

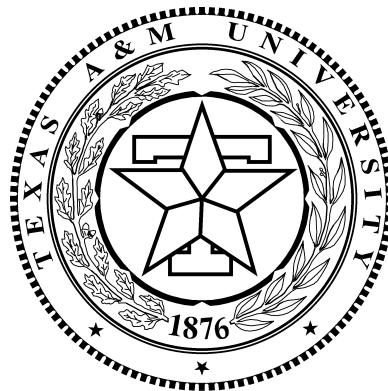
# ECEN 326

## Electronic Circuits

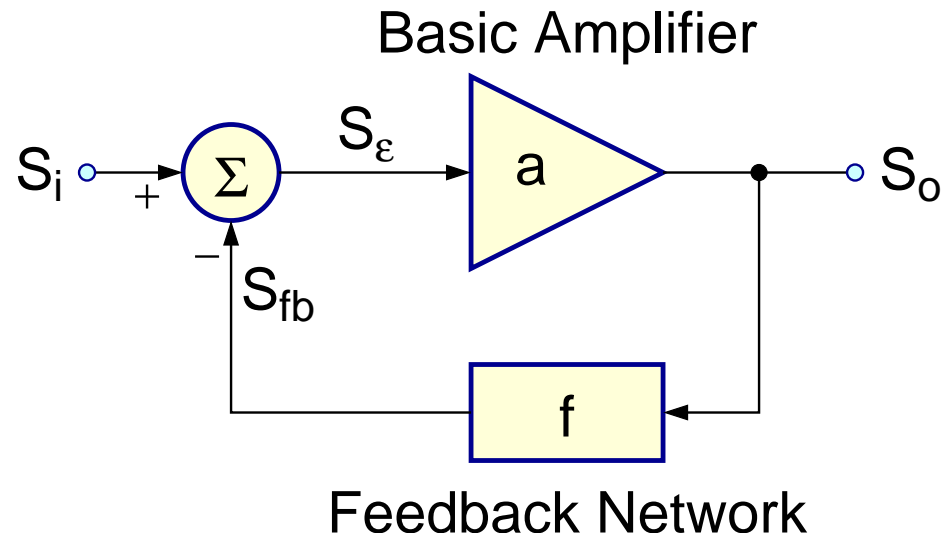
Feedback

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Texas A&M University  
Department of Electrical and Computer Engineering



# Ideal Feedback Configuration



$$\frac{S_o}{S_i} = A = \frac{a}{1 + T} \quad , \quad T = af$$

$$\frac{S_\epsilon}{S_i} = \frac{1}{1 + T} \quad , \quad \frac{S_{fb}}{S_i} = \frac{T}{1 + T}$$

Gain of the basic amplifier ( $a$ ) usually depends on temperature, operating conditions and process parameters.

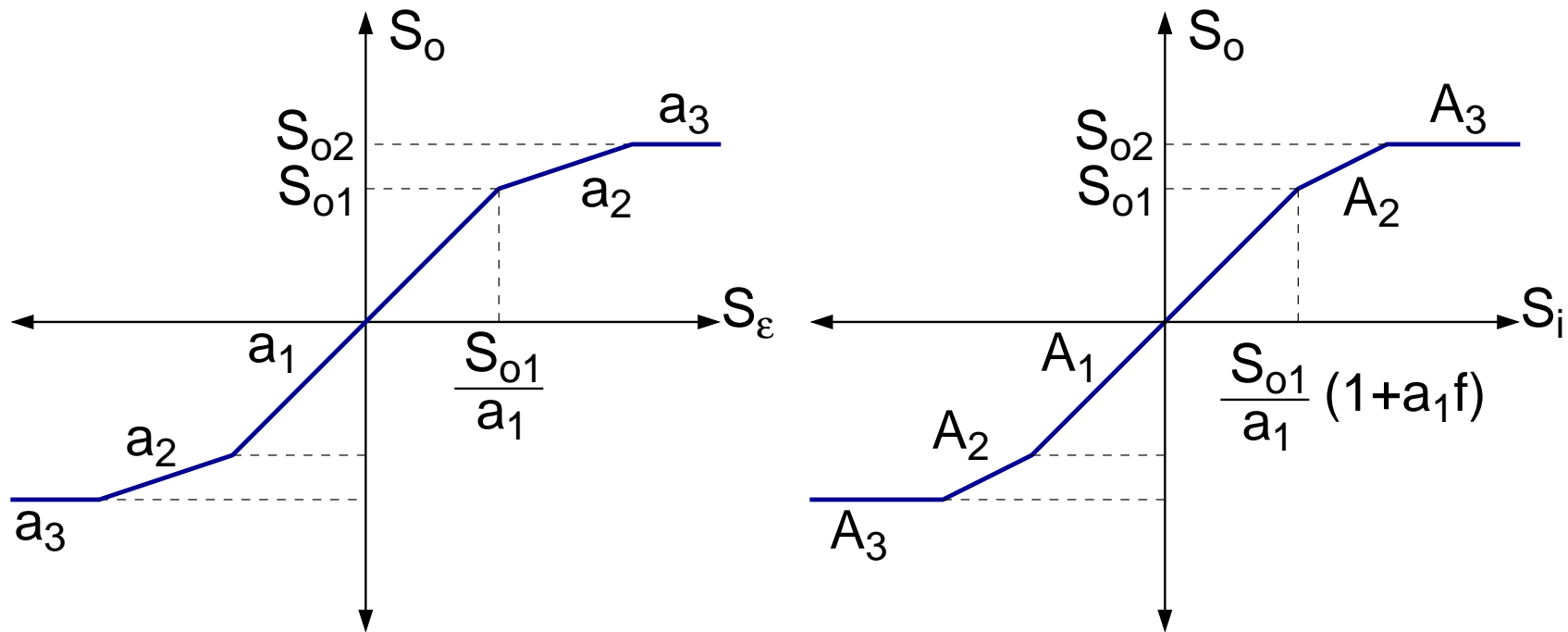
$$\frac{dA}{da} = \frac{(1 + af) - af}{(1 + af)^2} = \frac{1}{(1 + af)^2}$$

$$\delta A = \frac{\delta a}{(1 + af)^2} \Rightarrow \frac{\delta A}{A} = \frac{1 + af}{a} \frac{\delta a}{(1 + af)^2}$$

$$\frac{\delta A}{A} = \frac{\frac{\delta a}{a}}{1 + af} = \frac{\frac{\delta a}{a}}{1 + T}$$

# Effect of Feedback

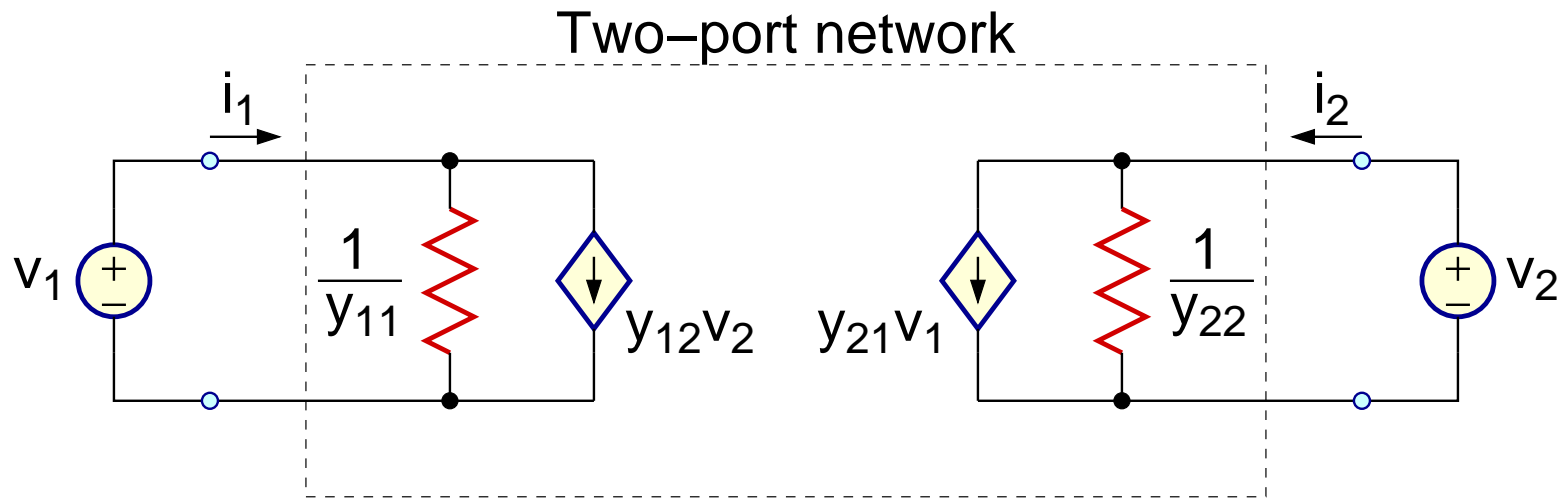
## Distortion



$$A_1 = \frac{a_1}{1 + a_1f} \approx \frac{1}{f} , \quad A_2 = \frac{a_2}{1 + a_2f} \approx \frac{1}{f}$$

# Two-Port Networks

y parameters



$$i_1 = y_{11}v_1 + y_{12}v_2$$

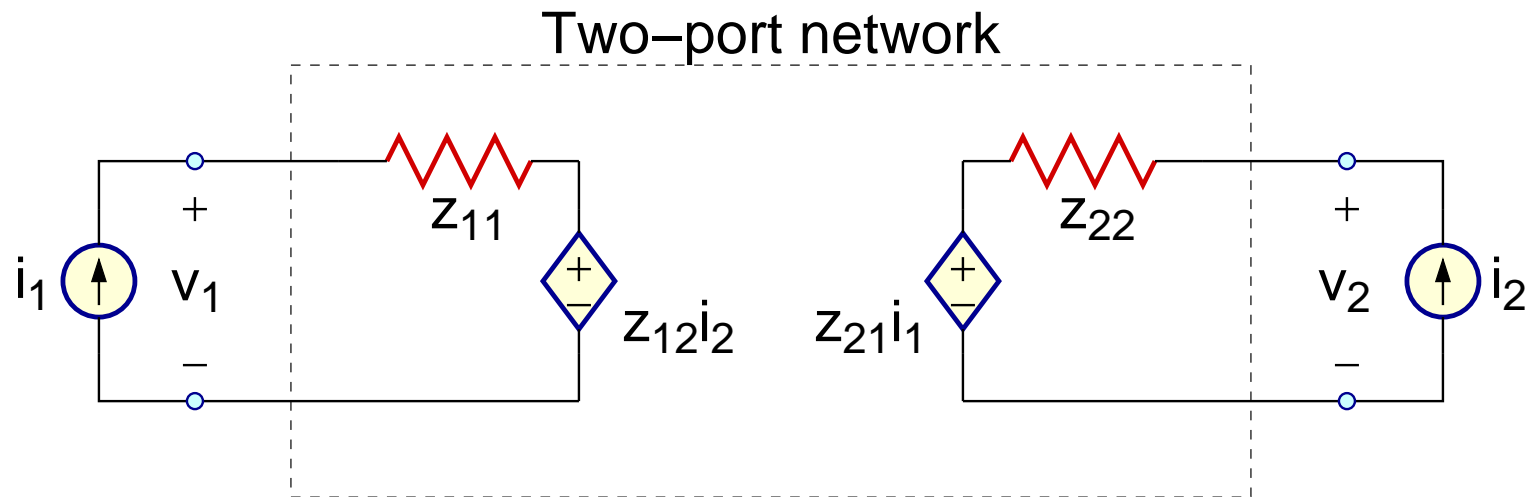
$$i_2 = y_{21}v_1 + y_{22}v_2$$

$$y_{11} = \left. \frac{i_1}{v_1} \right|_{v_2=0}, \quad y_{12} = \left. \frac{i_1}{v_2} \right|_{v_1=0}$$

$$y_{21} = \left. \frac{i_2}{v_1} \right|_{v_2=0}, \quad y_{22} = \left. \frac{i_2}{v_2} \right|_{v_1=0}$$

# Two-Port Networks

z parameters



$$v_1 = z_{11}i_1 + z_{12}i_2$$

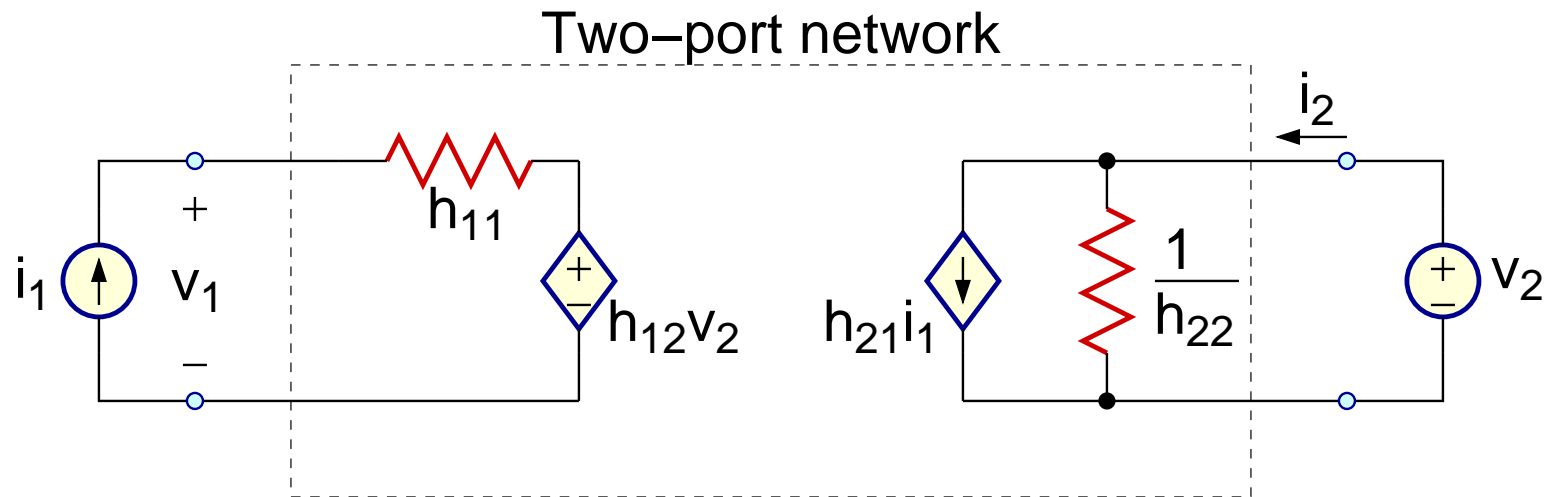
$$v_2 = z_{21}i_1 + z_{22}i_2$$

$$z_{11} = \left. \frac{v_1}{i_1} \right|_{i_2=0}, \quad z_{12} = \left. \frac{v_1}{i_2} \right|_{i_1=0}$$

$$z_{21} = \left. \frac{v_2}{i_1} \right|_{i_2=0}, \quad z_{22} = \left. \frac{v_2}{i_2} \right|_{i_1=0}$$

# Two-Port Networks

## h parameters



$$v_1 = h_{11}i_1 + h_{12}v_2$$

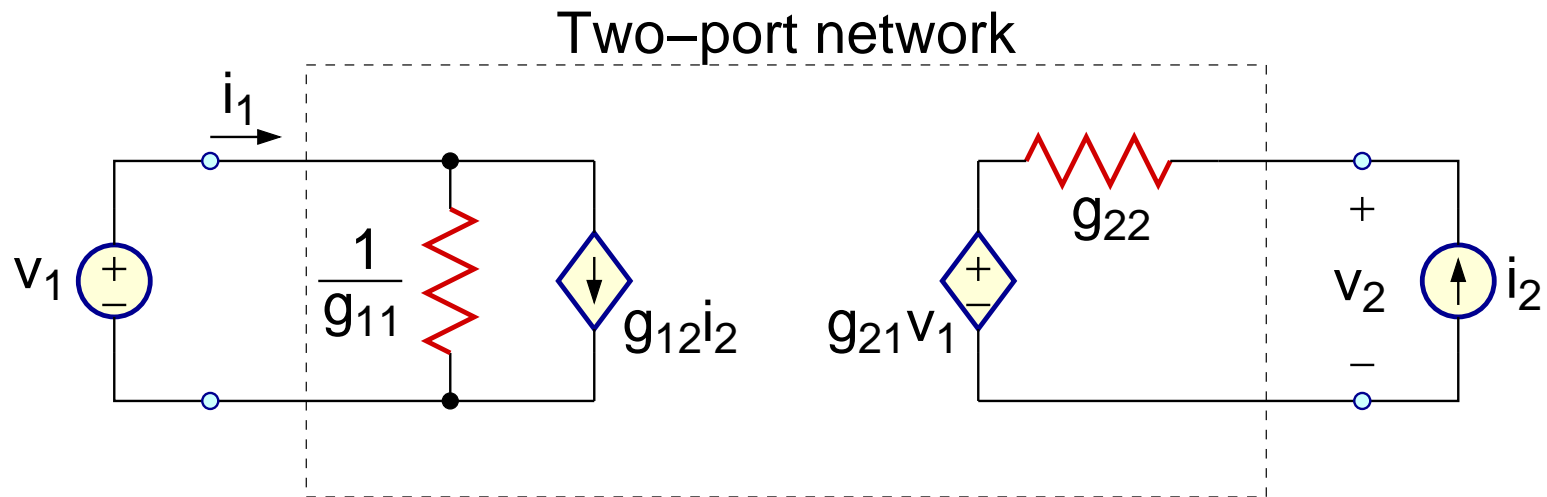
$$i_2 = h_{21}i_1 + h_{22}v_2$$

$$h_{11} = \left. \frac{v_1}{i_1} \right|_{v_2=0}, \quad h_{12} = \left. \frac{v_1}{v_2} \right|_{i_1=0}$$

$$h_{21} = \left. \frac{i_2}{i_1} \right|_{v_2=0}, \quad h_{22} = \left. \frac{i_2}{v_2} \right|_{i_1=0}$$

# Two-Port Networks

g parameters



$$i_1 = g_{11}v_1 + g_{12}i_2$$

$$v_2 = g_{21}v_1 + g_{22}i_2$$

$$g_{11} = \left. \frac{i_1}{v_1} \right|_{i_2=0}, \quad g_{12} = \left. \frac{i_1}{i_2} \right|_{v_1=0}$$

$$g_{21} = \left. \frac{v_2}{v_1} \right|_{i_2=0}, \quad g_{22} = \left. \frac{v_2}{i_2} \right|_{v_1=0}$$



# Feedback Configurations

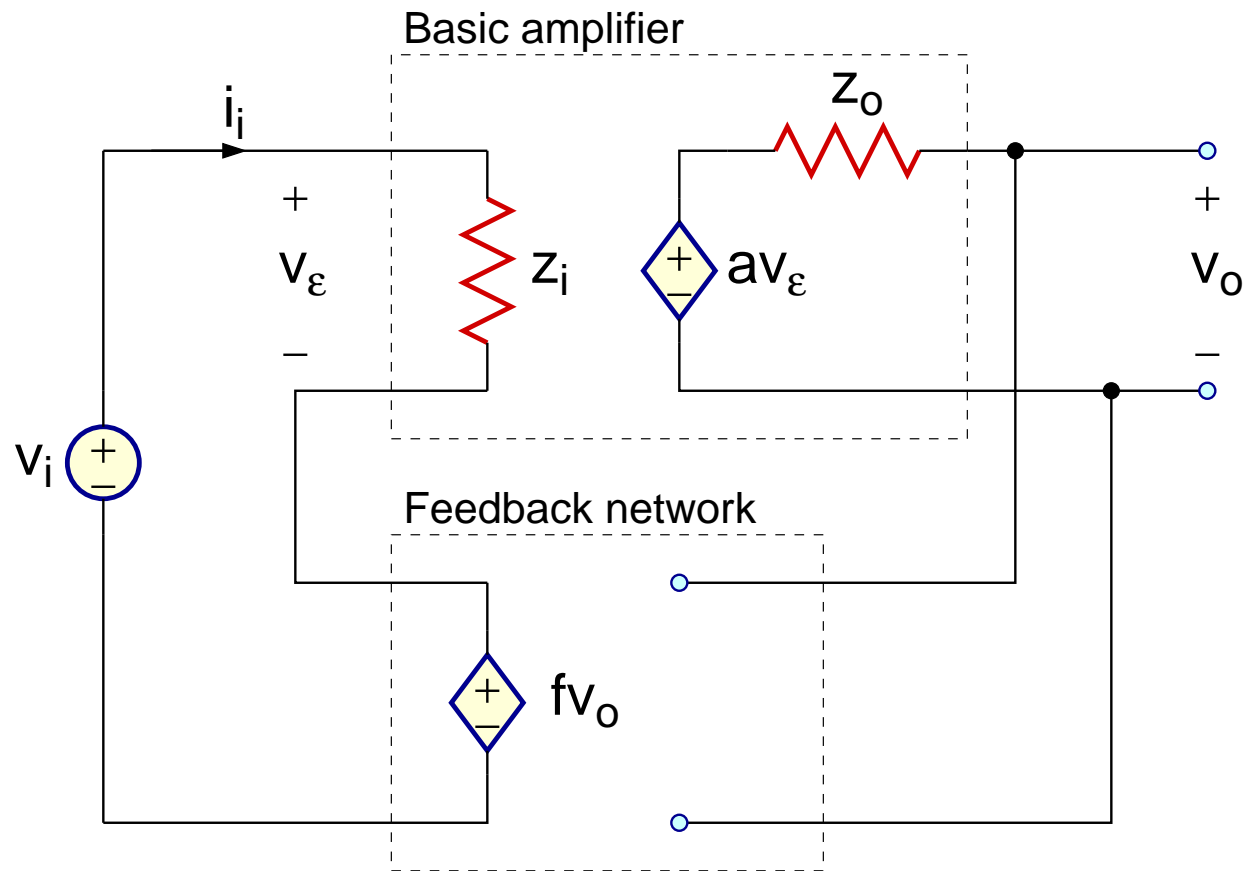
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According to whether the output signal  $\mathbf{S}_o$  is a current or a voltage and whether the feedback signal  $\mathbf{S}_{fb}$  is a current or a voltage, four feedback configurations exist:

- Series-Shunt Feedback  
 $\mathbf{S}_{fb} = \mathbf{v}_{fb}$  (voltage),  $\mathbf{S}_o = \mathbf{v}_o$  (voltage)
- Shunt-Shunt Feedback  
 $\mathbf{S}_{fb} = \mathbf{i}_{fb}$  (current),  $\mathbf{S}_o = \mathbf{v}_o$  (voltage)
- Shunt-Series Feedback  
 $\mathbf{S}_{fb} = \mathbf{i}_{fb}$  (current),  $\mathbf{S}_o = \mathbf{i}_o$  (current)
- Series-Series Feedback  
 $\mathbf{S}_{fb} = \mathbf{v}_{fb}$  (voltage),  $\mathbf{S}_o = \mathbf{i}_o$  (current)

# Series-Shunt

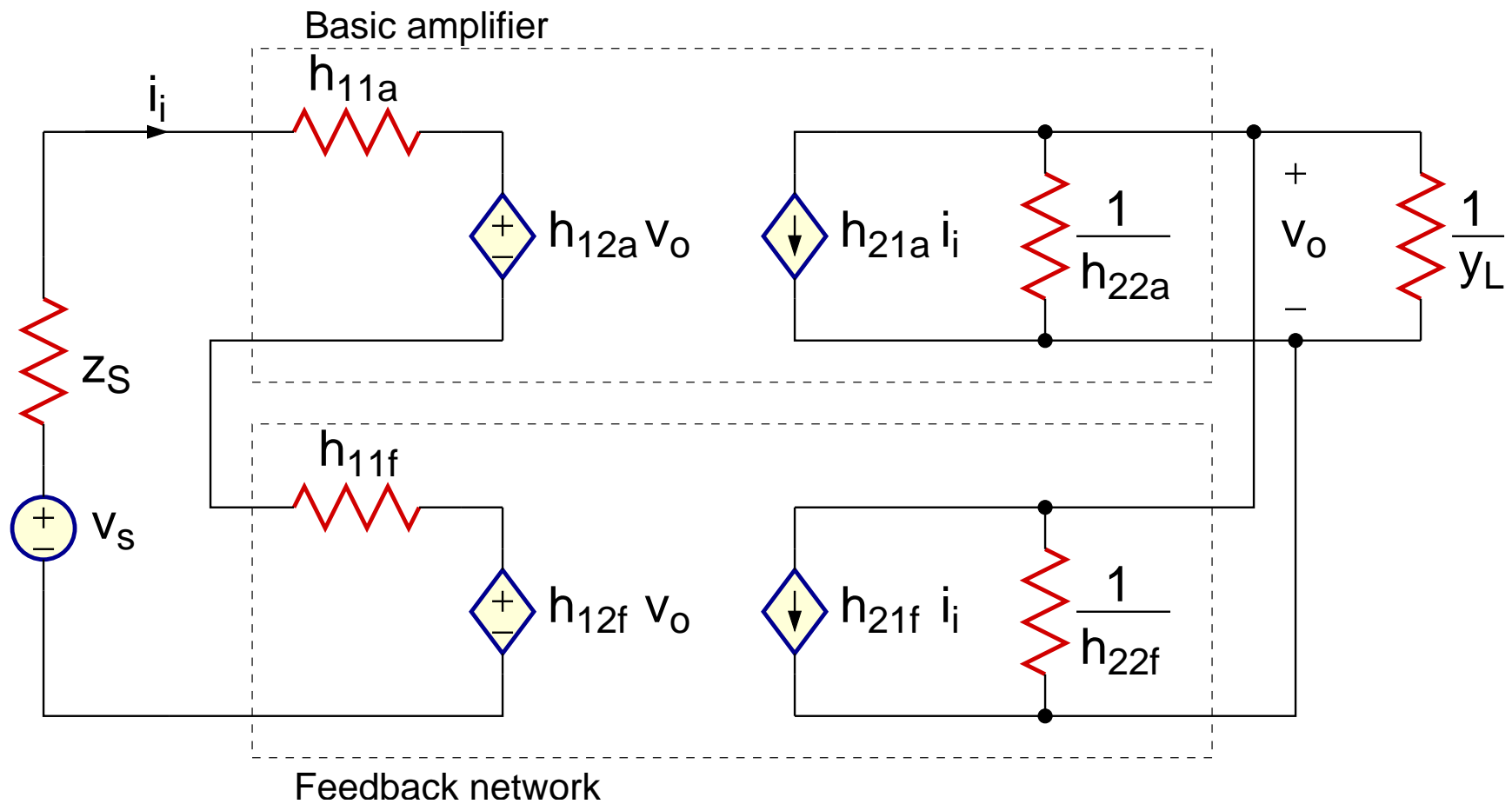
Ideal



$$\frac{v_o}{v_i} = \frac{a}{1 + af} \quad z_i = (1 + af)z_i \quad z_o = \frac{z_o}{1 + af}$$

# Series-Shunt

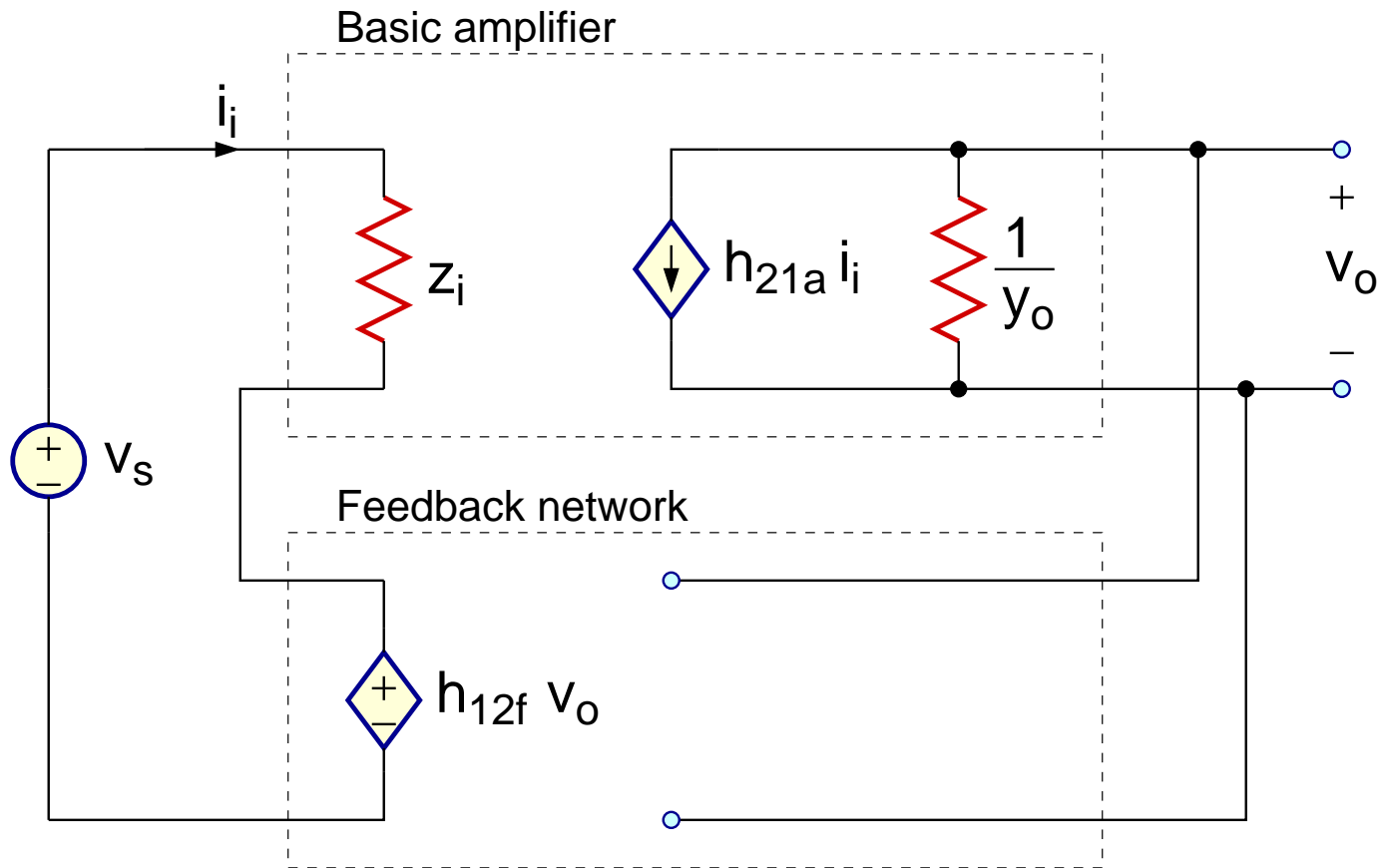
h-parameter representation



$$|h_{12f}| \gg |h_{12a}| \quad |h_{21a}| \gg |h_{21f}|$$

# Series-Shunt

h-parameter representation - simplified

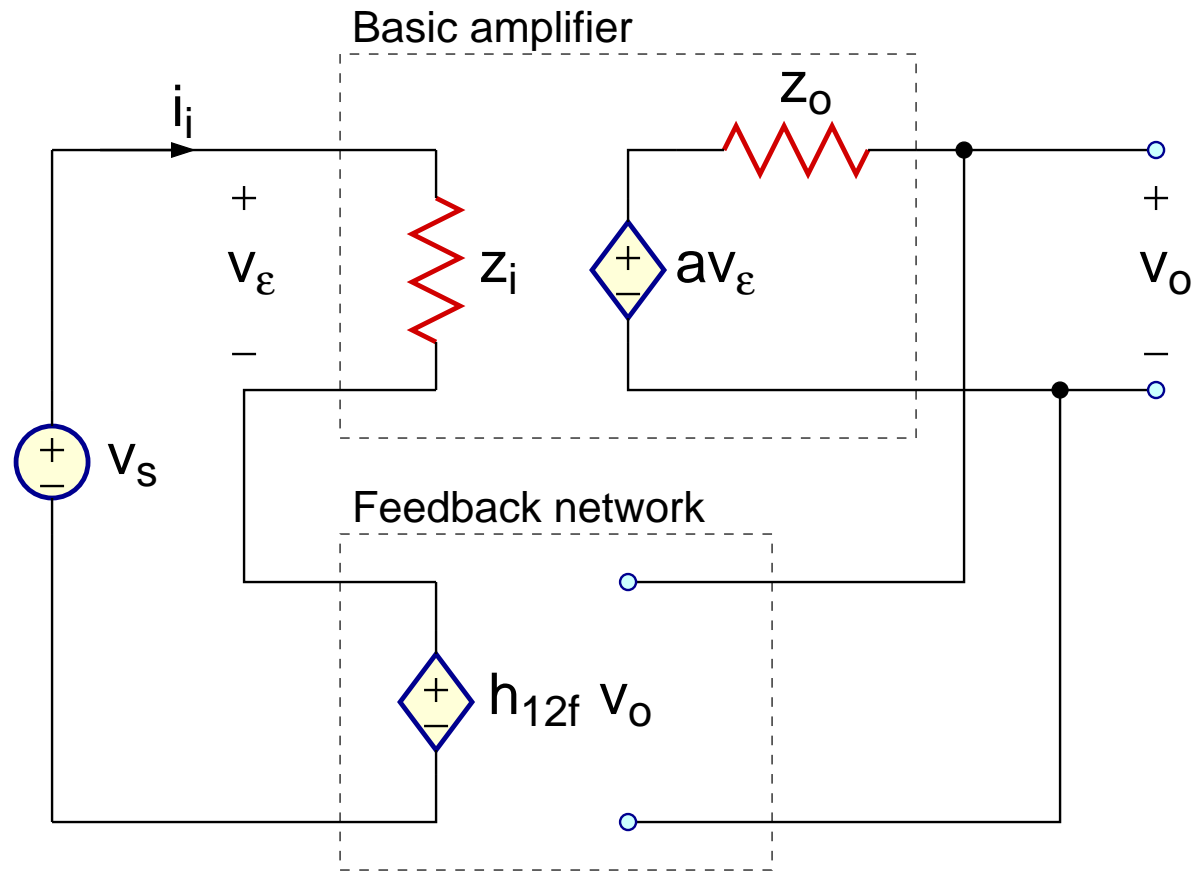


$$z_i = z_S + h_{11a} + h_{11f}$$

$$y_o = y_L + h_{22a} + h_{22f}$$

# Series-Shunt

h-parameter representation - simplified



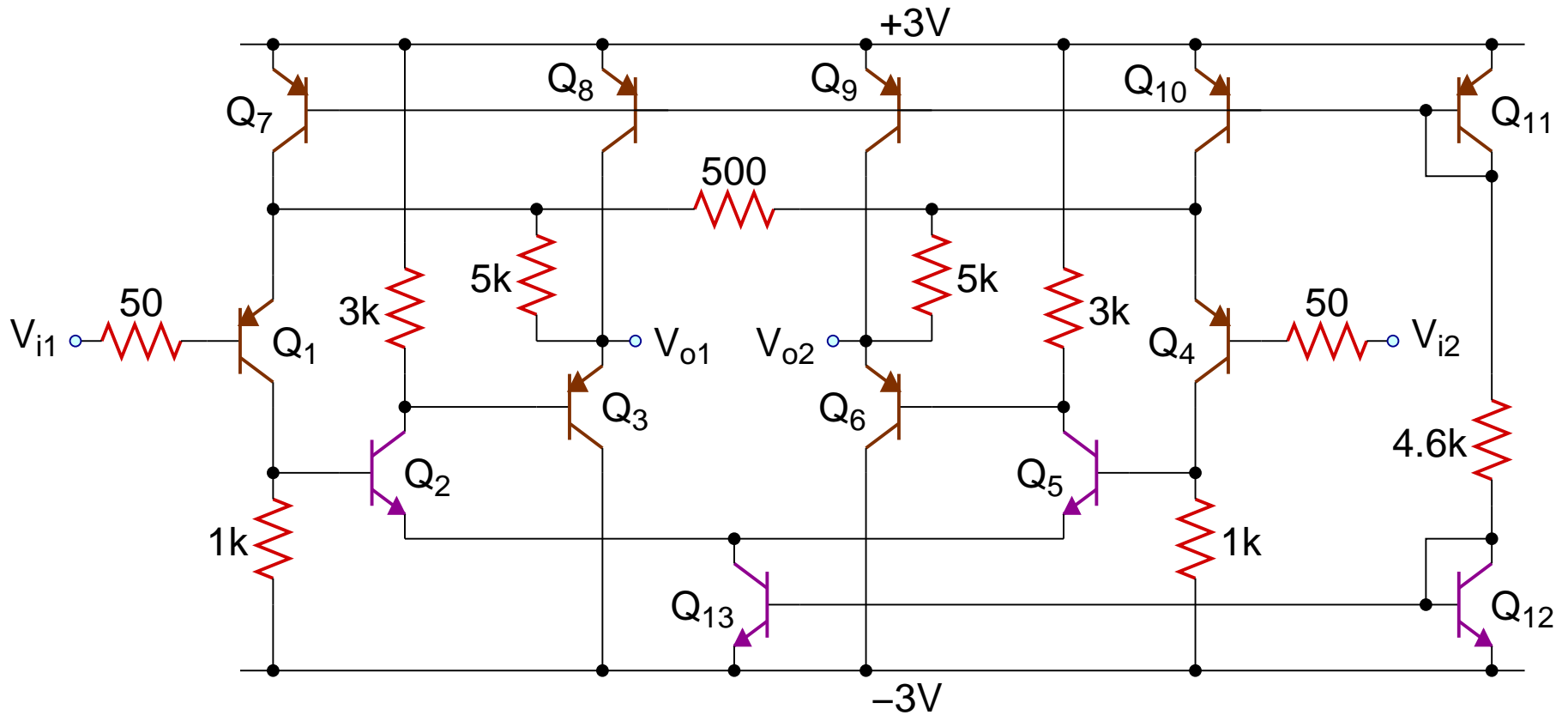
$$a = -\frac{h_{21a}}{z_i y_o}$$

$$f = h_{12f}$$

$$z_o = \frac{1}{y_o}$$

# Series-Shunt

Example

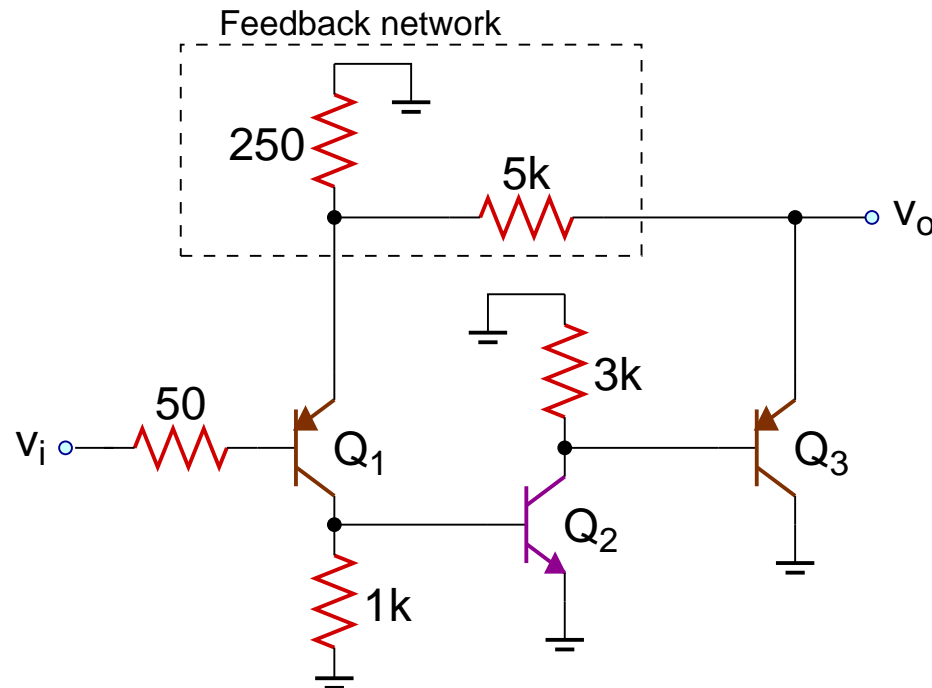


$$V_{i1,dc} = V_{i2,dc} = 0, \quad V_A = \infty, \quad V_T = 25mV, \quad \beta = 100$$

# Series-Shunt

## Example

Differential-mode AC half circuit:



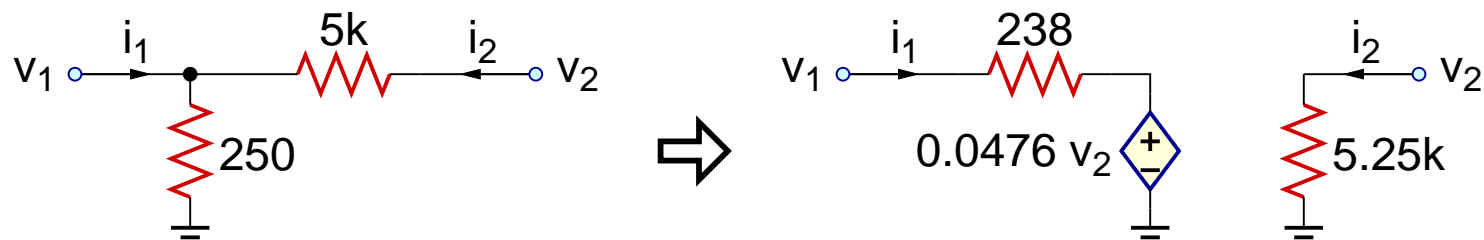
Input: Voltage  
Output: Voltage

$$I_{C1} = 1.3 \text{ mA}$$

$$I_{C2} = 0.5 \text{ mA}$$

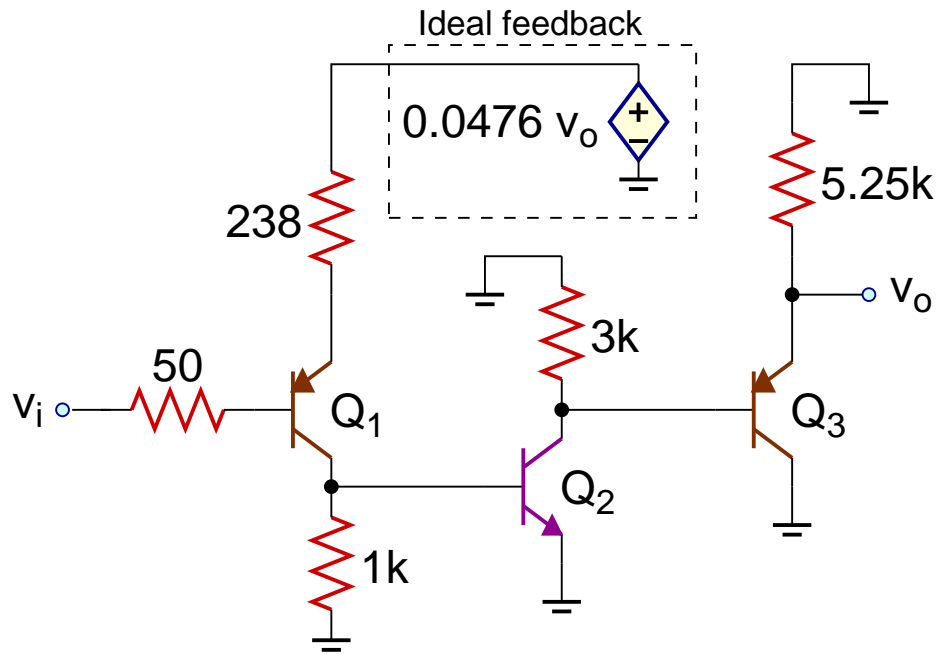
$$I_{C3} = 0.7 \text{ mA}$$

h-parameter representation of the feedback network:

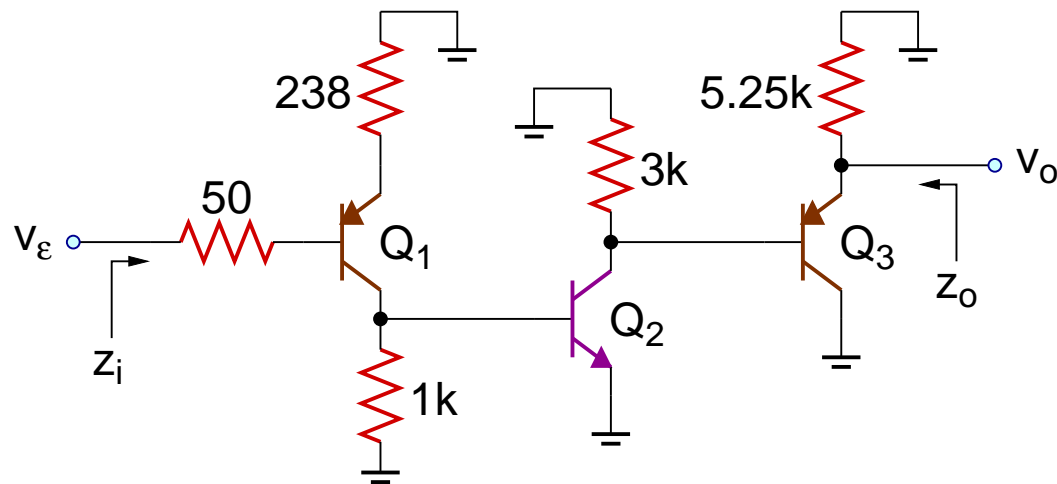


# Series-Shunt

## Example



$$f = 0.0476$$



$$a = \frac{v_o}{v_\epsilon} = 192$$

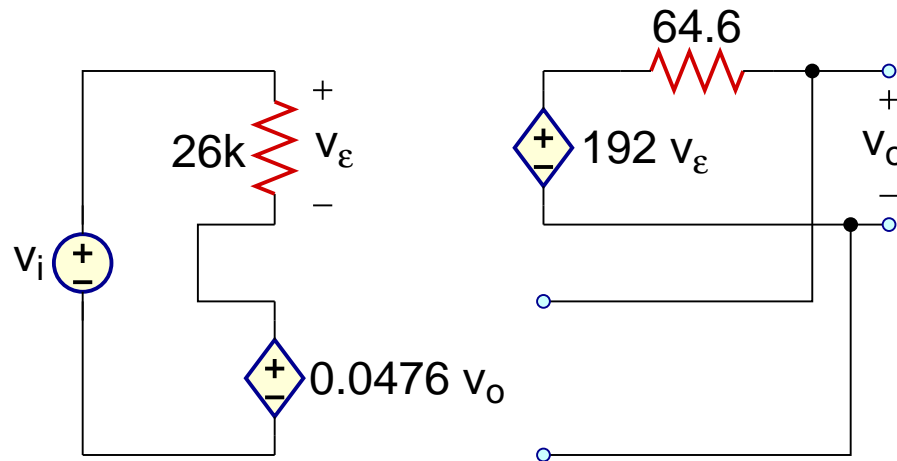
$$z_i = 26 \text{ k}\Omega$$

$$z_o = 64.6 \text{ }\Omega$$



# Series-Shunt

## Example

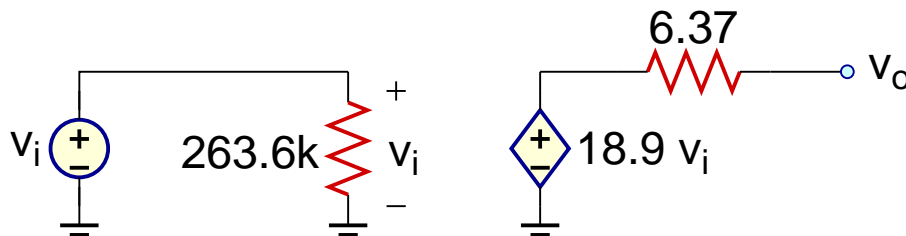


$$a = 192$$

$$f = 0.0476$$

$$z_i = 26 \text{ k}\Omega$$

$$z_o = 64.6 \Omega$$



$$A = \frac{v_o}{v_i} = \frac{a}{1 + af} = 18.9$$

$$Z_i = z_i(1 + af) = 263.6 \text{ k}\Omega$$

$$Z_o = \frac{z_o}{1 + af} = 6.37 \Omega$$

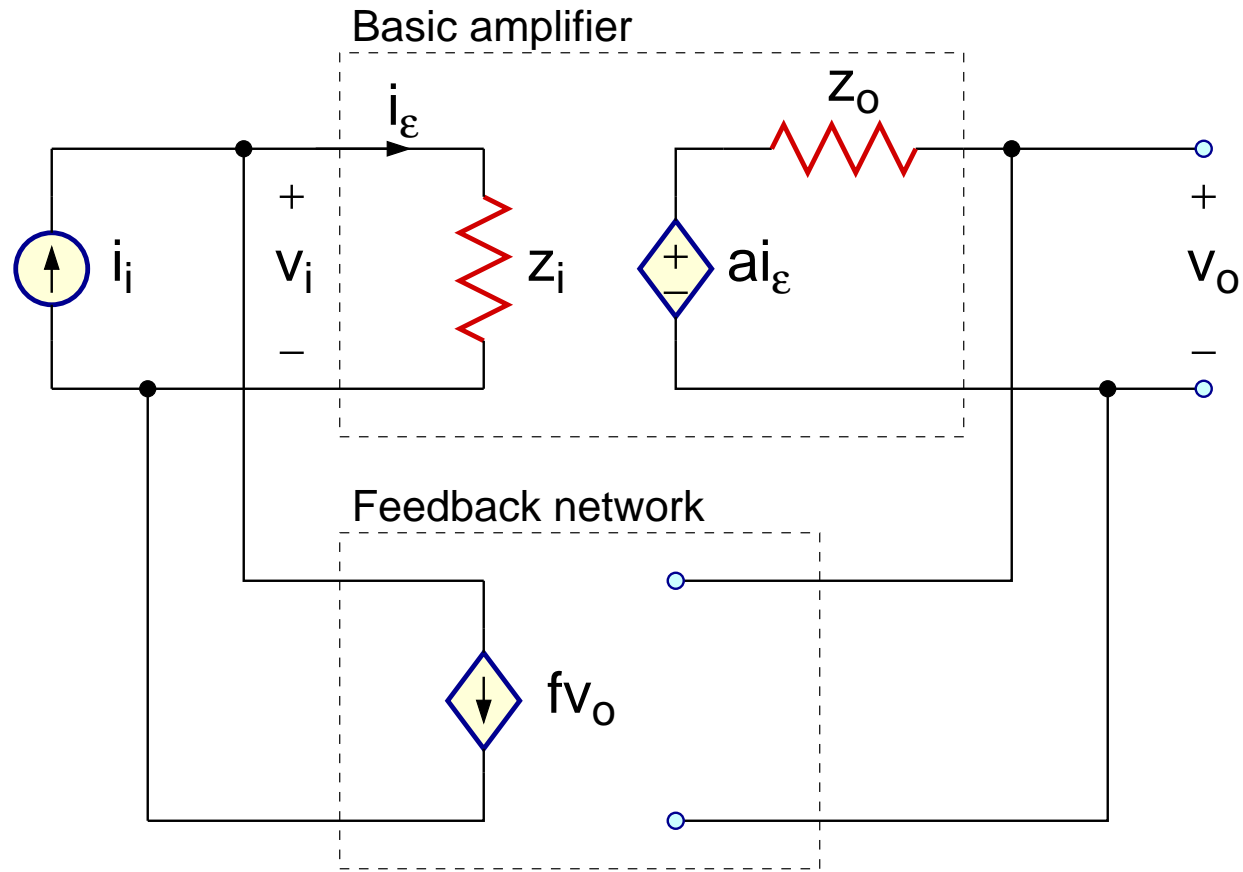
$$A_{dm} = 18.9$$

$$R_{id} = 2 \times 263.6 \text{ k} = 527.2 \text{ k}\Omega$$

$$R_{od} = 2 \times 6.37 = 12.7 \Omega$$

# Shunt-Shunt

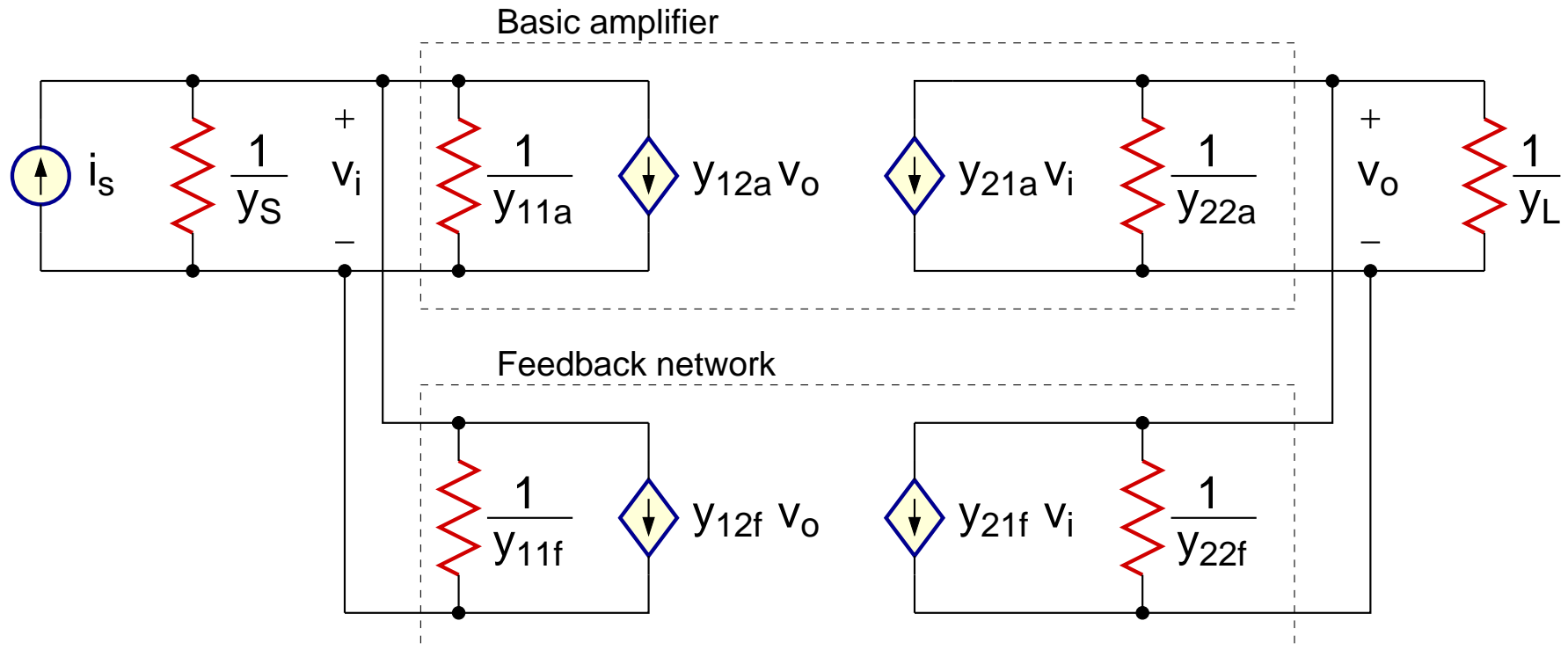
Ideal



$$\frac{v_o}{i_i} = \frac{a}{1 + af} \quad Z_i = \frac{z_i}{1 + af} \quad Z_o = \frac{z_o}{1 + af}$$

# Shunt-Shunt

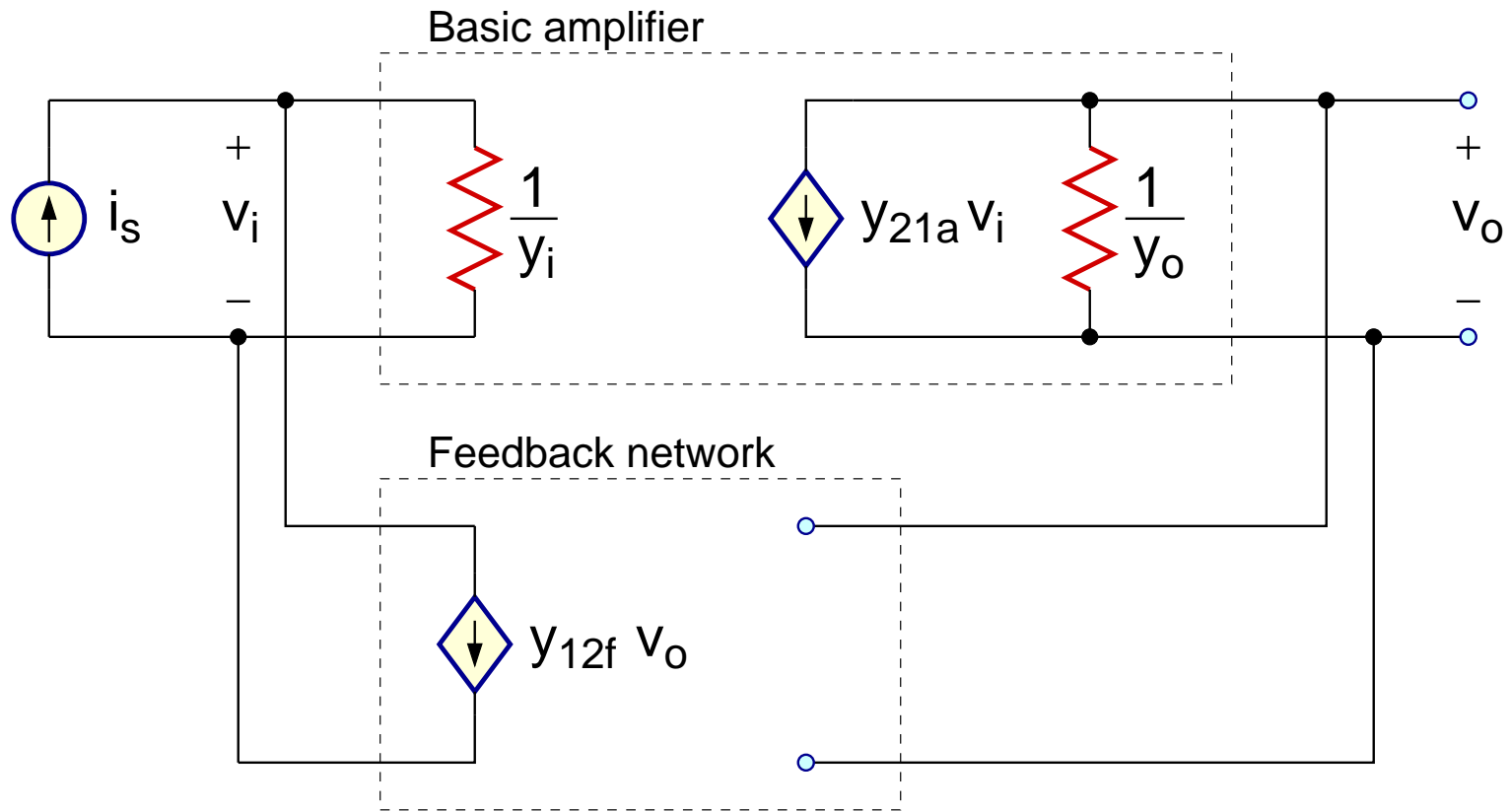
y-parameter representation



$$|y_{12f}| \gg |y_{12a}| \quad |y_{21a}| \gg |y_{21f}|$$

# Shunt-Shunt

y-parameter representation - simplified

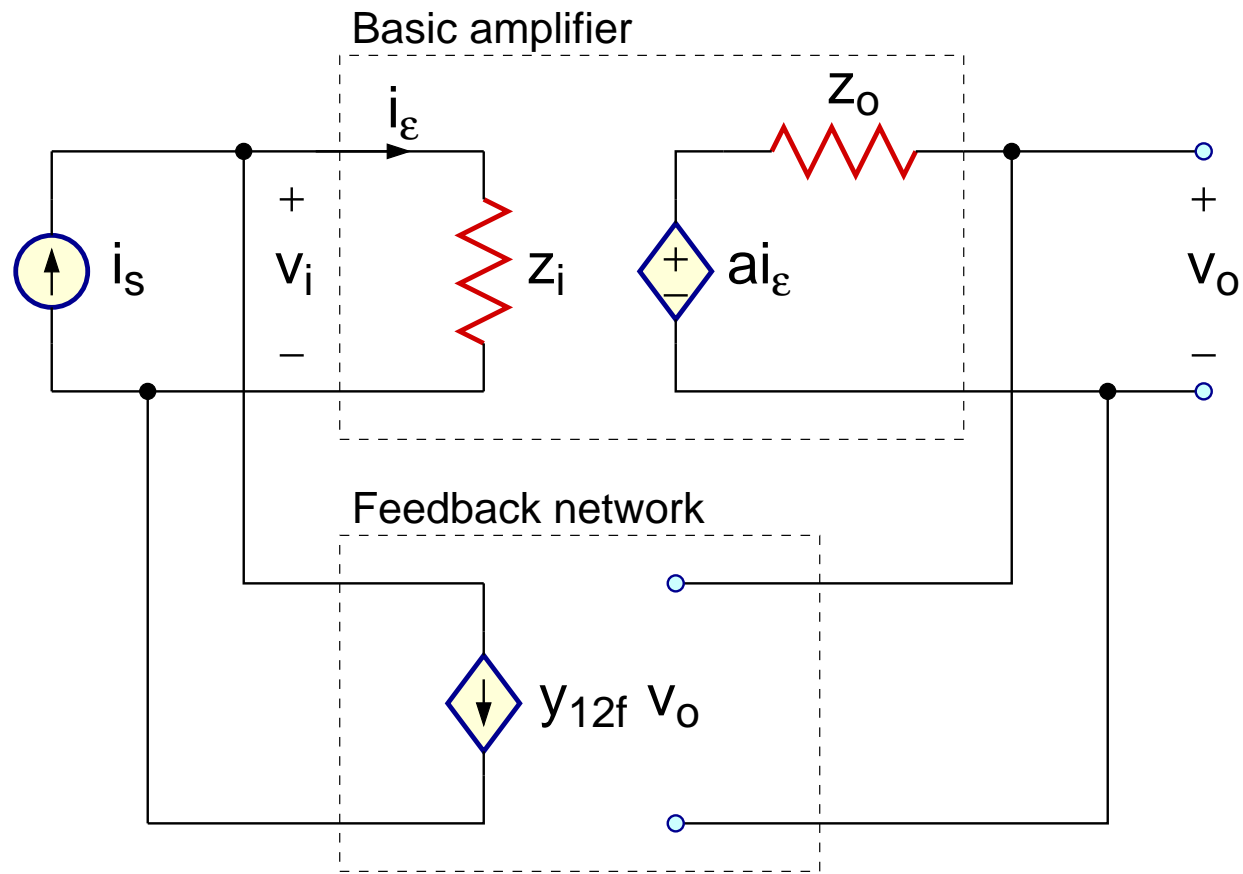


$$y_i = y_s + y_{11a} + y_{11f}$$

$$y_o = y_L + y_{22a} + y_{22f}$$

# Shunt-Shunt

y-parameter representation - simplified



$$a = -\frac{y_{21a}}{y_i y_o}$$

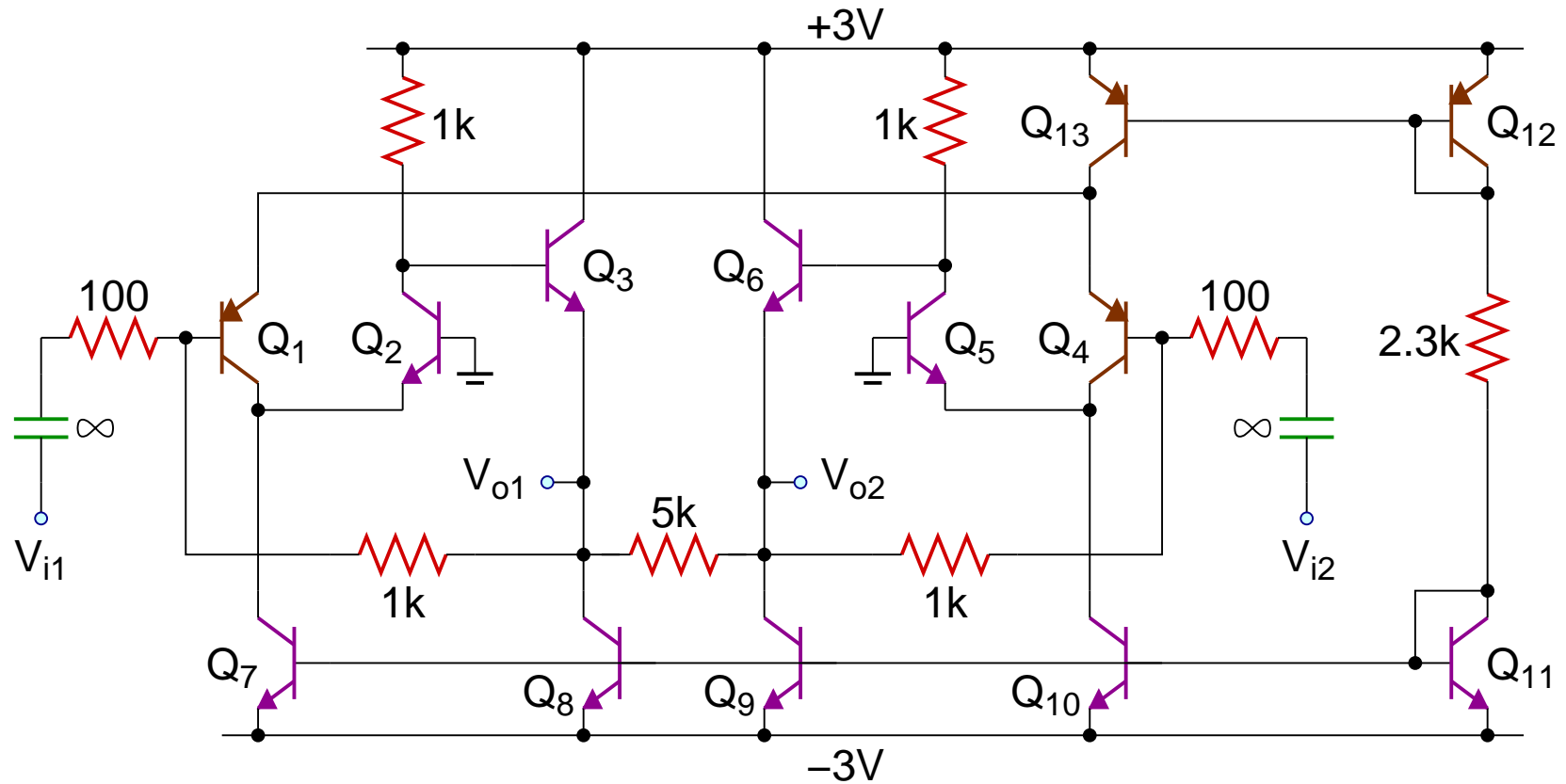
$$f = y_{12f}$$

$$z_i = \frac{1}{y_i}$$

$$z_o = \frac{1}{y_o}$$

# Shunt-Shunt

## Example

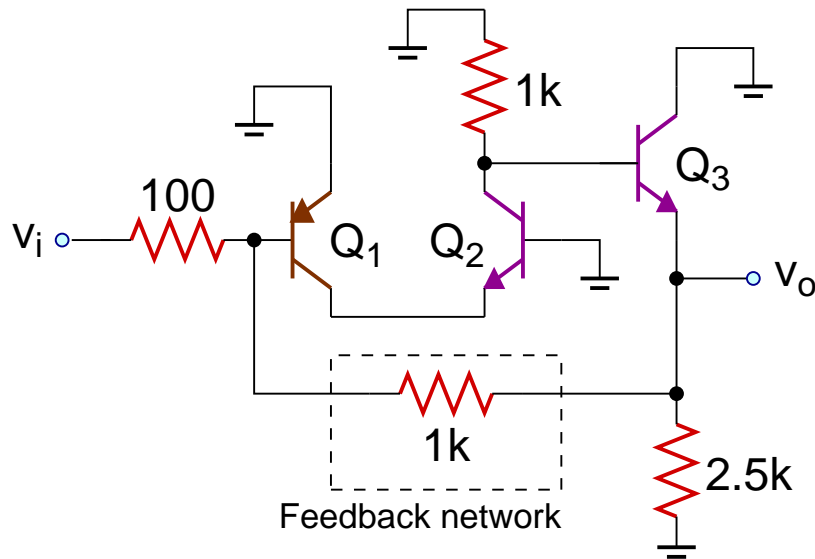


$$V_{i1,dc} = V_{i2,dc} = 0, \quad V_A = \infty, \quad V_T = 25\text{mV}, \quad \beta = 100$$

# Shunt-Shunt

## Example

Differential-mode AC half circuit:



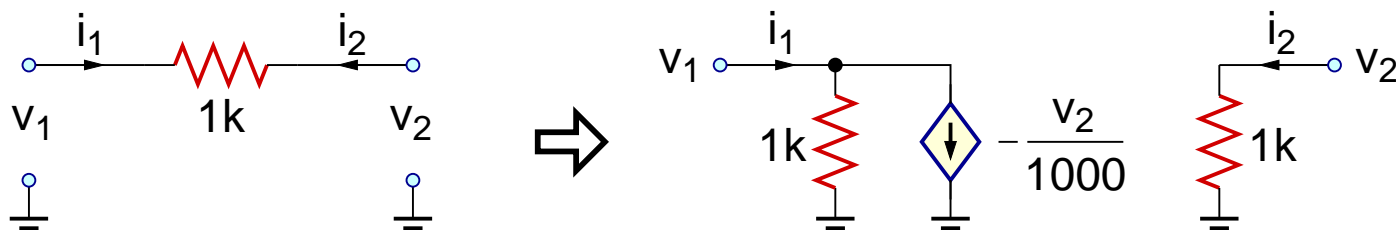
Input: Current  
Output: Voltage

$$I_{C1} = 1 \text{ mA}$$

$$I_{C2} = 1 \text{ mA}$$

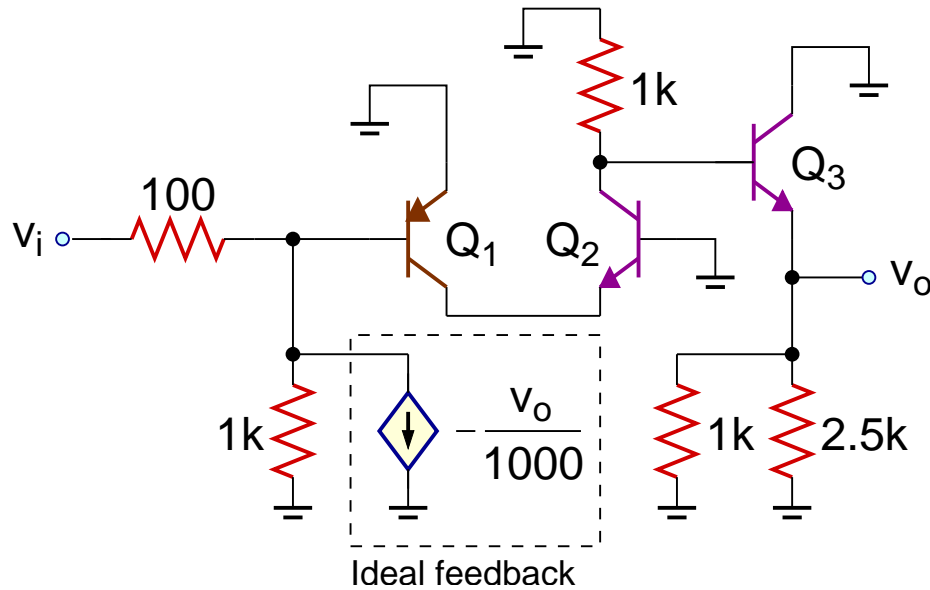
$$I_{C3} = 2 \text{ mA}$$

y-parameter representation of the feedback network:

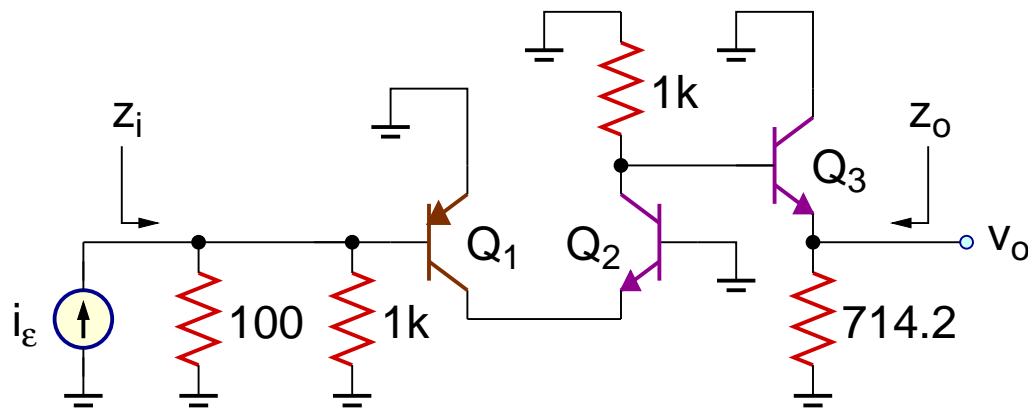


# Shunt-Shunt

## Example



$$f = -0.001$$



$$a = \frac{V_o}{i_\epsilon} = -3403$$

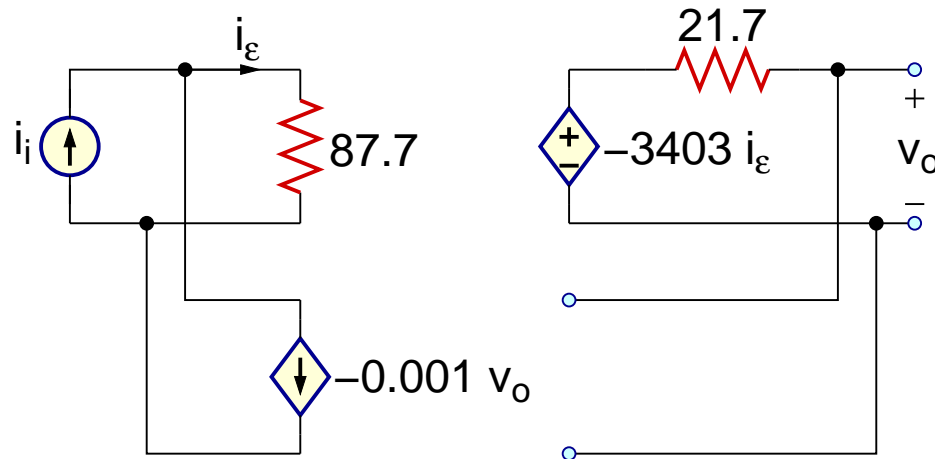
$$z_i = 87.7 \Omega$$

$$z_o = 21.7 \Omega$$



# Shunt-Shunt

## Example



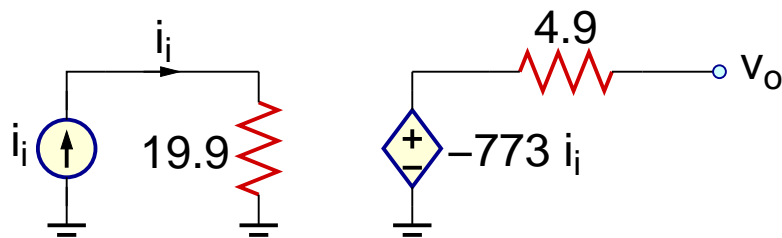
$$i_i = \frac{v_i}{100}$$

$$a = -3403$$

$$f = -0.001$$

$$z_i = 87.7 \Omega$$

$$z_o = 21.7 \Omega$$



$$A = \frac{v_o}{i_i} = \frac{a}{1+af} = -773$$

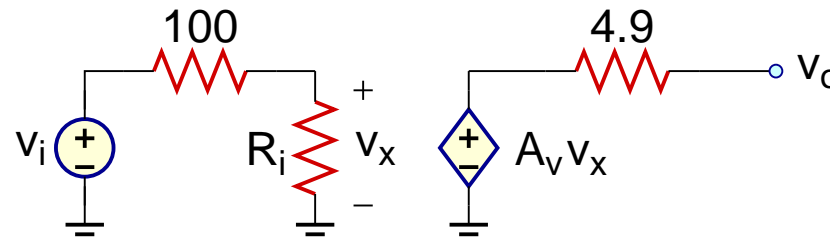
$$Z_i = \frac{z_i}{1+af} = 19.9 \Omega$$

$$Z_o = \frac{z_o}{1+af} = 4.9 \Omega$$

# Shunt-Shunt

## Example

Voltage-mode equivalent circuit:



$$100 \parallel R_i = Z_i \Rightarrow \frac{1}{100} + \frac{1}{R_i} = \frac{1}{Z_i} \Rightarrow R_i = 24.8 \Omega$$

$$i_i = \frac{v_i}{100}, v_o = -773i_i \Rightarrow \frac{v_o}{v_i} = -7.73$$

$$v_o = -7.73v_i = A_v \frac{R_i}{R_i + 100} v_i \Rightarrow A_v = -38.9$$

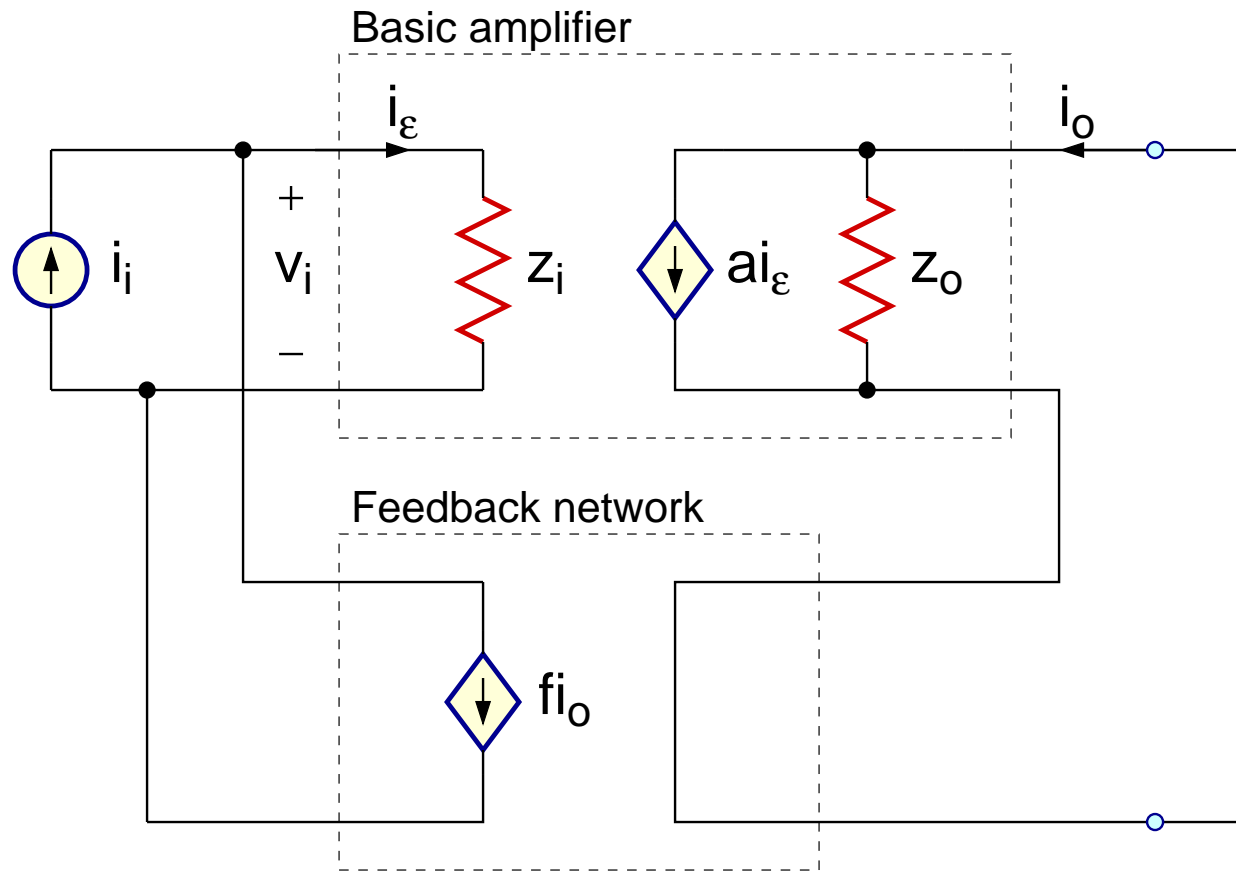
$$A_{dm} = -7.73$$

$$R_{id} = 2 \times (100 + 24.8) = 249.6 \Omega$$

$$R_{od} = 2 \times 4.9 = 9.8 \Omega$$

# Shunt-Series

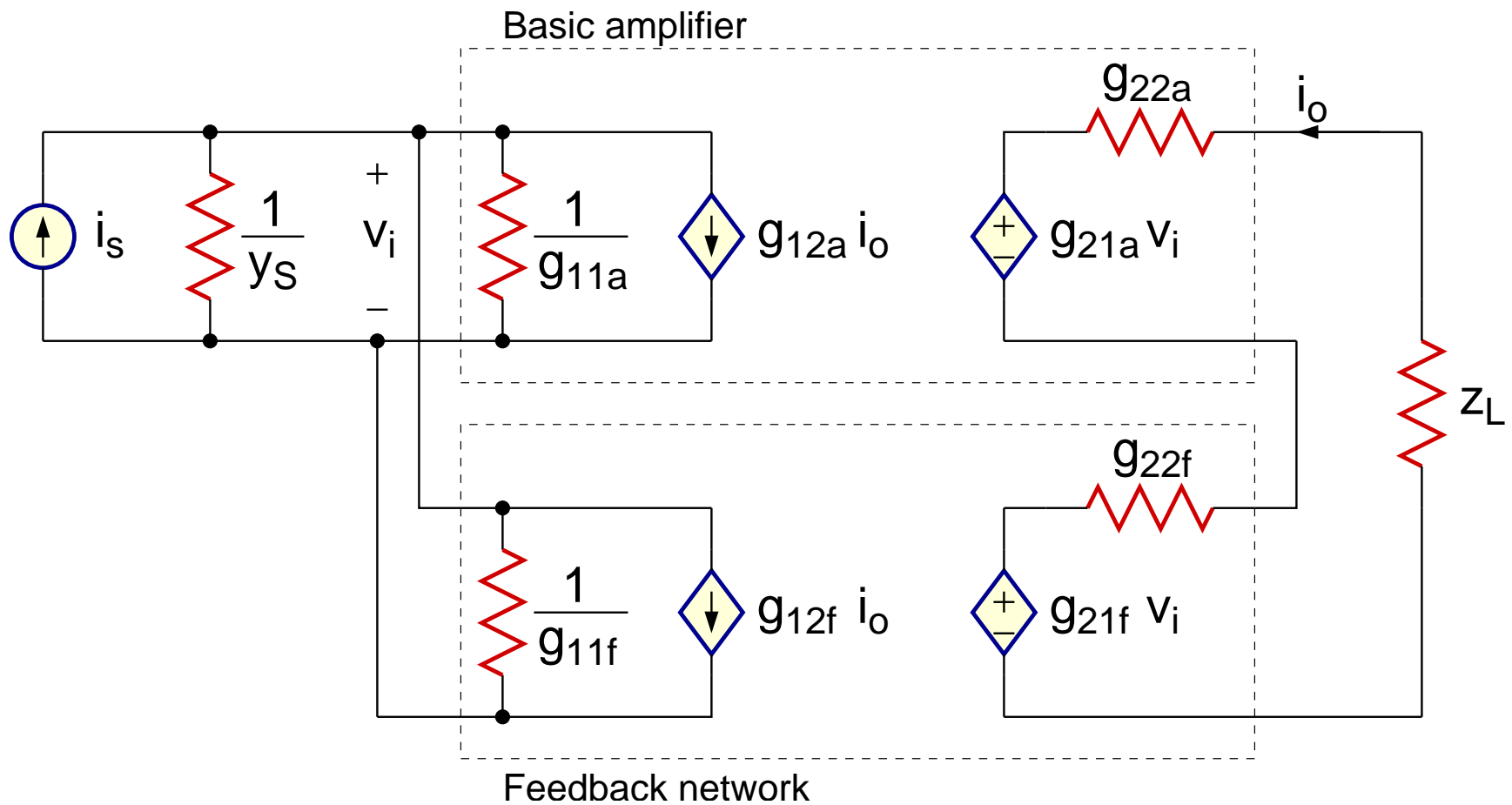
Ideal



$$\frac{i_o}{i_i} = \frac{a}{1 + af} \quad Z_i = \frac{z_i}{1 + af} \quad Z_o = z_o(1 + af)$$

# Shunt-Series

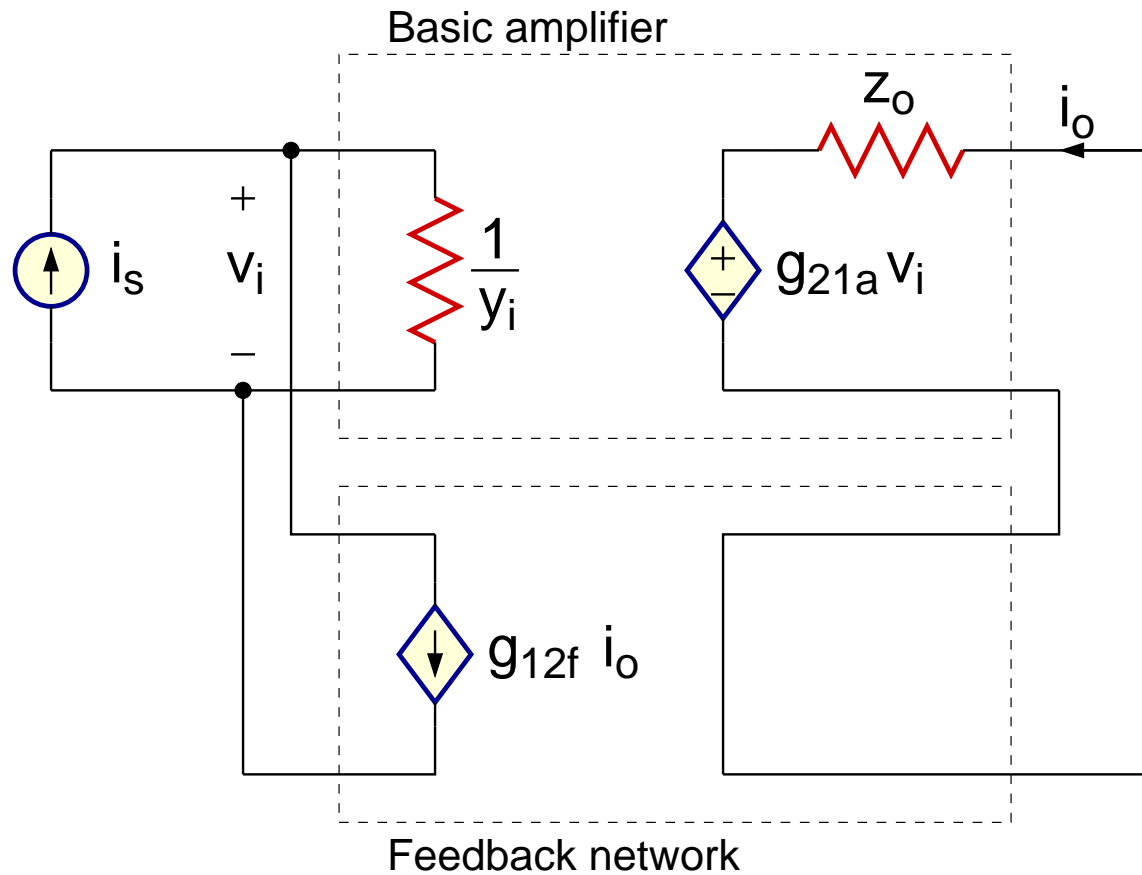
g-parameter representation



$$|g_{12f}| \gg |g_{12a}| \quad |g_{21a}| \gg |g_{21f}|$$

# Shunt-Series

g-parameter representation - simplified

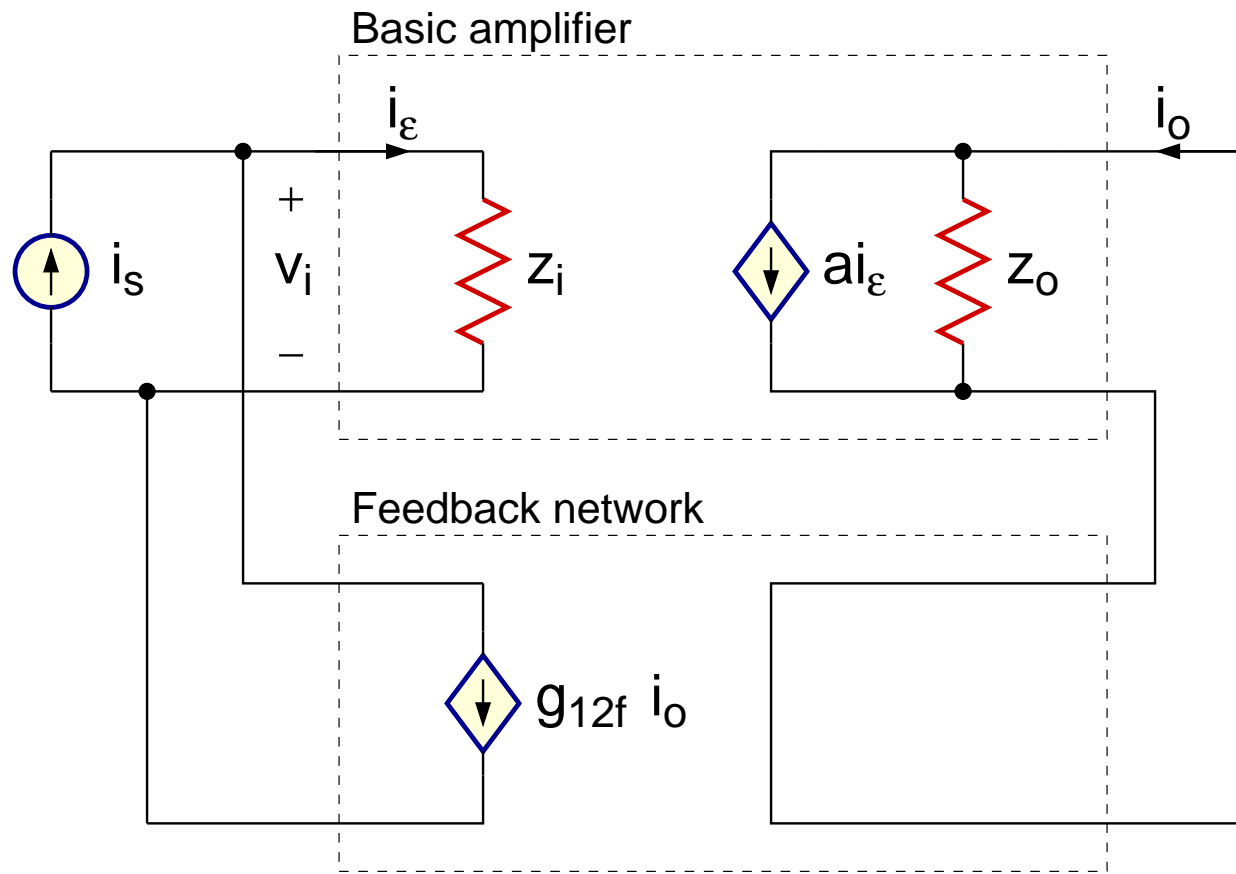


$$y_i = y_s + g_{11a} + g_{11f}$$

$$z_o = z_L + g_{22a} + g_{22f}$$

# Shunt-Series

g-parameter representation - simplified



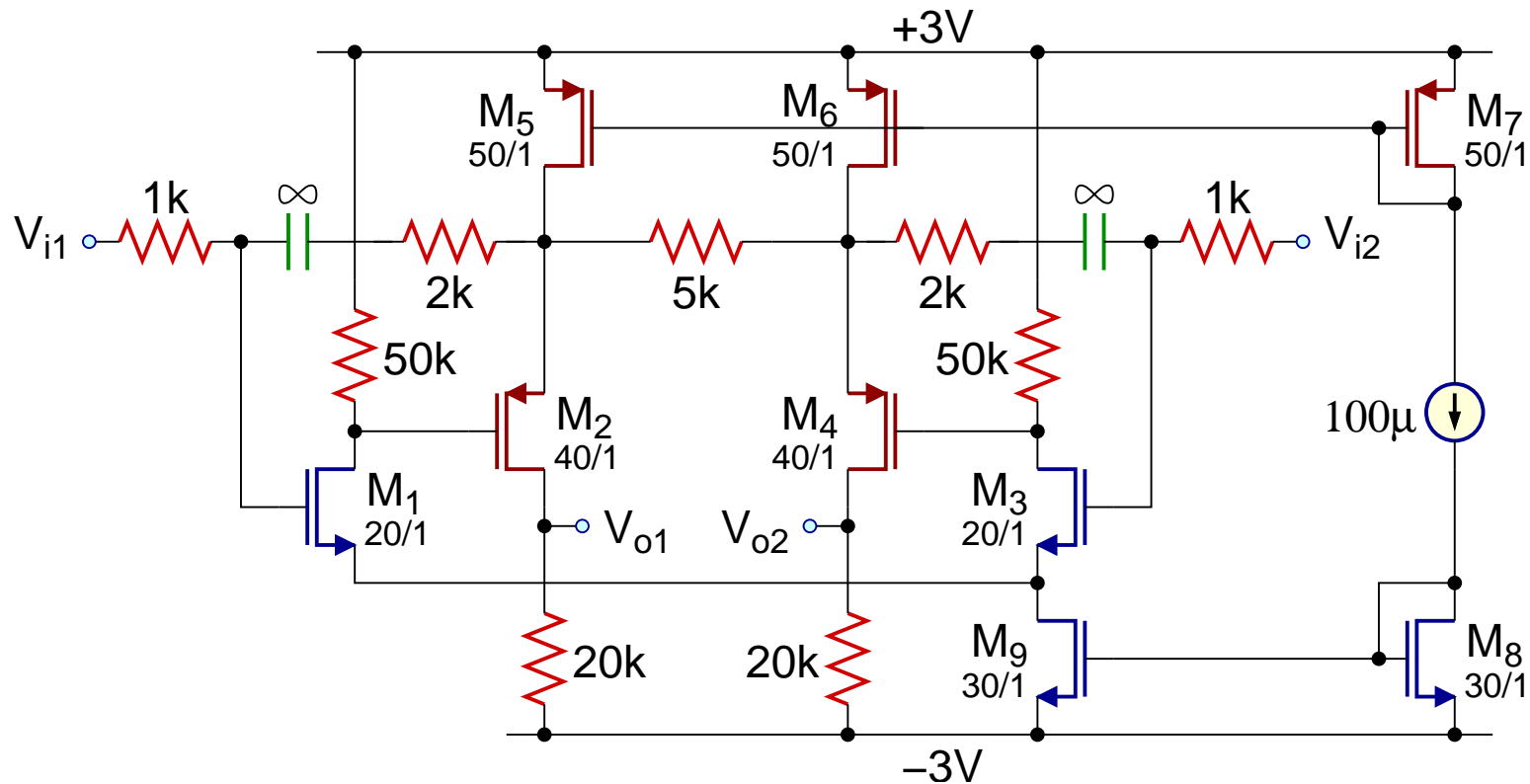
$$a = -\frac{g_{21a}}{y_i z_o}$$

$$f = g_{12f}$$

$$z_i = \frac{1}{y_i}$$

# Shunt-Series

## Example



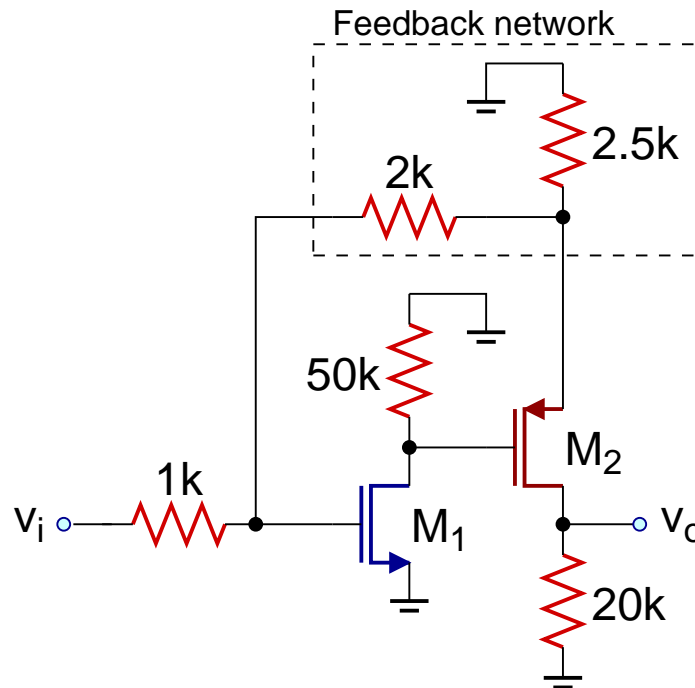
$$k'_n = 190 \mu\text{A}/\text{V}^2, \quad k'_p = 110 \mu\text{A}/\text{V}^2, \quad \lambda_n = \lambda_p = 0$$

$$V_{tn} = 1.5 \text{ V}, \quad V_{tp} = -1.6 \text{ V}, \quad \chi = 0$$

# Shunt-Series

## Example

Differential-mode AC half circuit:

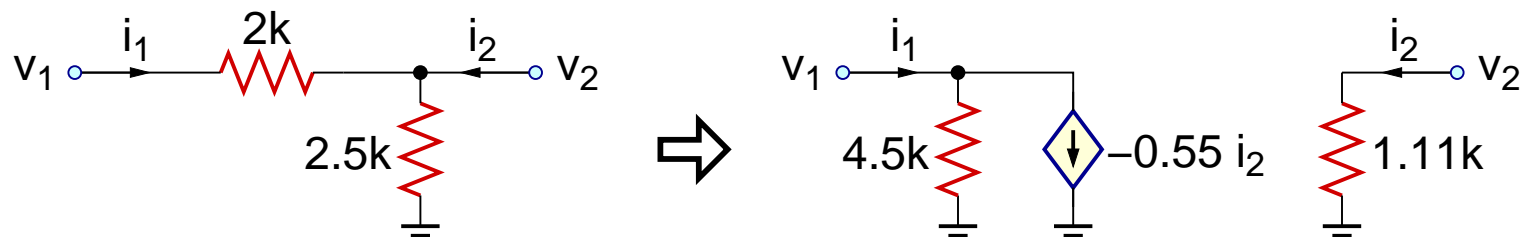


Input: Current  
Output: Current

$$I_{D1} = 50 \mu\text{A}$$

$$I_{D2} = 100 \mu\text{A}$$

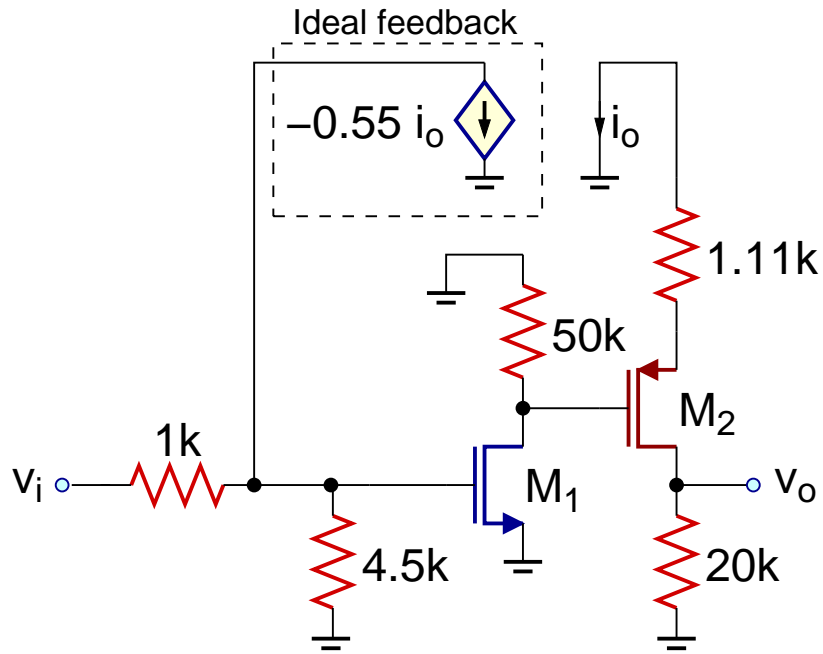
g-parameter representation of the feedback network:



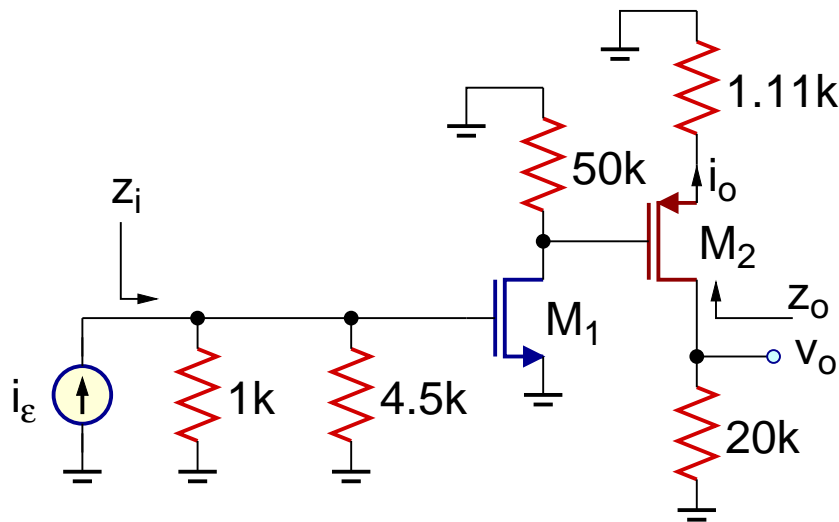


# Shunt-Series

## Example



$$f = -0.55$$



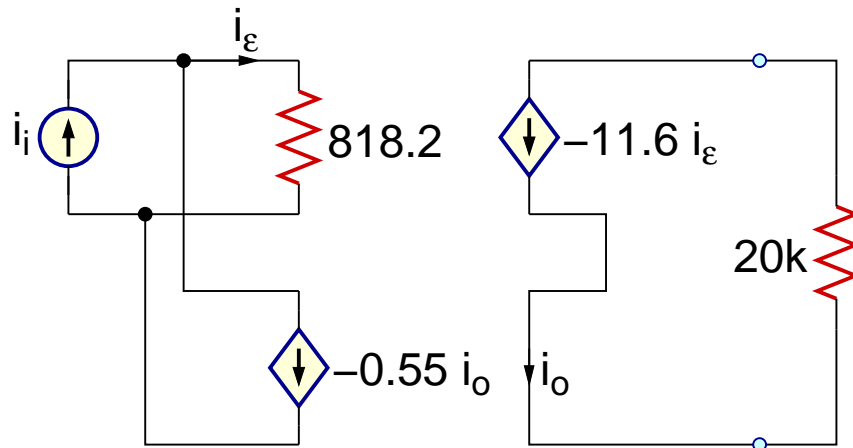
$$a = \frac{i_o}{i_\epsilon} = -11.6$$

$$z_i = 818.2 \Omega$$

$$z_o = \infty$$

# Shunt-Series

Example



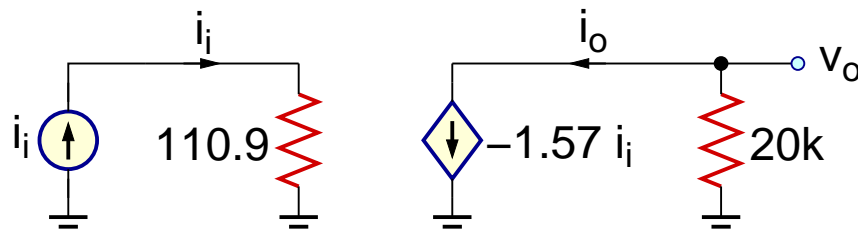
$$i_i = \frac{v_i}{1k}$$

$$a = -11.6$$

$$f = -0.55$$

$$z_i = 818.2 \Omega$$

$$z_o = \infty$$



$$A = \frac{i_o}{i_i} = \frac{a}{1 + af} = -1.57$$

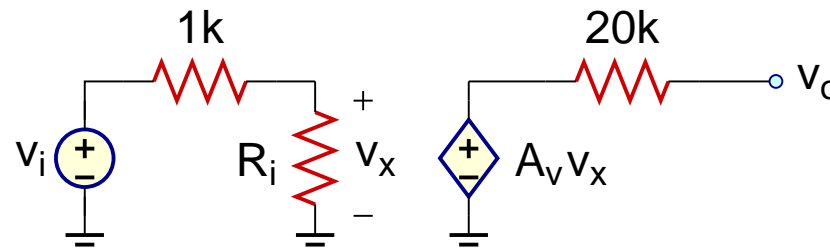
$$Z_i = \frac{z_i}{1 + af} = 110.9 \Omega$$

$$Z_o = \infty$$

# Shunt-Series

## Example

Voltage-mode equivalent circuit:



$$1\text{k} \parallel R_i = Z_i \Rightarrow \frac{1}{1\text{k}} + \frac{1}{R_i} = \frac{1}{Z_i} \Rightarrow R_i = 124.7 \Omega$$

$$i_i = \frac{v_i}{1\text{k}}, v_o = -(20\text{k})(-1.57i_i) \Rightarrow \frac{v_o}{v_i} = 31.4$$

$$v_o = 31.4v_i = A_v \frac{R_i}{R_i + 1\text{k}} v_i \Rightarrow A_v = 283.2$$

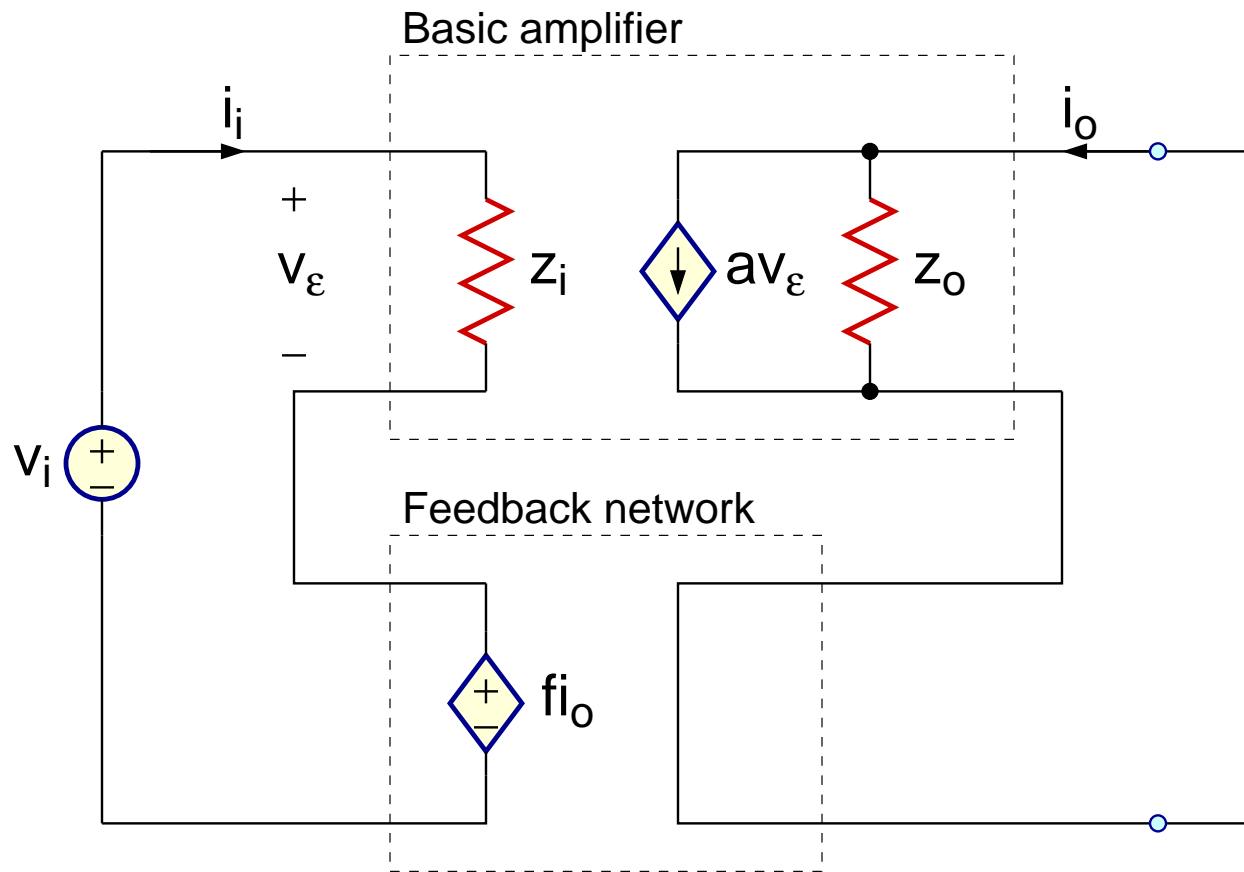
$$A_{dm} = 31.4$$

$$R_{id} = 2 \times (1\text{k} + 124.7) = 2.25 \text{ k}\Omega$$

$$R_{od} = 2 \times 20\text{k} = 40 \text{ k}\Omega$$

# Series-Series

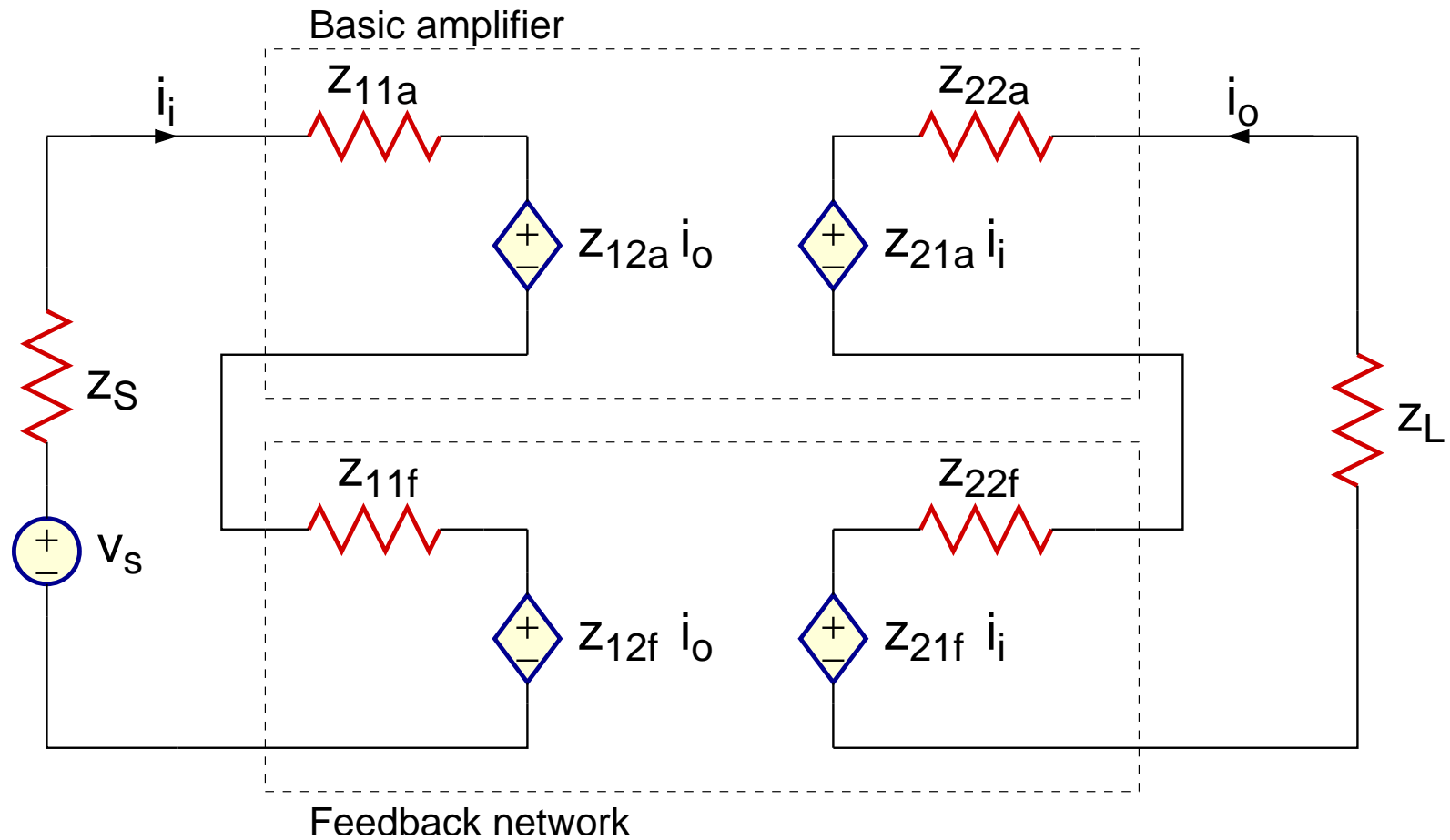
Ideal



$$\frac{i_o}{v_i} = \frac{a}{1 + af} \quad Z_i = z_i(1 + af) \quad Z_o = z_o(1 + af)$$

# Series-Series

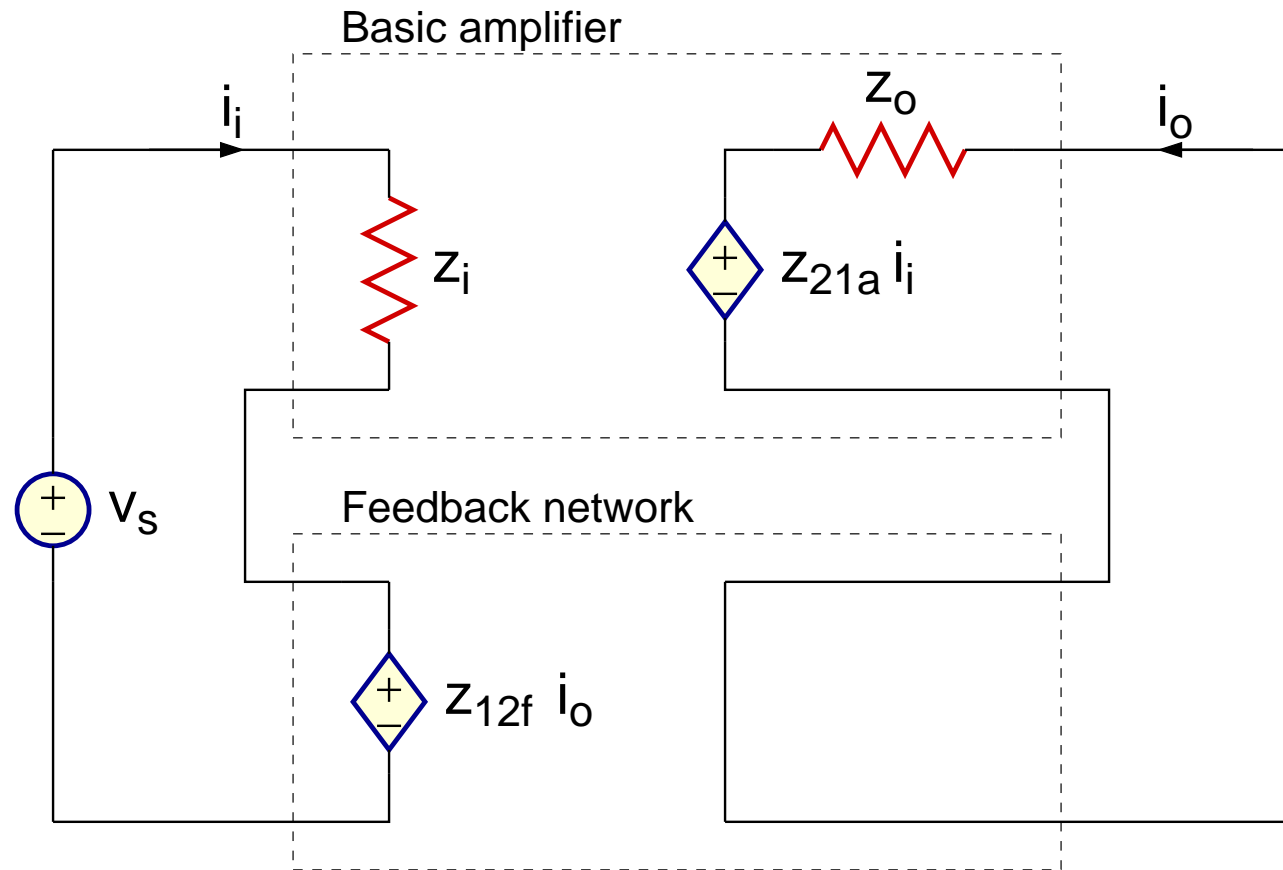
z-parameter representation



$$|z_{12f}| \gg |z_{12a}| \quad |z_{21a}| \gg |z_{21f}|$$

# Series-Series

z-parameter representation - simplified

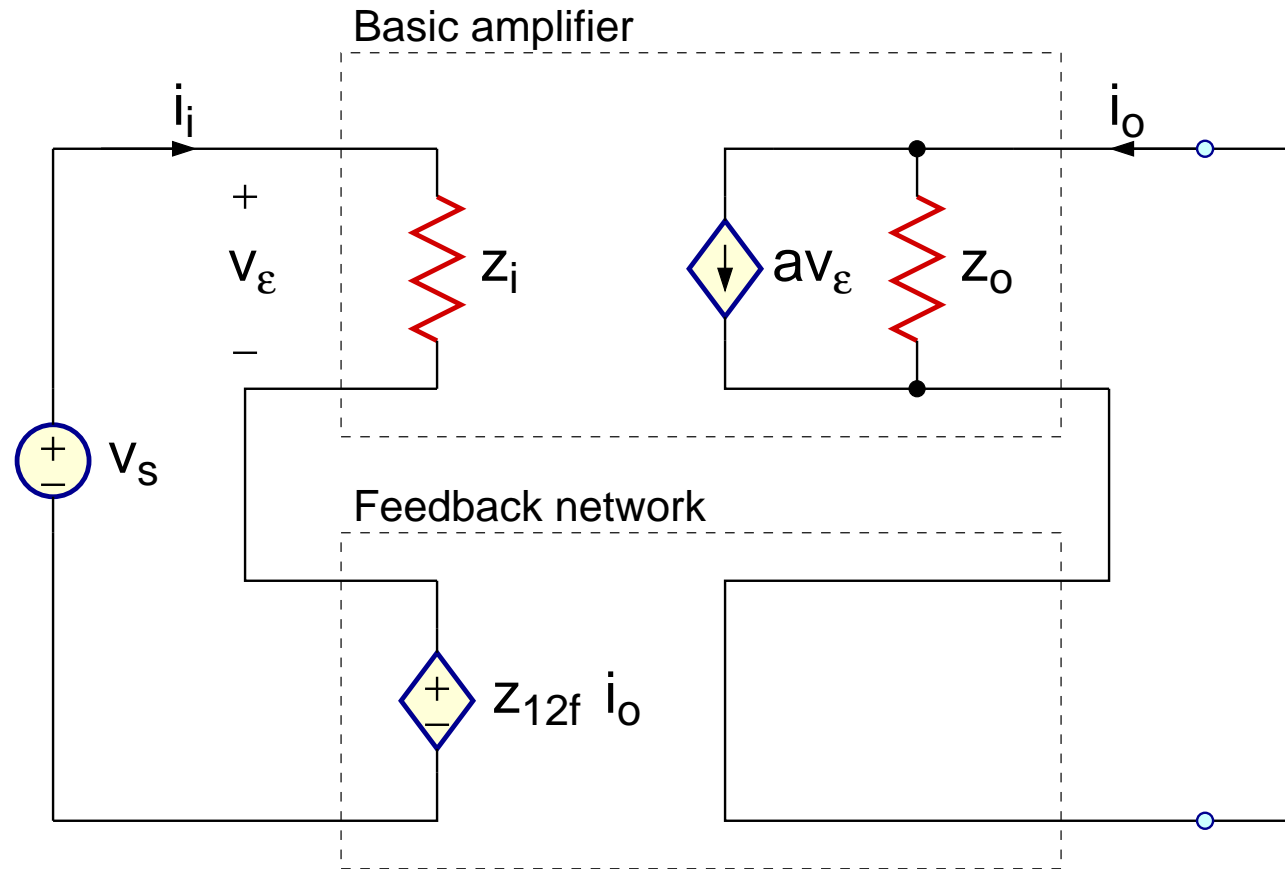


$$z_i = y_S + z_{11a} + z_{11f}$$

$$z_o = z_L + z_{22a} + z_{22f}$$

# Series-Series

z-parameter representation - simplified

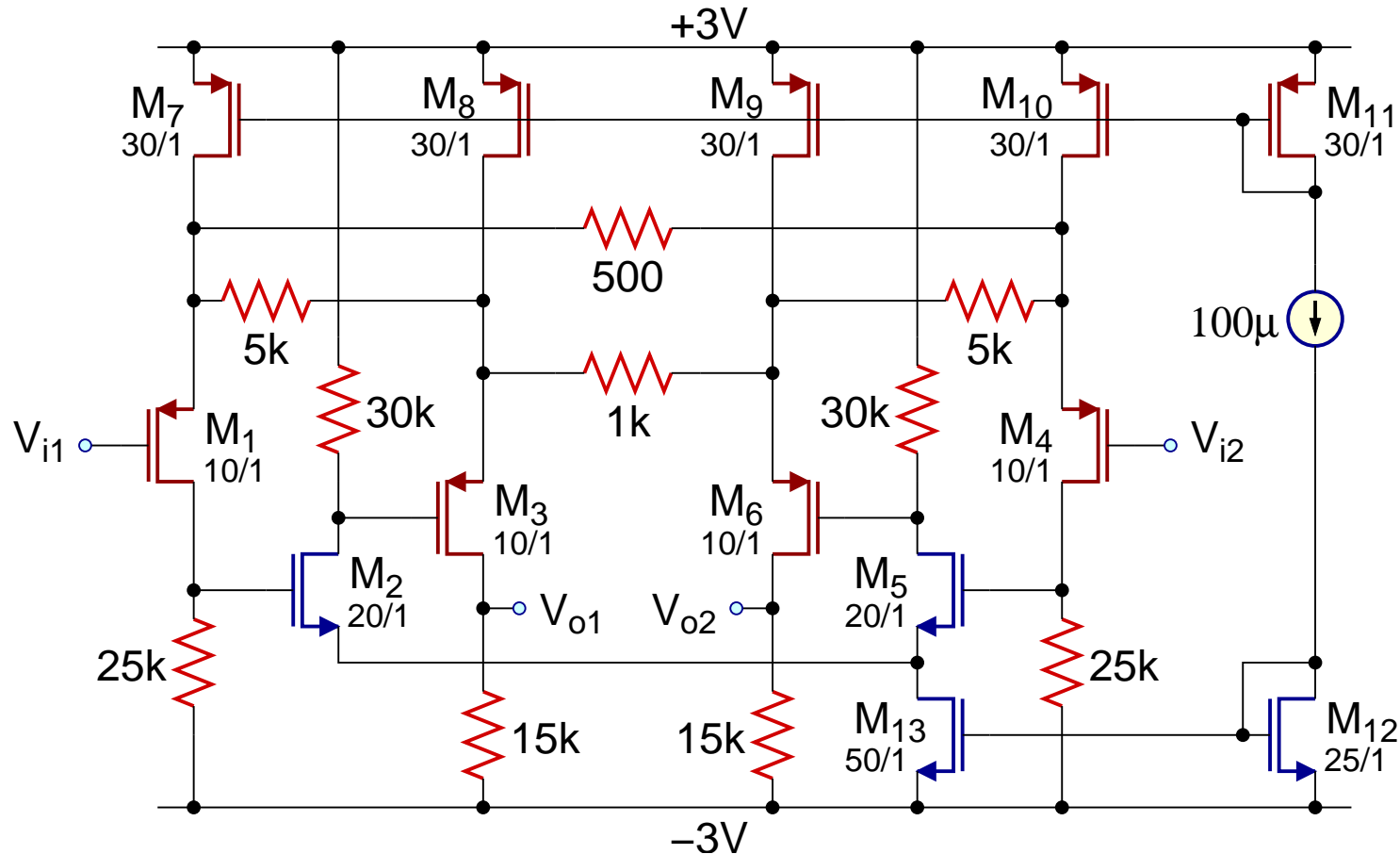


$$a = -\frac{Z_{21a}}{Z_i Z_o}$$

$$f = z_{12f}$$

# Series-Series

## Example



$$\kappa'_n = 190 \mu\text{A}/\text{V}^2, \kappa'_p = 110 \mu\text{A}/\text{V}^2, \lambda_n = \lambda_p = 0$$

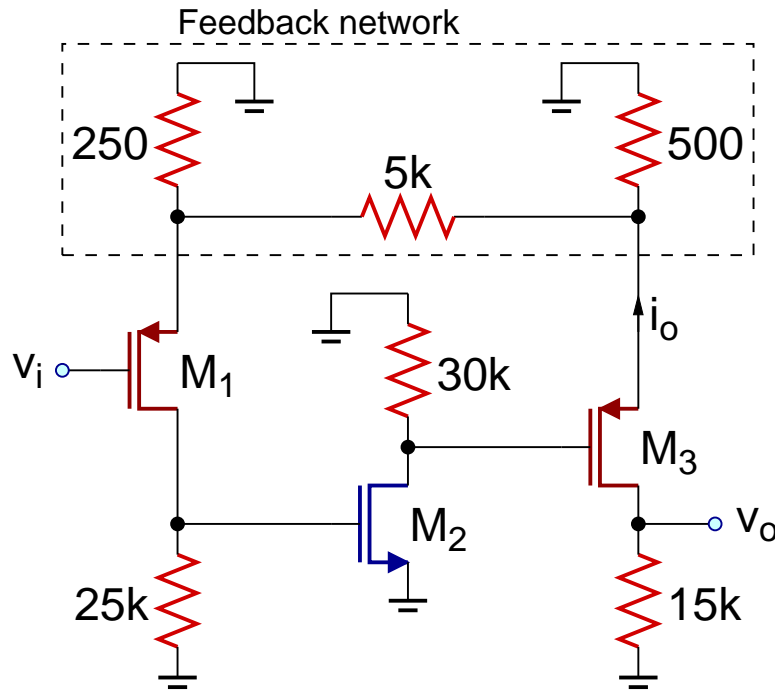
$$V_{tn} = 1.5 \text{ V}, V_{tp} = -1.6 \text{ V}, \chi = 0$$



# Series-Series

## Example

Differential-mode AC half circuit:



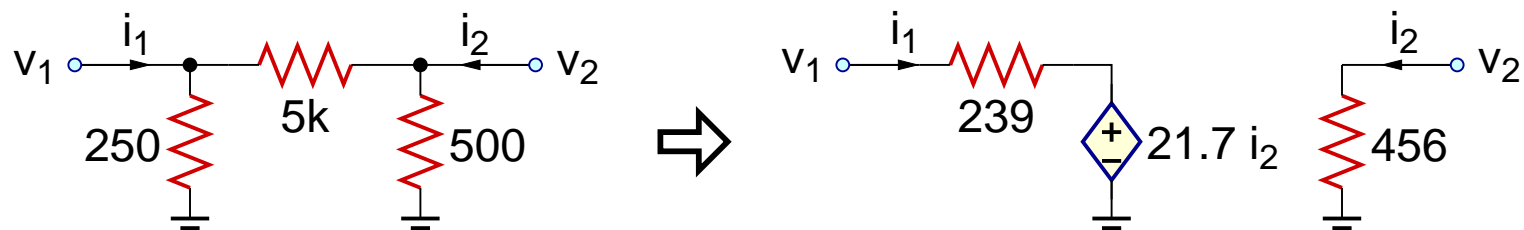
Input: Voltage  
Output: Current

$$I_{D1} = 100 \mu\text{A}$$

$$I_{D2} = 100 \mu\text{A}$$

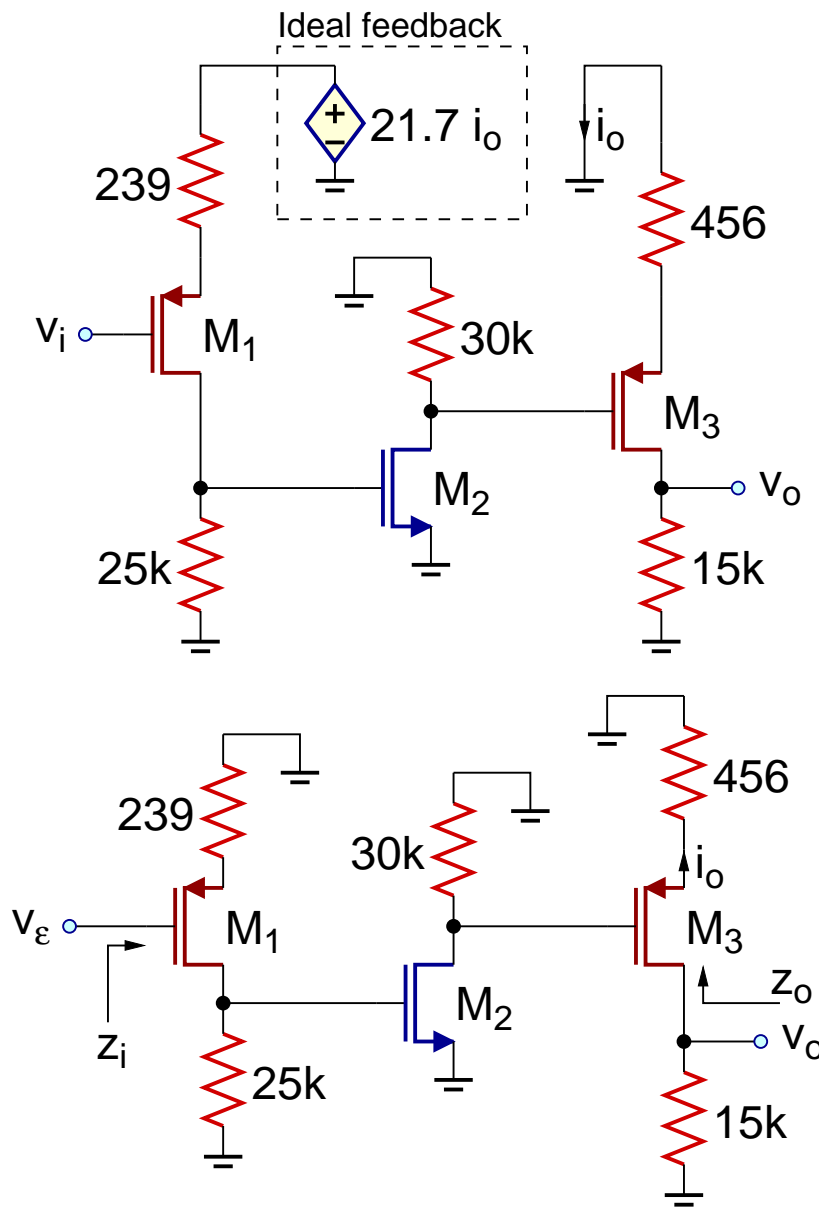
$$I_{D3} = 100 \mu\text{A}$$

z-parameter representation of the feedback network:



# Series-Series

## Example



$$f = 21.7$$

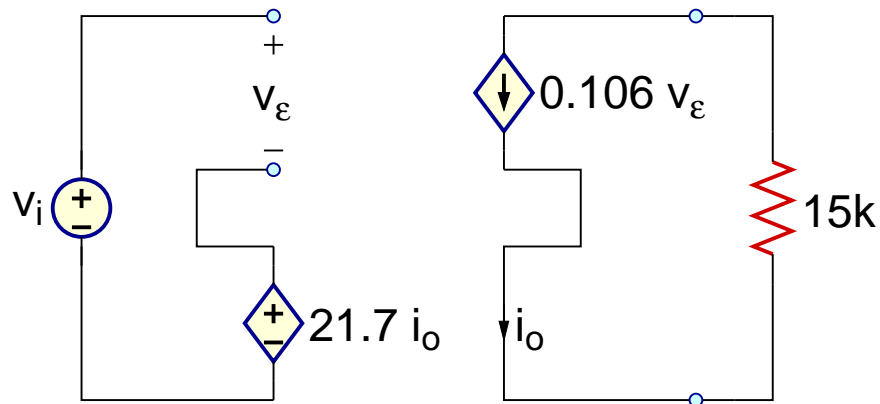
$$a = \frac{i_o}{V_\epsilon} = 0.106$$

$$Z_i = \infty$$

$$Z_o = \infty$$

# Series-Series

Example

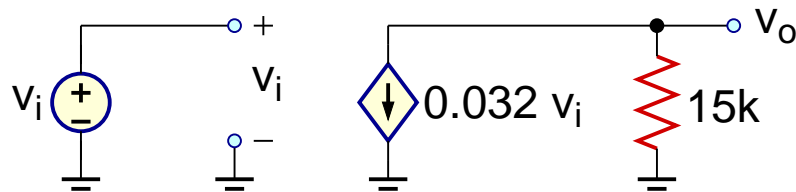


$$a = 0.106$$

$$f = 21.7$$

$$Z_i = \infty$$

$$Z_o = \infty$$

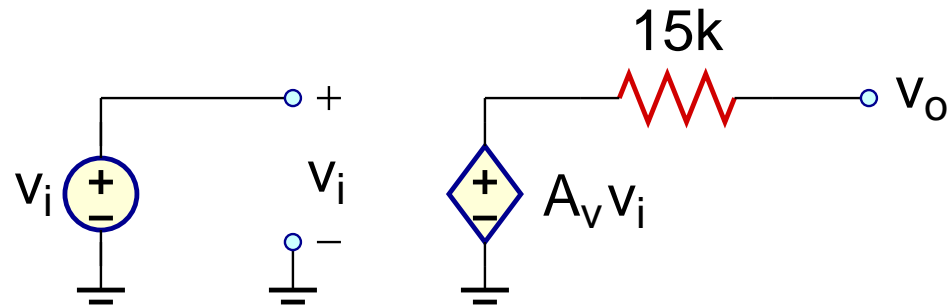


$$A = \frac{i_o}{v_i} = \frac{a}{1 + af} = 0.032$$

$$Z_i = \infty$$

$$Z_o = \infty$$

Voltage-mode equivalent circuit:



$$v_o = -(15k)(0.032v_i) = A_v v_i \Rightarrow A_v = -480$$

$$A_{dm} = -480$$

$$R_{id} = \infty$$

$$R_{od} = 2 \times 15k = 30 \text{ k}\Omega$$