain-bandwidth product. Give the stage number and the per-stage gain and bandwidth. Also compute the per-stage gain-bandwidth product.

$$n_{opt} = 2 \ln(G_{tot}) = 2 \ln(50.1) = 7.83 \Rightarrow \text{use } 8 \text{ stages}$$

$$W/n = 8 \quad A_{vs} = \sqrt[8]{50.1} = 1.63$$

$$W_{3dB_{tot}} = W_{3dB_s} \sqrt{2^n - 1} \Rightarrow W_{3dB_s} = \frac{W_{3dB_{tot}}}{\sqrt{2^n - 1}} = \frac{2\pi(20\text{GHz})}{\sqrt{2^8 - 1}} = 4176 \text{ rad/s} = 66.56 \text{ Hz}$$

$$GBW_s = (1.63)(4176 \text{ rad/s}) = 6806 \text{ rad/s} = 108 \text{ GHz}$$

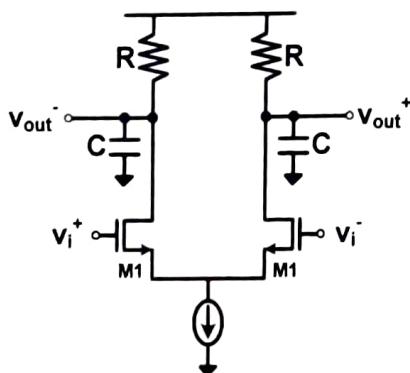
$$n = 8$$

$$A_{vs} = 1.63$$

$$\omega_{3dB_s} = 4176 \text{ rad/s} \quad (66.56 \text{ Hz})$$

$$GBW_s = 6806 \text{ rad/s} \quad (108 \text{ GHz})$$

- b) Assume that the simple differential amplifier stage shown below can only achieve a maximum  $GBW_s = 70 \text{ GHz}$ . Propose a change to the stage design below to achieve the required  $GBW_s$  from part (a).



⇒ Add shunt peaking inductors

$$W/L = \frac{R^2 C}{2.41} \text{ can}$$

increase BW by 72%  
(6806 rad/s to up to 120 GHz)

w/ no peaking in magnitude response.