

Texas A&M University
Department of Electrical and Computer Engineering

ECEN 474 – (Analog) VLSI Circuit Design

Fall 2012

Exam #2

Instructor: Sam Palermo

- Please write your name in the space provided below
- Please verify that there are 5 pages (1 blank) in your exam
- You may use one double-sided page of notes and equations for the exam
- Good Luck!

Problem	Score	Max Score
1		30
2		30
3		40
Total		100

Name: _____

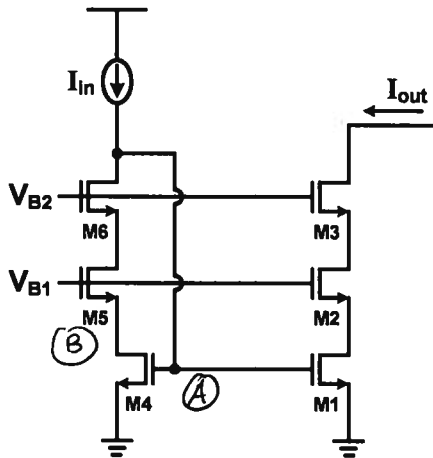
SAM PALERMO

UIN: _____

Problem 1 (30 points)

For the following current source obtain the following:

- Give an expression for the output resistance. You can assume that all transistors are operating in saturation and that you can neglect body effect.
- Give an expression for the compliance voltage at the output necessary to keep all transistors in saturation.
- Assume that all of the same transistors have the same V_{DSAT} value and that $V_{Tn}=0.7V$. What is the maximum V_{DSAT} voltage possible, while all of the transistors are still in saturation?



a. $r_o \cong r_{o3} g_{m3} r_{o2} g_{m2} r_{o1}$

b. Compliance Voltage:

$$V_{out} \geq V_{DSAT1} + V_{DSAT2} + V_{DSAT3}$$

c. Node A = $V_T + V_{OSAT}$

Node B = $A - 2V_{DSAT} = V_T + V_{OSAT} - 2V_{DSAT} = V_T - V_{DSAT}$

$$V_B \geq V_{DSAT}$$

$$V_T - V_{OSAT} \geq V_{DSAT}$$

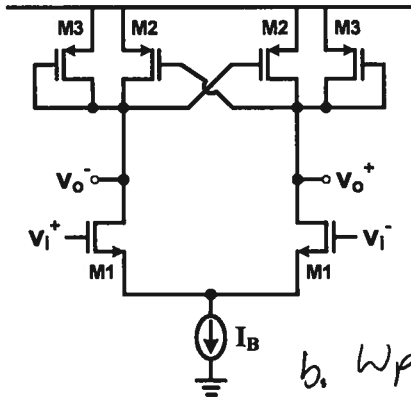
$$V_{OSAT} \leq \frac{V_T}{2} = \frac{0.7V}{2} = 0.35V$$

$$V_{OSAT} \leq 0.35V$$

Problem 2 (30 points)

For the fully differential amplifier below obtain the following:

- a) Give an expression for the differential gain, $A_{vd} = (v_o^+ - v_o^-) / (v_i^+ - v_i^-)$. Do NOT neglect the transistors' r_o . Assume all transistors are operating in saturation and that you can neglect body effect.
- b) Give an expression for the dominant pole of the amplifier. This expression should include all the appropriate transistor capacitances and include the Miller effect when appropriate.



$$a. A_{vd} = \frac{g_{m1}}{g_{m3} - g_{m2} + g_{o1} + g_{o2} + g_{o3}}$$

$$b. \omega_p = \frac{g_{m3} - g_{m2} + g_{o1} + g_{o2} + g_{o3}}{C_{DB1} + C_{DG1} + C_{DB2} + C_{GS2} + 4(C_{GD2} + C_{DB3} + C_{GS3})}$$

Note neglecting Miller in C_{GD1} because $1 - (A_{DG1}) = 1 - (-\frac{1}{A_{vd}})$

Need to include Miller in $C_{GD2} = C_{DG2}$ total is $4C_{GD}$ w/miller
 If we consider $v_o^+ \Rightarrow C_{DG2} (1 - (-1)) = 2C_{DG2}$, $C_{GD2} (1 - (-1)) = 2C_{GD2}$
 this is generally very small

- c) Now simplify the differential gain expression by letting the transistors' $r_o = \infty$. Assume that $\mu_n = 4\mu_p$ and that the transistors have the following transistor sizes:

M1 Size = W/L

M2 Size = $\alpha * W/L$

M3 Size = $(1-\alpha) * W/L$

What should α be to achieve a differential gain of 4?

$$A_{vd} = \frac{g_{m1}}{g_{m3} - g_{m2}}$$

$$A_{vd} = \frac{\sqrt{\mu_n} \left(\alpha \frac{W}{L} \right) 2 \left(\frac{I_B}{2} \right)}{\sqrt{\mu_p} \left(\alpha (1-\alpha) \frac{W}{L} \right) 2 \left(\frac{I_B}{2} \right) (1-\alpha) - \sqrt{\mu_p} \left(\alpha \frac{W}{L} \right) 2 \left(\frac{I_B}{2} \right) \alpha}$$

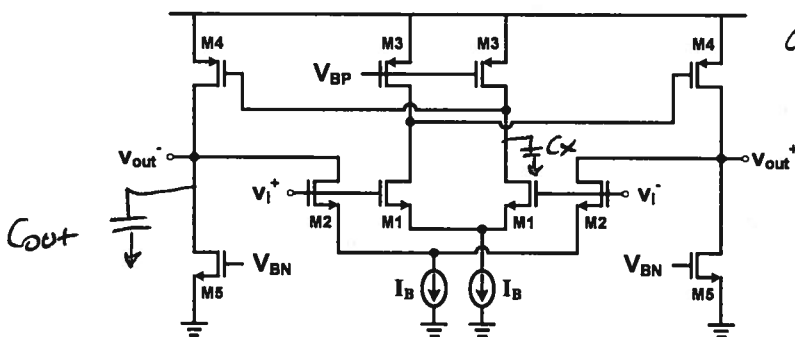
$$= \sqrt{\frac{\mu_n}{\mu_p}} \left(\frac{1}{1-\alpha-\alpha} \right) = \frac{2}{1-2\alpha} = 4$$

$$1 - 2\alpha = \frac{1}{2} \Rightarrow \alpha = \frac{1}{4}$$

$$\boxed{\alpha = \frac{1}{4}}$$

Problem 3 (40 points)

- d) For the amplifier below, assume all transistors are operating in saturation and that you can neglect body effect. Obtain expressions for the following:
 - a) Small-signal transconductance.
 - b) Output resistance.
 - c) DC gain.
 - d) The amplifier's two poles. Note, it's OK here to state this as a function of an effective capacitance at a certain node, but make sure to appropriately label the nodes.
 - e) Output referred noise current power spectral density. Consider only thermal noise and include all important noise sources.
 - f) Input referred noise voltage power spectral density. Consider only thermal noise and include all important noise sources.



a. $\frac{g_{m1} g_{m4}}{g_{o1} + g_{o3}} + g_{m2}$

b. $R_{out} = \frac{1}{g_{o2} + g_{o4} + g_{o5}}$

c. $A_v = G_m R_{out} = \frac{\frac{g_{m1} g_{m4}}{g_{o1} + g_{o3}} + g_{m2}}{g_{o2} + g_{o4} + g_{o5}}$

d. $\omega_{p1} = \frac{g_{o2} + g_{o4} + g_{o5}}{C_{out}}, \omega_{p2} = \frac{g_{o1} + g_{o3}}{C_x}$

e. $\frac{i_{o,n}^2}{\Delta f} = (i_{o1}^2 + i_{o2}^2 + i_{o3}^2 + i_{o4}^2 + i_{o5}^2) \cdot 2 =$

$\frac{16}{3} kT \left(g_{m1} \left(\frac{1}{g_{o1} + g_{o3}} \right)^2 g_{m4}^2 + g_{m2} + g_{m3} \left(\frac{1}{g_{o1} + g_{o3}} \right)^2 g_{m4}^2 + g_{m4} + g_{m5} \right)$

f. $\frac{v_{i,n}^2}{\Delta f} = \frac{i_{o,n}^2}{\Delta f} \left(\frac{1}{G_m} \right)^2$

Scratch Paper