

Texas A&M University
Department of Electrical and Computer Engineering

ECEN 326 – Electronic Circuits

Fall 2017

Exam #3

Instructor: Sam Palermo

- Please write your name in the space provided below
- Please verify that there are 6 pages in your exam
- You may use one double-sided page of notes and equations for the exam
- Good Luck!

Problem	Score	Max Score
1		35
2		35
3		30
Total		100

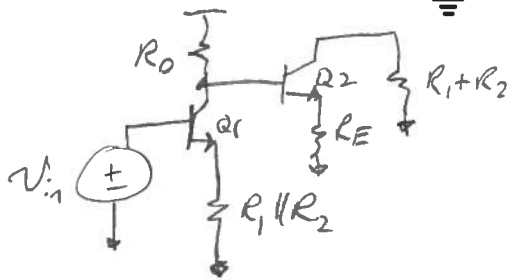
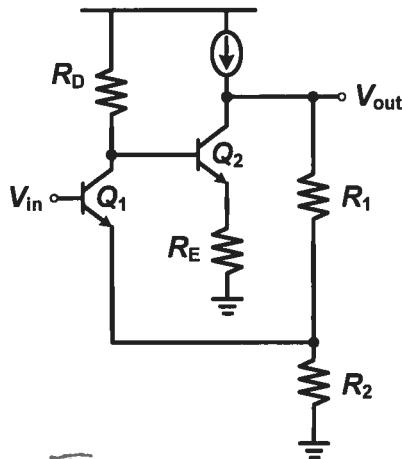
Name: SAM PALERMO

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Problem 1 (35 points)

For the circuit shown below, assume that all transistors are operating in the active region and that $V_A = \infty$.

- What type of feedback is present in the circuit?
- Give expressions for the **open-loop** gain (V_{out}/V_{in}), input resistance, and output resistance. Make sure to include feedback loading effects.
- What is the feedback factor, K ?
- Give expressions for the **closed-loop** gain (V_{out}/V_{in}), input resistance, and output resistance.



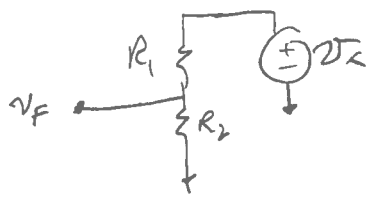
a. Voltage - Voltage Feedback
 (Sensing) (Return) or Series - Shunt+
 (FB) (Sensing)

b. Breaking Loop

$$A_{OL} = \left(\frac{-\alpha (R_D \parallel (r_{\pi 2} + (\beta + 1)R_E))}{r_{e1} + R_1 \parallel R_2} \right) \left(\frac{-\alpha (R_1 + R_2)}{r_{e2} + R_E} \right)$$

$$\approx \left(\frac{g_{m1} (R_D \parallel (r_{\pi 2} + (\beta + 1)R_E))}{1 + g_{m1} (R_1 \parallel R_2)} \right) \left(\frac{g_{m2} (R_1 + R_2)}{1 + g_{m2} R_E} \right)$$

For K :



$$R_{in,OL} = r_{\pi 1} + (\beta + 1)(R_1 \parallel R_2)$$

$$R_{out,OL} = R_1 + R_2$$

$$K = \frac{R_2}{R_1 + R_2}$$

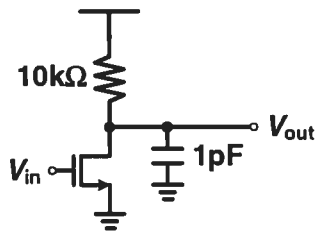
d.
$$A_{CL} = \frac{A_{OL}}{1 + KA_{OL}}$$

$$R_{in,CL} = R_{in,OL} (1 + KA_{OL})$$

$$R_{out,CL} = \frac{R_{out,OL}}{1 + KA_{OL}}$$

Problem 2 (35 points)

- a. Give the transfer function (**w/ numbers**) of the single-stage amplifier shown below. Assume the transistor operates in saturation with $g_m=1\text{mA/V}$ and $\lambda=0$. Only consider the explicitly drawn capacitors, i.e. no transistor capacitors.

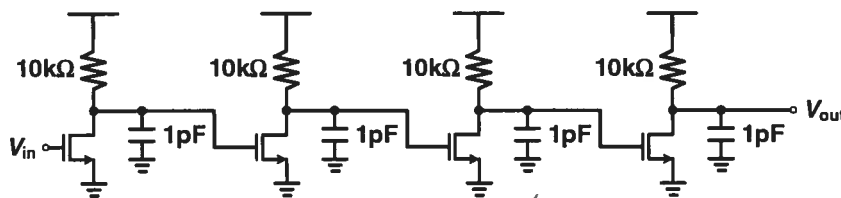


$$A_{DC} = -g_m R_D = -(1\text{mA/V})(10\text{k}\Omega) = -10\text{V/V}$$

$$|\omega_p| = \frac{1}{R_D C} = \frac{1}{(10\text{k}\Omega)(1\text{pF})} = 100\text{Mrad/s}$$

$$H_1(s) = \frac{V_{out}(s)}{V_{in}(s)} = \frac{-10}{1 + \frac{s}{10^8}}$$

- b. Now this single-stage amplifier is used in a 4-stage amplifier. Again, assume all transistors operate in saturation with $g_m=1\text{mA/V}$ and $\lambda=0$ and only consider the explicitly drawn capacitors, i.e. no transistor capacitors. Give the 4-stage amplifier transfer function and the frequency at which the amplifier's phase equals -180° (ω_{PX}).



$$H(s) = (H_1(s))^4 = \frac{10^4}{\left(1 + \frac{s}{10^8}\right)^4}$$

$$\tan^{-1}\left(\frac{\omega_{PX}}{10^8}\right) = 45^\circ$$

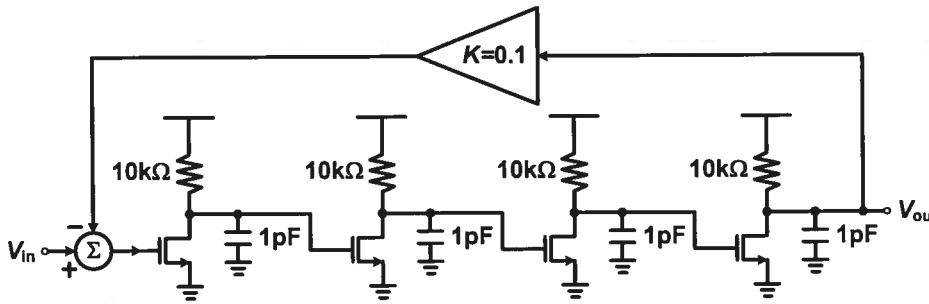
$$\omega_{PX} = 10^8 \text{ rad/s}$$

$$\angle H(j\omega) = -4 \tan^{-1}\left(\frac{\omega_{PX}}{10^8}\right) = -180^\circ$$

$$H(s) = \frac{V_{out}(s)}{V_{in}(s)} = \frac{10^4}{\left(1 + \frac{s}{10^8}\right)^4}$$

$$\omega_{PX} = 100\text{Mrad/s}$$

- c. Now this 4-stage amplifier is placed in feedback with $K=0.1$. Give the frequency at which the feedback system $|KH(s)|=1$ (ω_{GX}). Is the system stable?



$$|KH(s)| = 1$$

$$\frac{(0.1)(10^4)}{\left(1 + \frac{\omega_{GX}^2}{10^{16}}\right)^4} = 1$$

$$\left(1 + \frac{\omega_{GX}^2}{10^{16}}\right)^2 = 10^3$$

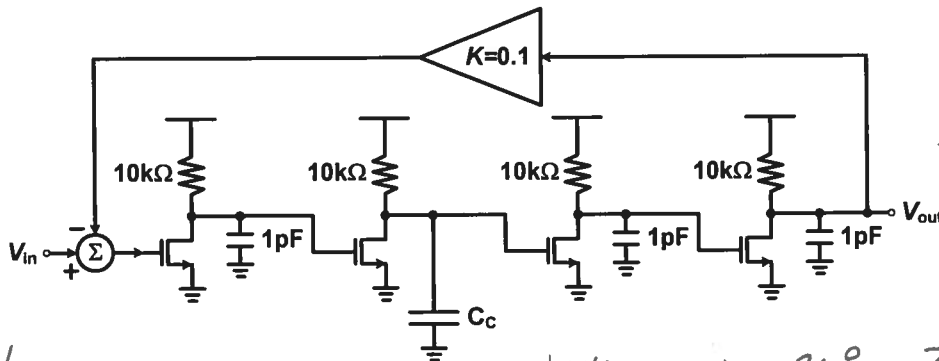
$$1 + \frac{\omega_{GX}^2}{10^{16}} = 10^{1.5}$$

$$\omega_{GX} = 10^8 \sqrt{10^{1.5} - 1} = 553M$$

$$\omega_{GX} = 553M \text{ rad/s}$$

System Stable? (Yes or No) *No* ($\omega_{GX} > \omega_{PX}$)

- d. Now only the second stage is modified with a large compensation capacitor C_C to establish a single dominant pole system. Assume that this dominant pole contributes -90° at the new ω_{GX} . Considering the other poles in the system, what is the capacitor value necessary for the feedback system (KH) to have a phase margin of 45° ?



For $PM = 45^\circ$

$$\angle KH(j\omega_{GX_{new}}) = -135^\circ$$

w/ one dominant pole $\angle KH(j\omega_{GX_{new}}) = -90^\circ - 3 \tan^{-1}\left(\frac{\omega_{GX_{new}}}{10^8}\right) = -135^\circ$

$$\tan^{-1}\left(\frac{\omega_{GX_{new}}}{10^8}\right) = 15^\circ$$

To place $\omega_{GX_{new}}$ at $26.8M \text{ rad/s}$

$$\omega_{P1}' = \frac{\omega_{GX_{new}}}{|KH|} = \frac{26.8M \text{ rad/s}}{10^3} = 26.8K \text{ rad/s}$$

$$\omega_{GX_{new}} = 26.8M \text{ rad/s}$$

$$C_C (PM=45^\circ) = 3.73nF$$

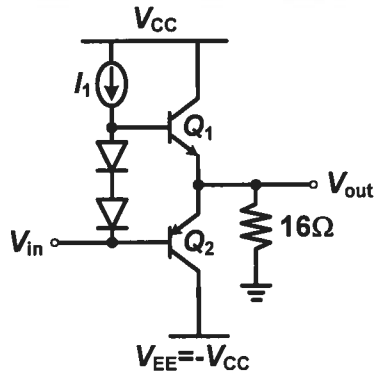
$$\omega_{P1}' = \frac{1}{R_D C_C}$$

$$C_C = \frac{1}{(10k\Omega)(26.8K \text{ rad/s})} = 3.73nF$$

Problem 3 (30 points)

The transistors used in the circuit below have a maximum average power rating of 2W.

a. What is the largest power that the circuit can deliver to a 16Ω load?



The maximum average power of the transistors

$$P_{Q1,max} = \frac{V_{CC}^2}{\pi^2 R_L} \quad \text{with} \quad V_P = \frac{2V_{CC}}{\pi}$$

$$\Rightarrow V_{CC} = \frac{\pi V_P}{2}$$

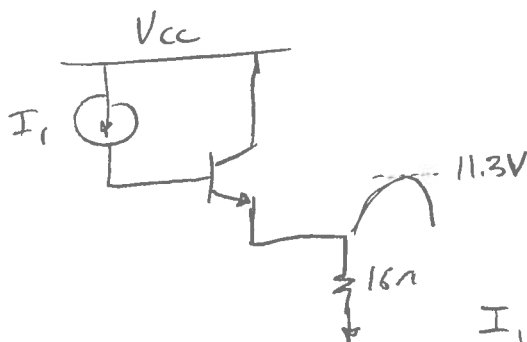
$$P_{Q1,max} = \frac{\left(\frac{\pi V_P}{2}\right)^2}{\pi^2 R_L} \Rightarrow V_P = 2\sqrt{P_{Q1} R_L} = 2\sqrt{2W(16\Omega)} = 11.3V$$

$$P_{RL} = \frac{V_P^2}{2R_L} = 2P_{Q1} = 2(2W) = 4W$$

$$P_{RL,max} = 4W$$

b. When the circuit is delivering this maximum power to the load, determine the necessary I_1 to support the required output swing with minimal distortion. Assume both transistors have $\beta=40$.

Equivalent circuit during positive peak



During the max positive amplitude, I_1 must support the necessary base current.

$$I_1 = \frac{I_E}{\beta+1} = \frac{V_P}{R_L(\beta+1)} = \frac{11.3V}{16(40+1)} = 17.2mA$$

$$I_1 = 17.2mA$$

Scratch Paper