

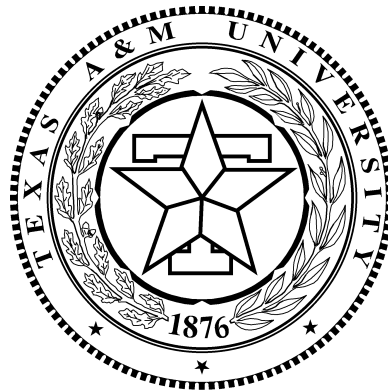
ECEN 325

Electronics

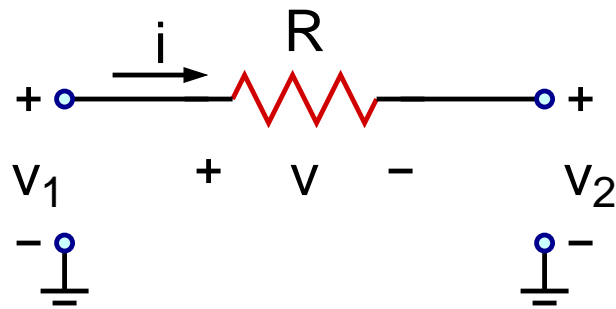
Introduction

Dr. Aydın İlker Karşilayan

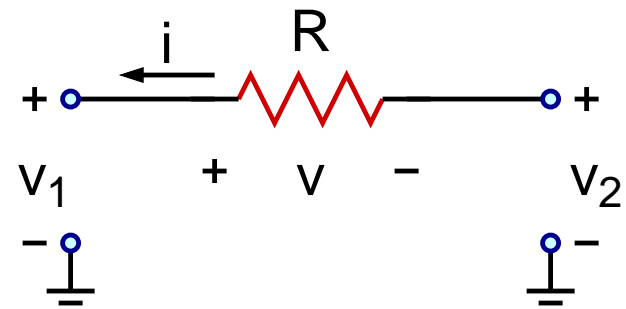
Texas A&M University
Department of Electrical and Computer Engineering



Ohm's Law



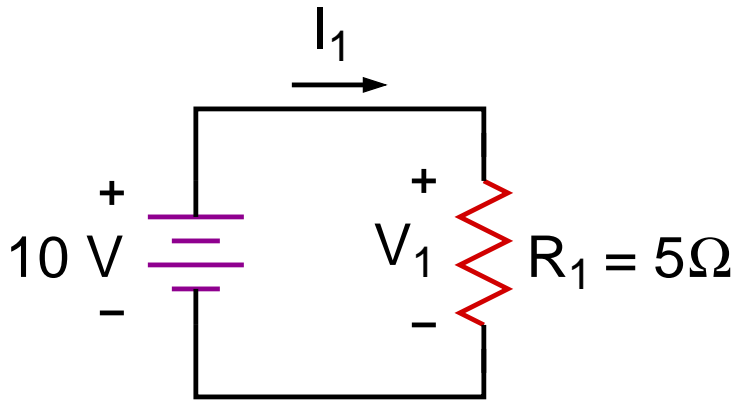
$$\begin{aligned}v &= V_1 - V_2 \\v &= iR \\i &= Gv\end{aligned}$$



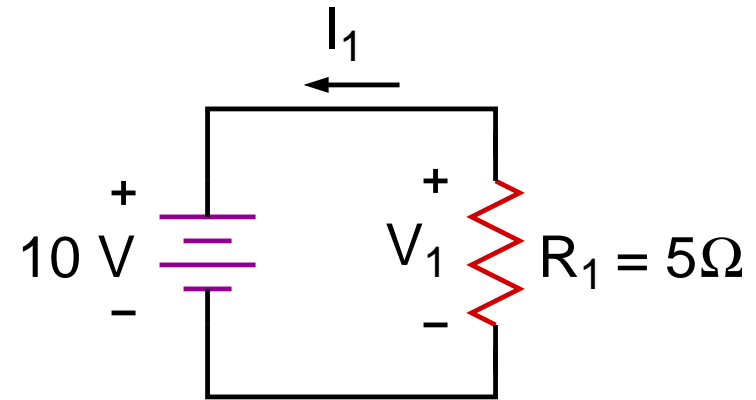
$$\begin{aligned}v &= V_1 - V_2 \\v &= -iR \\i &= -Gv\end{aligned}$$

Ohm's Law

Example



$$V_1 = 10 \text{ V}$$
$$I_1 = 2 \text{ A}$$



$$V_1 = 10 \text{ V}$$
$$I_1 = -2 \text{ A}$$

KVL & KCL

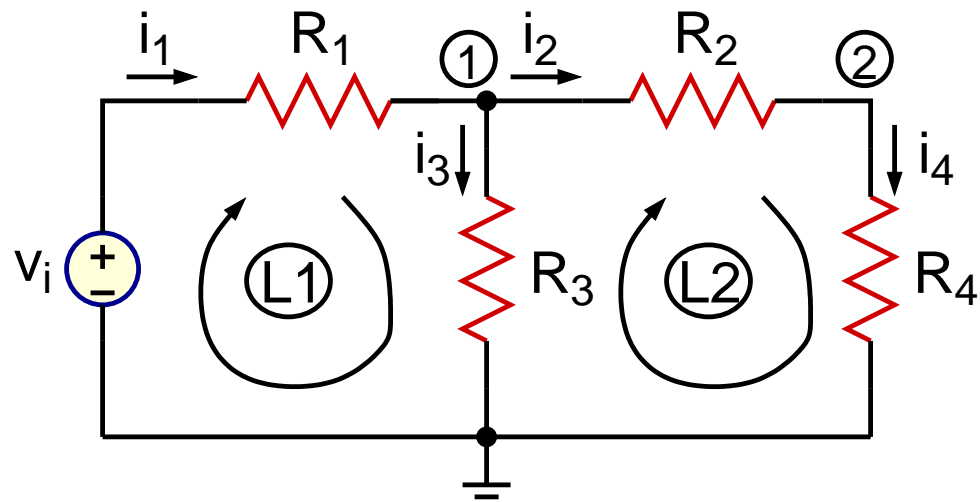
KVL: Kirchoff's Voltage Law

Sum of all node-to-node voltages around the closed loop is zero.

KCL: Kirchoff's Current Law

Sum of all currents leaving a node is zero.

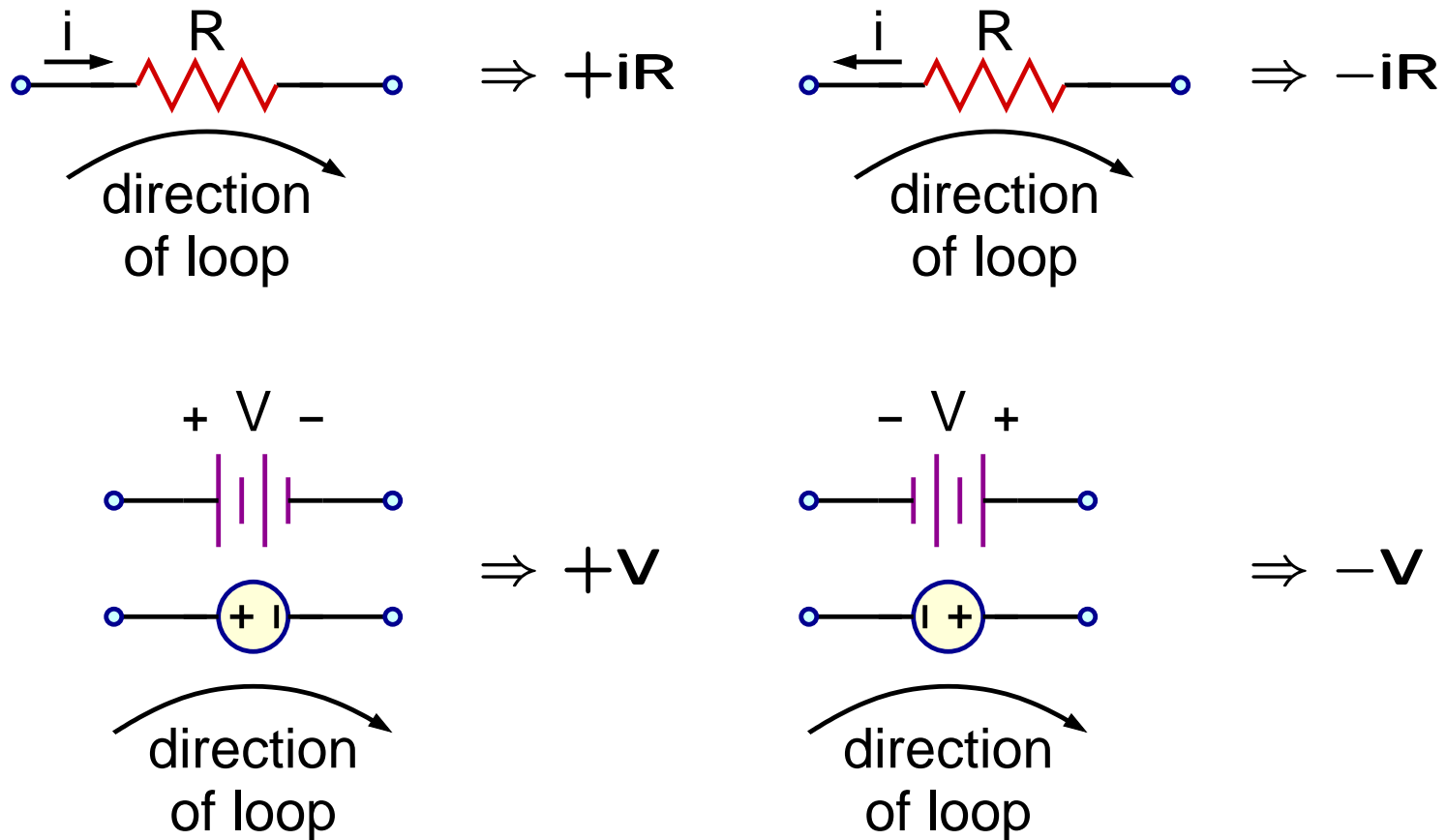
KVL



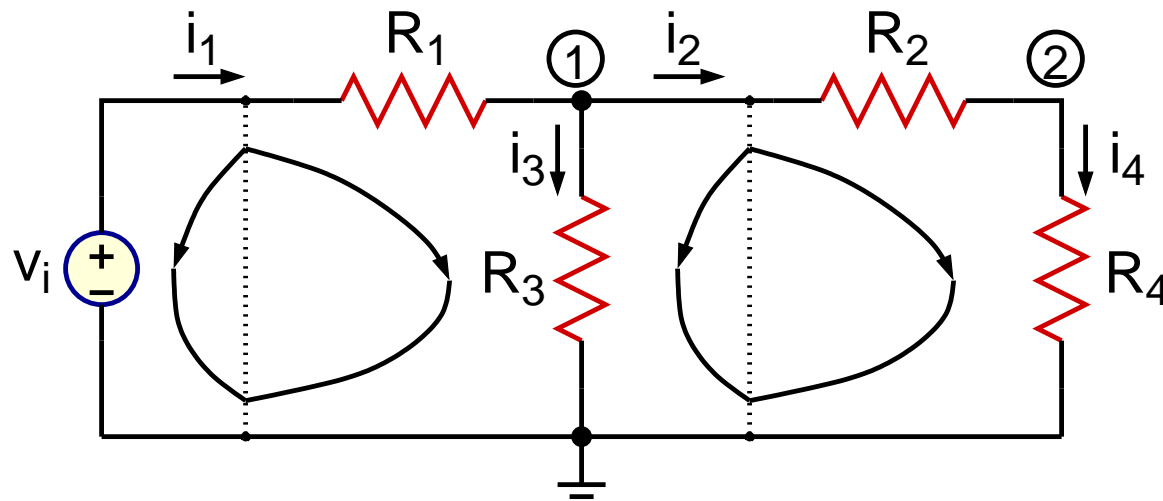
$$L_1 \rightarrow -v_i + i_1 R_1 + i_3 R_3 = 0$$

$$L_2 \rightarrow i_2 R_2 + i_4 R_4 - i_3 R_3 = 0$$

KVL

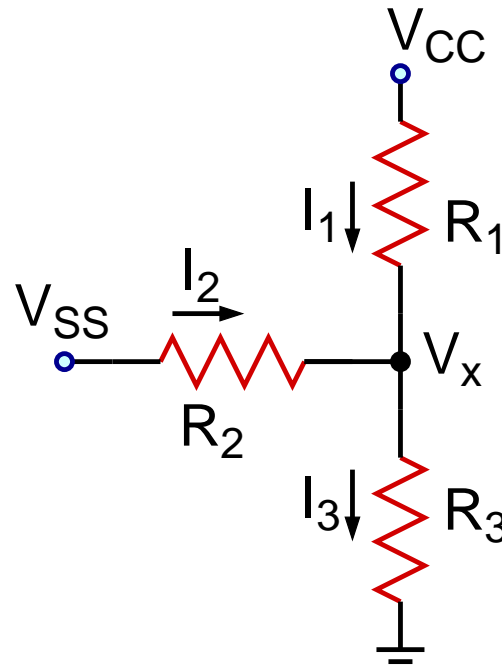


KVL



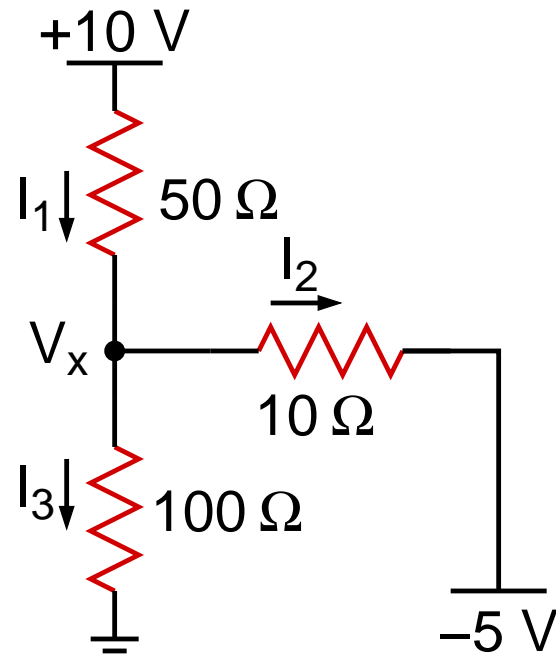
$$L_1 \rightarrow v_i = i_1 R_1 + i_3 R_3$$

$$L_2 \rightarrow i_3 R_3 = i_2 R_2 + i_4 R_4$$



$$V_{CC} = I_1 R_1 + I_3 R_3$$

$$V_{SS} = I_2 R_2 + I_3 R_3$$

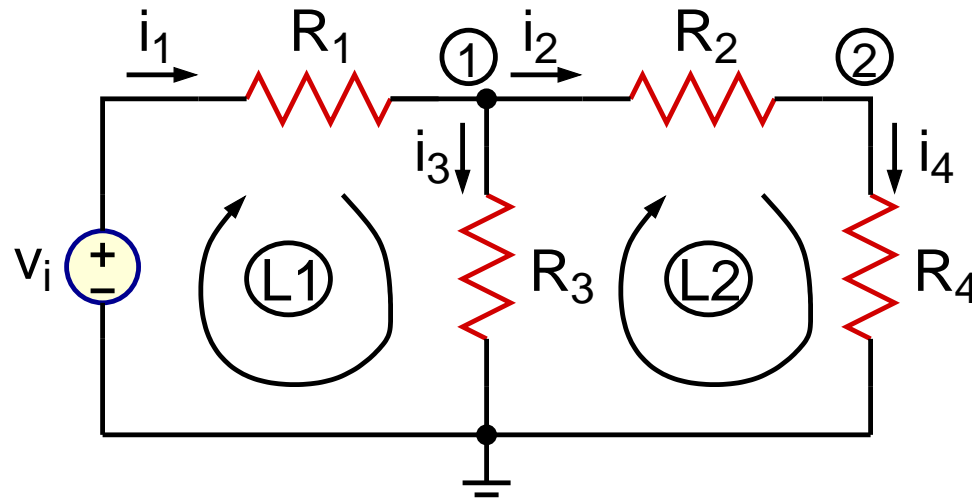


$$10 = 50I_1 + 100I_3$$

$$-5 = -10I_2 + 100I_3$$

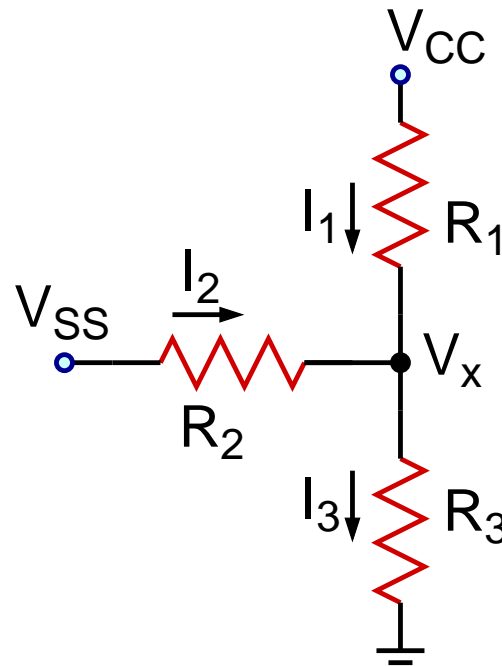
$$10 = 50I_1 + 10I_2 - 5$$

KCL

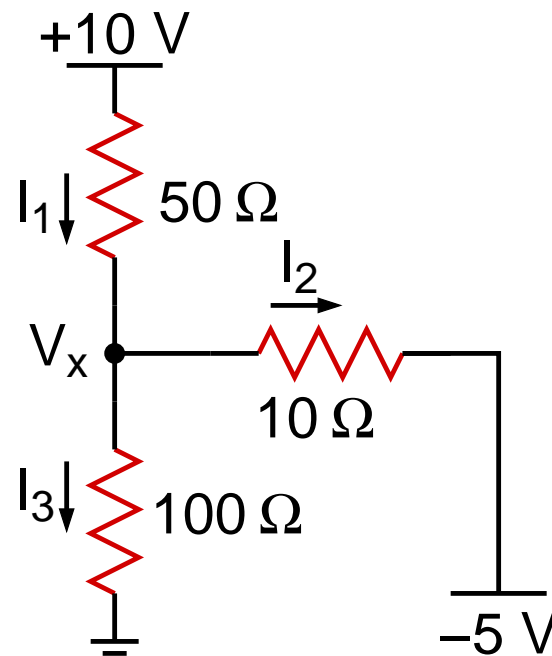


$$\textcircled{1} \rightarrow -i_1 + i_2 + i_3 = 0 \rightarrow \frac{v_1 - v_i}{R_1} + \frac{v_1 - v_2}{R_2} + \frac{v_1}{R_3} = 0$$

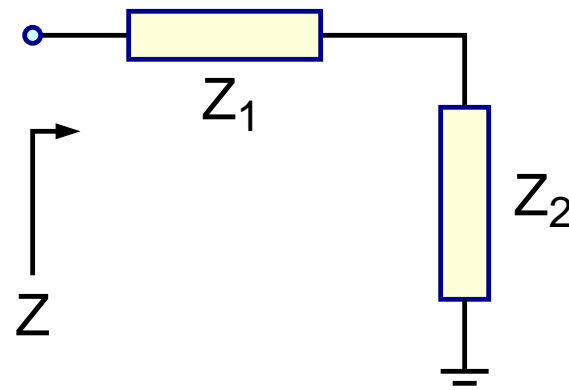
$$\textcircled{2} \rightarrow -i_2 + i_4 = 0 \rightarrow \frac{v_2 - v_1}{R_2} + \frac{v_2}{R_4} = 0$$



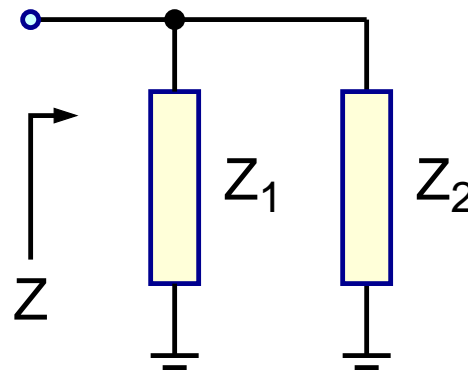
$$\frac{V_x - V_{SS}}{R_2} + \frac{V_x - V_{CC}}{R_1} + \frac{V_x}{R_3} = 0$$



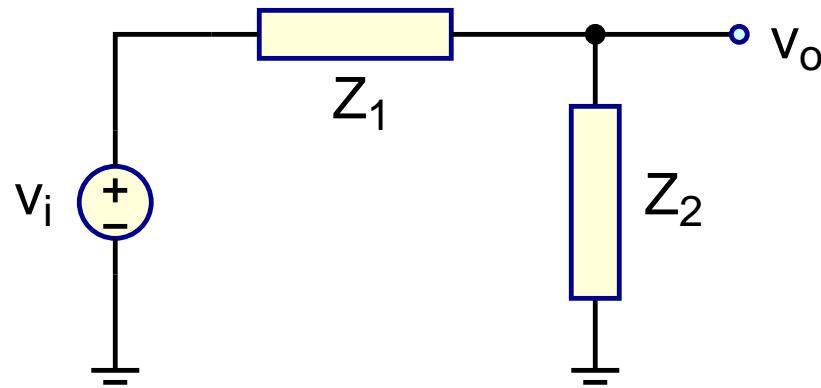
$$\frac{V_x - (-5)}{10} + \frac{V_x}{100} + \frac{V_x - 10}{50} = 0$$



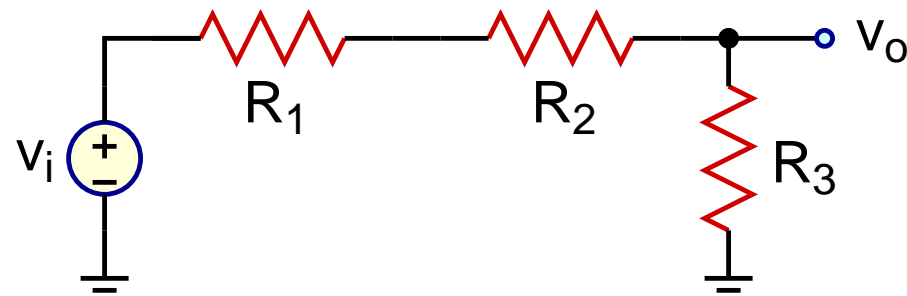
$$Z = Z_1 + Z_2$$



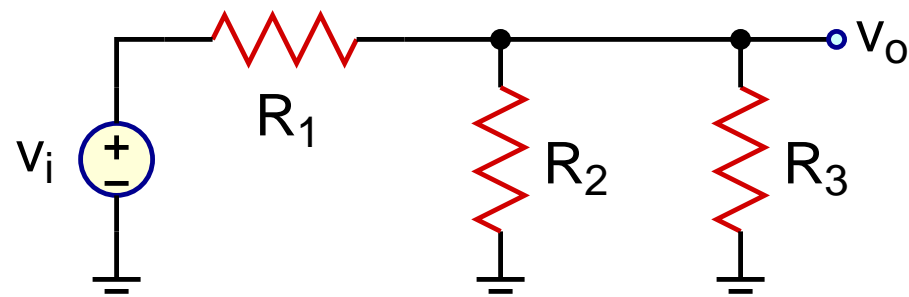
$$Z = Z_1 \parallel Z_2$$



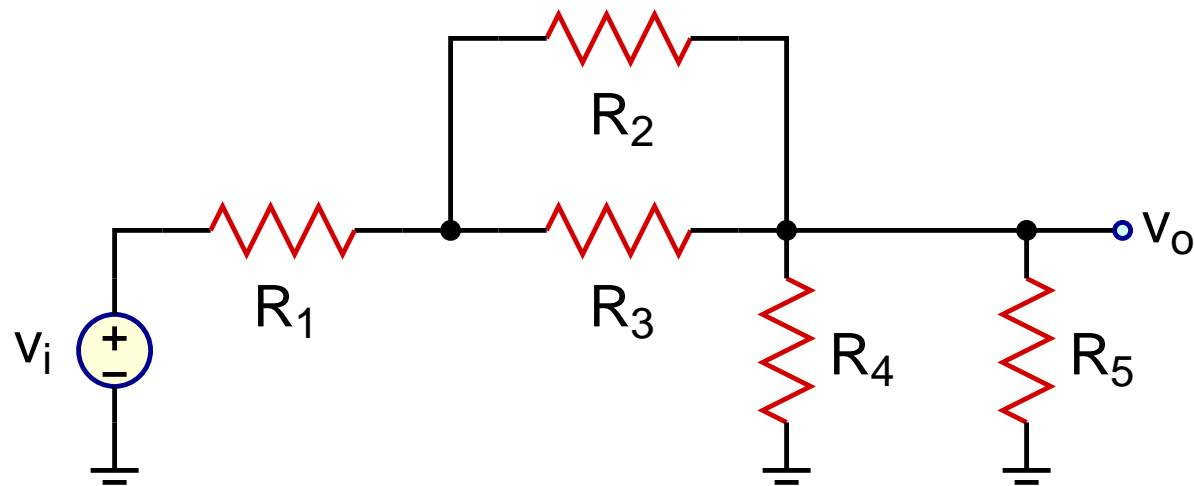
$$\frac{V_o}{V_i} = \frac{Z_2}{Z_1 + Z_2}$$



$$\frac{V_o}{V_i} = \frac{R_3}{R_1 + R_2 + R_3}$$

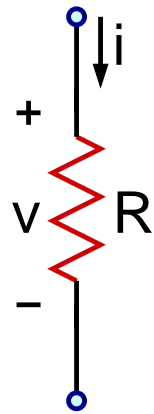


$$\frac{v_o}{v_i} = \frac{R_2 \parallel R_3}{R_1 + (R_2 \parallel R_3)}$$



$$\frac{V_o}{V_i} = \frac{R_4 \parallel R_5}{R_1 + (R_2 \parallel R_3) + (R_4 \parallel R_5)}$$

Linear Network Analysis



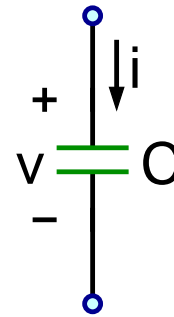
$$v = iR$$

$$Z = R$$



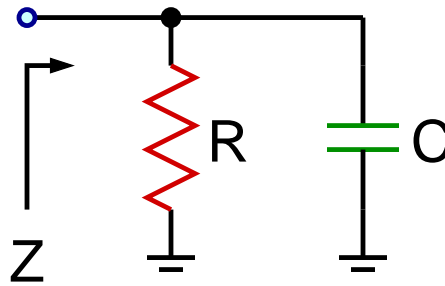
$$v = sLi$$

$$Z = sL$$

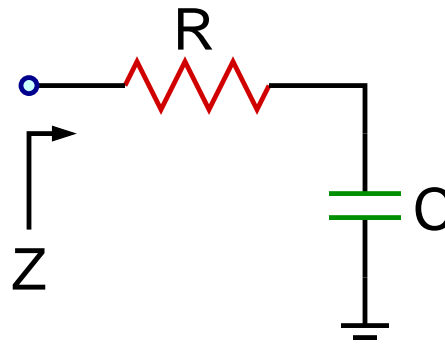


$$v = \frac{1}{sC}i$$

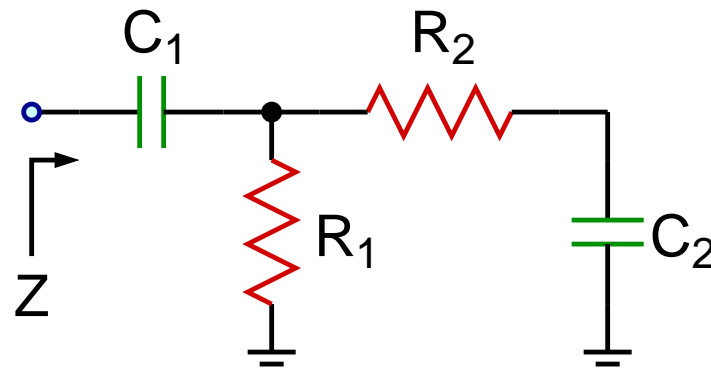
$$Z = \frac{1}{sC}$$



$$Z = R \parallel \frac{1}{sC}$$



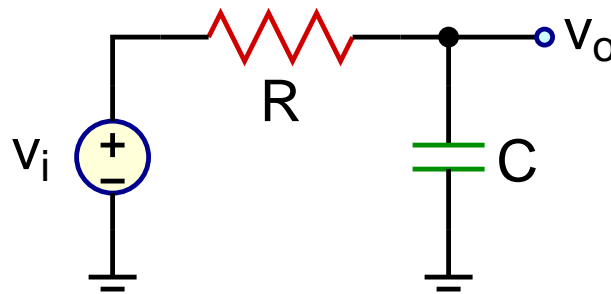
$$Z = R + \frac{1}{sC}$$



$$Z = \frac{1}{sC_1} + \left(R_1 \parallel \left(R_2 + \frac{1}{sC_2} \right) \right)$$

Low-pass Network

Transfer function



$$\frac{V_o}{V_i} = \frac{\frac{1}{sC}}{R + \frac{1}{sC}} = \frac{1}{sRC + 1} = \frac{1}{\frac{s}{\omega_0} + 1} = T(s)$$

$$\omega_0 = \frac{1}{RC}$$

$$T(s) = \frac{1}{\frac{s}{\omega_0} + 1} \Rightarrow T(j\omega) = \frac{1}{\frac{j\omega}{\omega_0} + 1}$$

$$|T(j\omega)| = \frac{1}{\sqrt{\left(\frac{\omega}{\omega_0}\right)^2 + 1}}$$

$$20 \log |T(j\omega)| = -20 \log \sqrt{\left(\frac{\omega}{\omega_0}\right)^2 + 1}$$

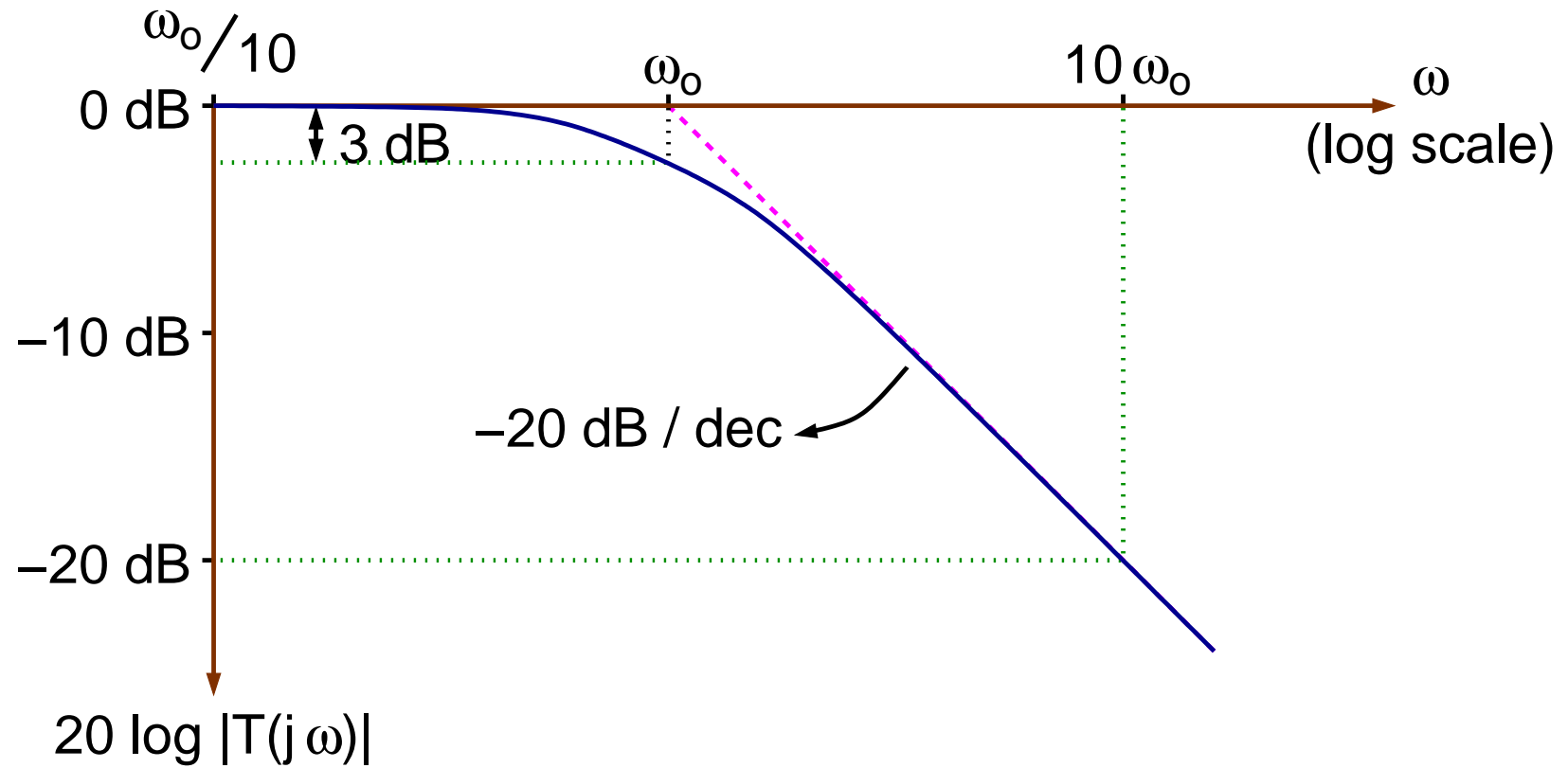
$$\omega \ll \omega_0 \Rightarrow 20 \log |T(j\omega)| \approx 0$$

$$\omega \gg \omega_0 \Rightarrow 20 \log |T(j\omega)| \approx 20 \log \omega_0 - 20 \log \omega$$

$$\omega = \omega_0 \Rightarrow 20 \log |T(j\omega)| = -20 \log \sqrt{2} \approx -3 \text{ dB}$$

Low-pass Network

Bode magnitude plot



$$T(s) = \frac{1}{\frac{s}{\omega_0} + 1} \Rightarrow T(j\omega) = \frac{1}{\frac{j\omega}{\omega_0} + 1}$$

$$\angle T(j\omega) = -\tan^{-1}\left(\frac{\omega}{\omega_0}\right)$$

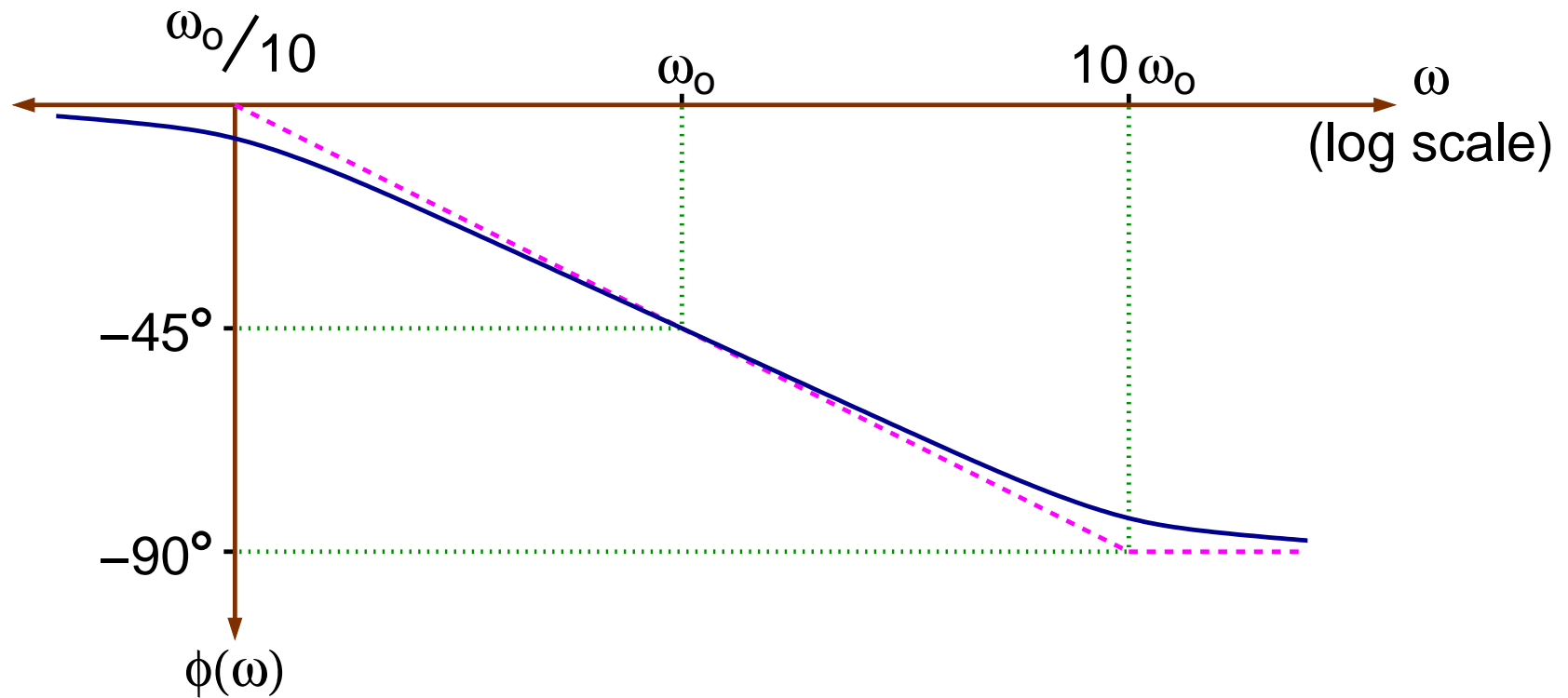
$$\omega \ll \omega_0 \Rightarrow \angle T(j\omega) \approx 0^\circ$$

$$\omega \gg \omega_0 \Rightarrow \angle T(j\omega) \approx -90^\circ$$

$$\omega = \omega_0 \Rightarrow \angle T(j\omega) = -45^\circ$$

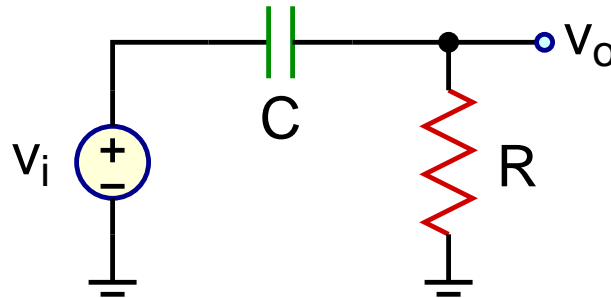
Low-pass Network

Bode phase plot



High-pass Network

Transfer function



$$\frac{V_o}{V_i} = \frac{R}{\frac{1}{sC} + R} = \frac{s}{s + \frac{1}{RC}} = \frac{s}{s + \omega_0} = T(s)$$

$$\omega_0 = \frac{1}{RC}$$

$$T(s) = \frac{s}{s + \omega_0} \Rightarrow T(j\omega) = \frac{j\omega}{j\omega + \omega_0} = \frac{1}{1 - \frac{j\omega_0}{\omega}}$$

$$|T(j\omega)| = \frac{1}{\sqrt{1 + \left(\frac{\omega_0}{\omega}\right)^2}}$$

$$20 \log |T(j\omega)| = -20 \log \sqrt{1 + \left(\frac{\omega_0}{\omega}\right)^2}$$

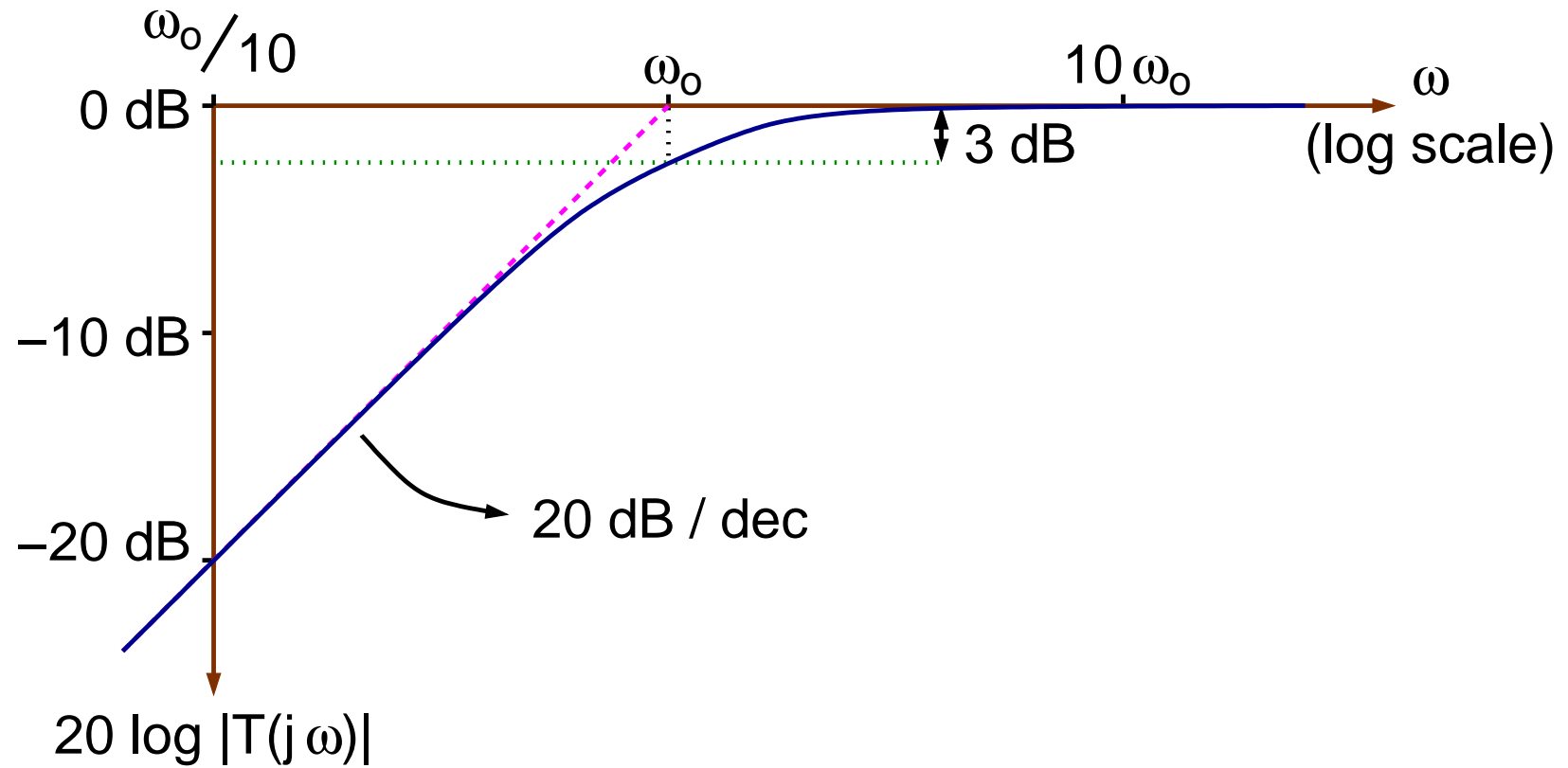
$$\omega \ll \omega_0 \Rightarrow 20 \log |T(j\omega)| \approx 20 \log \omega - 20 \log \omega_0$$

$$\omega \gg \omega_0 \Rightarrow 20 \log |T(j\omega)| \approx 0$$

$$\omega = \omega_0 \Rightarrow 20 \log |T(j\omega)| = -20 \log \sqrt{2} \approx -3 \text{ dB}$$

High-pass Network

Bode magnitude plot



$$T(s) = \frac{s}{s + \omega_0} \Rightarrow T(j\omega) = \frac{j\omega}{j\omega + \omega_0} = \frac{1}{1 - \frac{j\omega_0}{\omega}}$$

$$\angle T(j\omega) = \tan^{-1} \left(\frac{\omega_0}{\omega} \right)$$

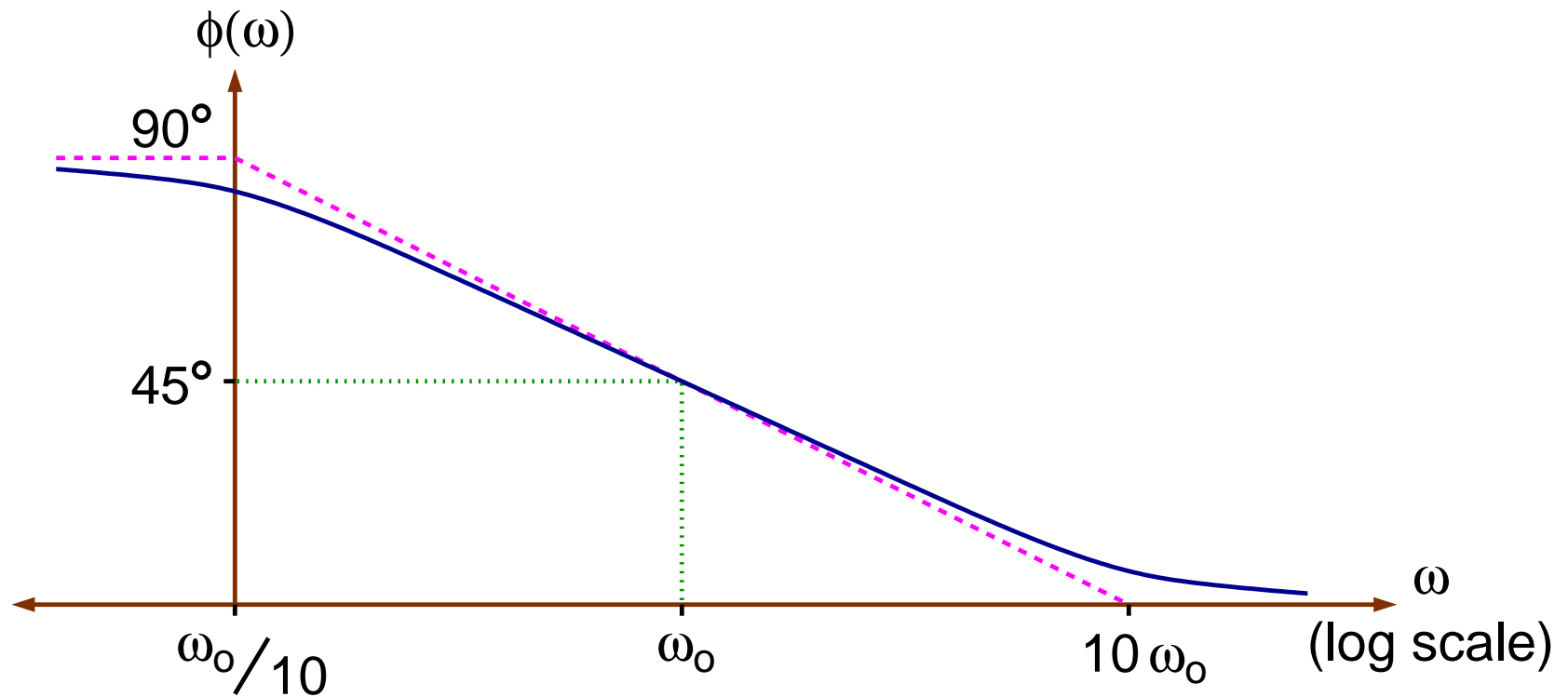
$$\omega \ll \omega_0 \Rightarrow \angle T(j\omega) \approx 90^\circ$$

$$\omega \gg \omega_0 \Rightarrow \angle T(j\omega) \approx 0^\circ$$

$$\omega = \omega_0 \Rightarrow \angle T(j\omega) = 45^\circ$$

High-pass Network

Bode phase plot



Generalized first order low-pass:

$$T(s) = \frac{K}{\frac{s}{\omega_0} + 1}$$

$$20 \log |T(j\omega)| = 20 \log K - 20 \log \sqrt{\left(\frac{\omega}{\omega_0}\right)^2 + 1}$$

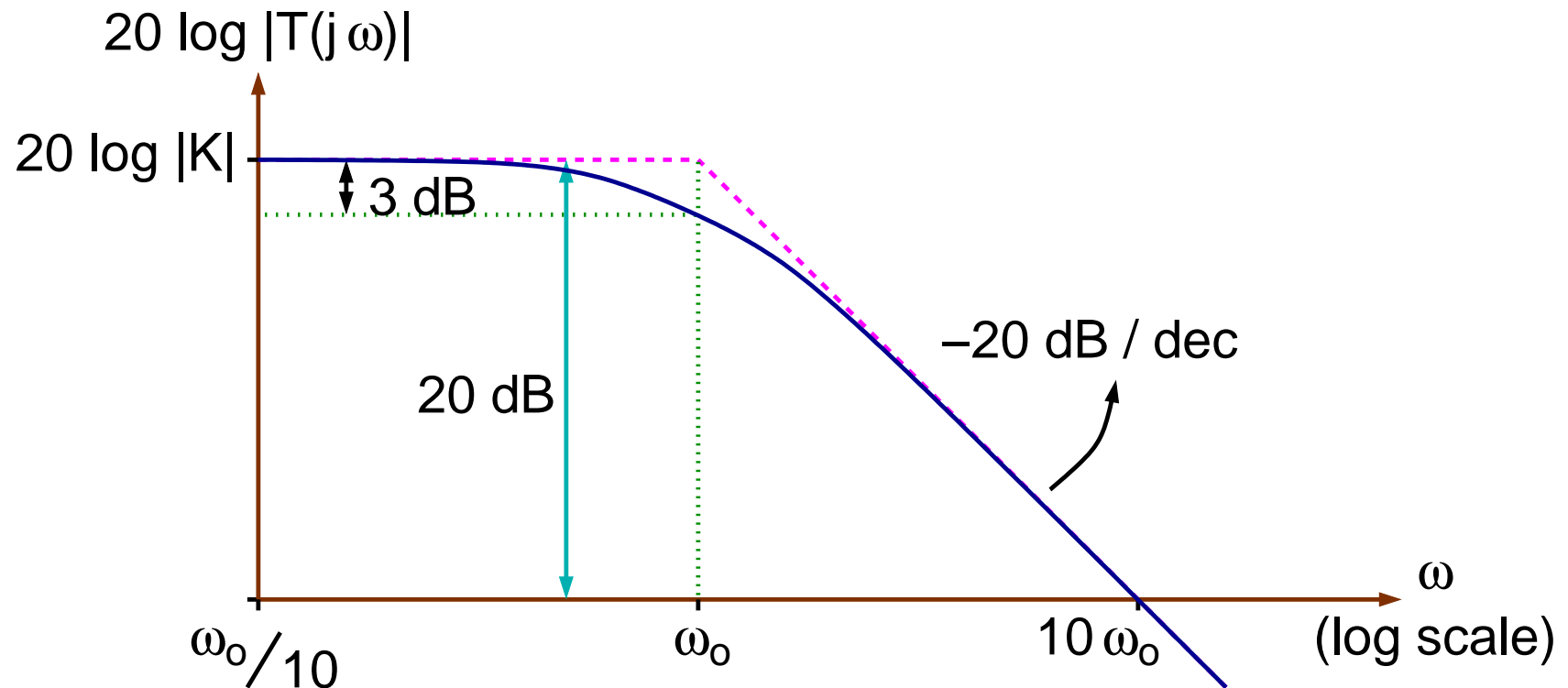
Generalized first order high-pass:

$$T(s) = \frac{Ks}{s + \omega_0}$$

$$20 \log |T(j\omega)| = 20 \log K - 20 \log \sqrt{1 + \left(\frac{\omega_0}{\omega}\right)^2}$$

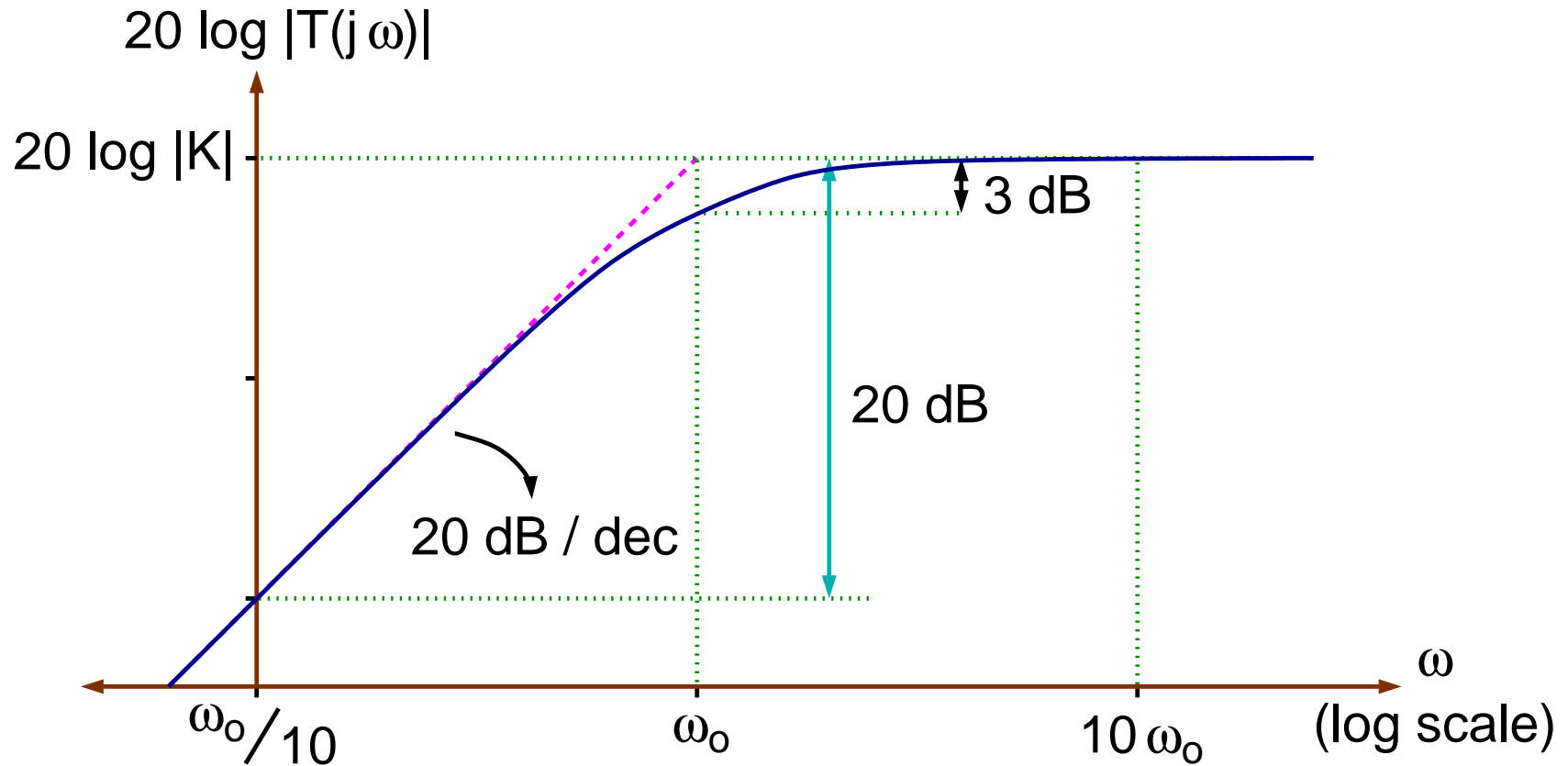
Generalized Low-pass

Bode magnitude plot

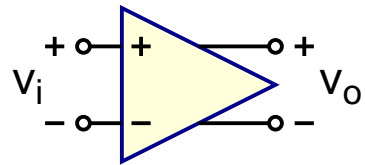


Generalized High-pass

Bode magnitude plot

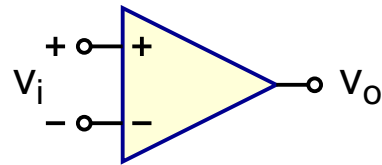


Amplifiers



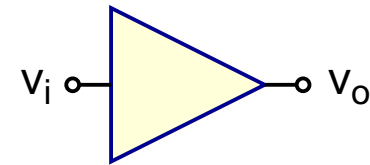
In: Differential

Out: Differential



Differential

Single-ended

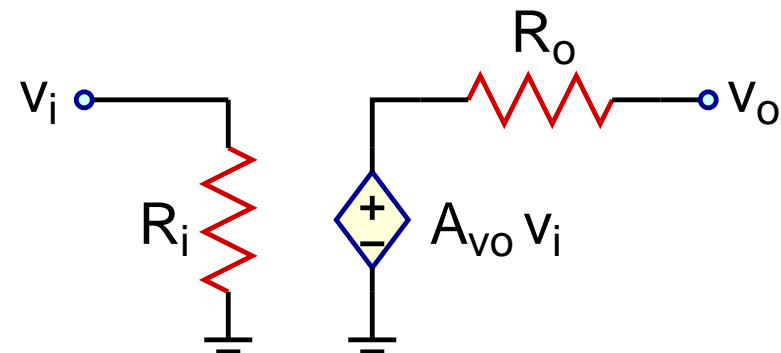


Single-ended

Single-ended

Voltage Amplifier

Circuit model



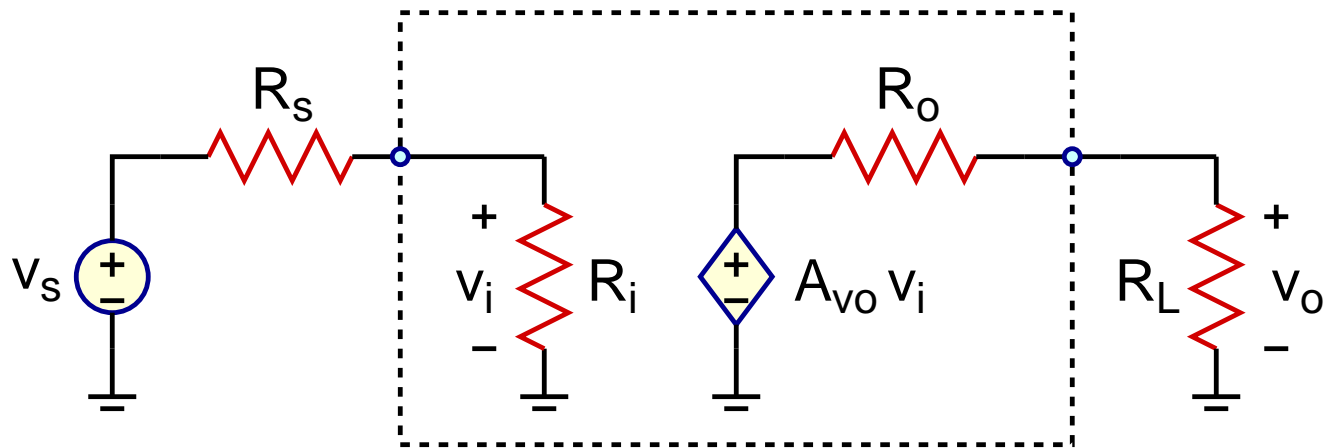
R_i : Input resistance

R_o : Output resistance

A_{vo} : Open-loop voltage gain

Voltage Amplifier

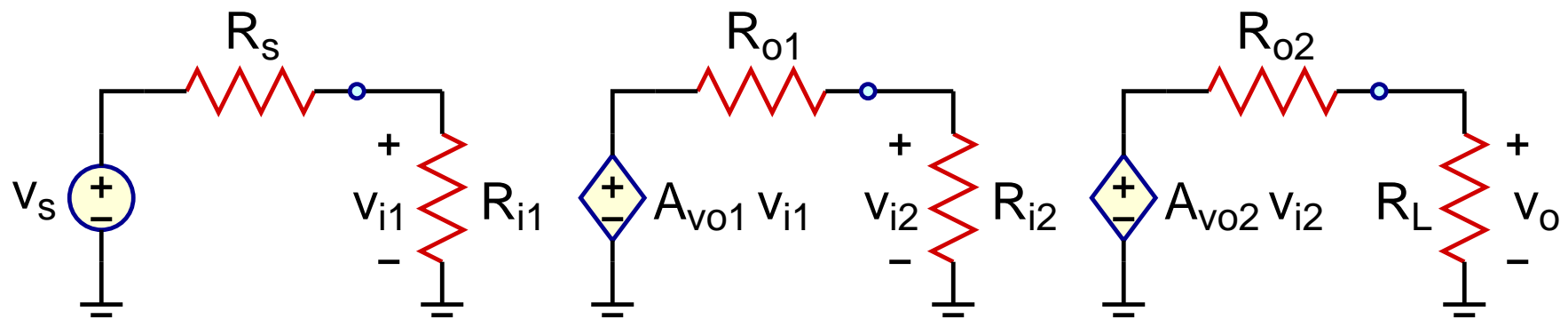
Source and load connected



$$\frac{v_o}{v_s} = \frac{R_i}{R_s + R_i} A_{vo} \frac{R_L}{R_o + R_L}$$

Voltage Amplifier

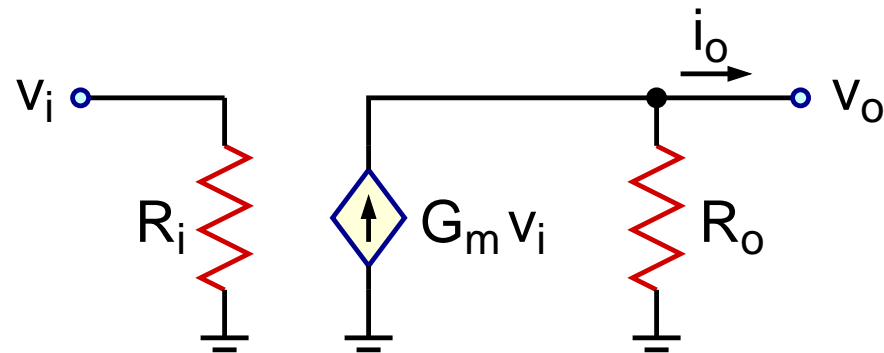
Cascaded



$$\frac{V_o}{V_s} = \frac{R_{i1}}{R_s + R_{i1}} A_{vo1} \frac{R_{i2}}{R_{o1} + R_{i2}} A_{vo2} \frac{R_L}{R_{o2} + R_L}$$

Transconductance amplifier

Circuit model



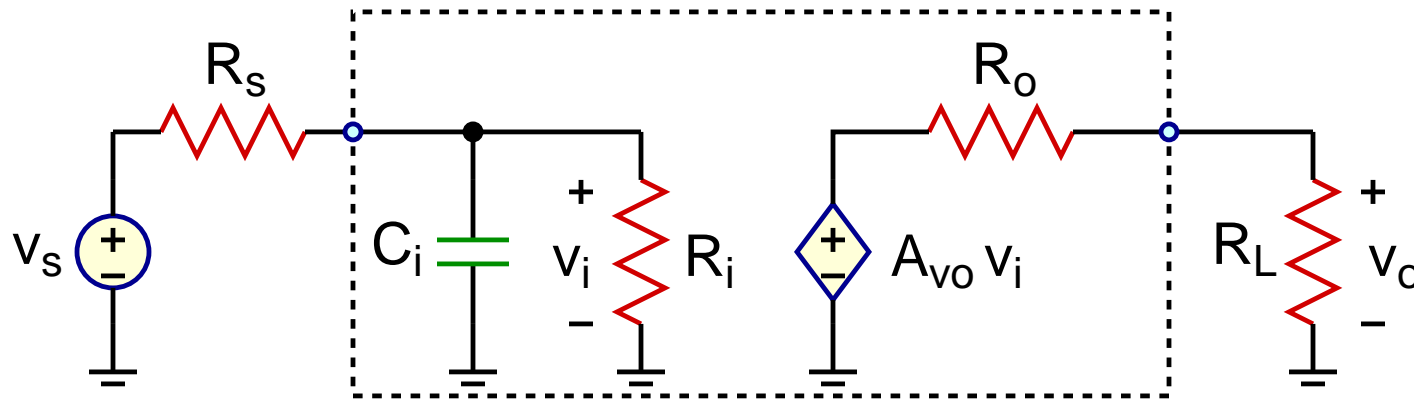
R_i : Input resistance

R_o : Output resistance

G_m : Short-circuit transconductance gain

Voltage Amplifier

Frequency response



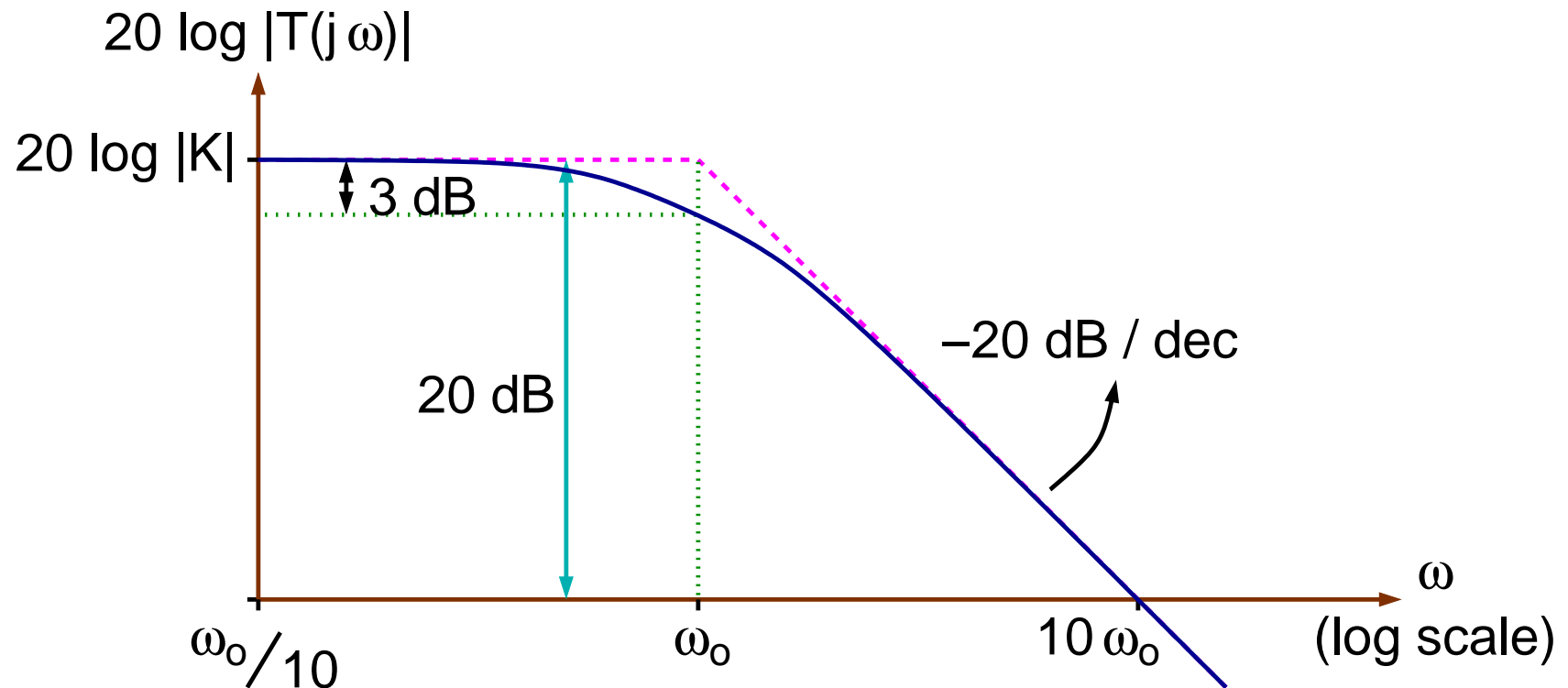
$$\frac{v_o}{v_s} = \frac{R_i \parallel \frac{1}{sC_i}}{R_s + \left(R_i \parallel \frac{1}{sC_i} \right)} A_{vo} \frac{R_L}{R_o + R_L} = T(s)$$

$$T(s) = \frac{K}{\frac{s}{\omega_0} + 1}$$

$$K = \frac{R_i}{R_s + R_i} A_{vo} \frac{R_L}{R_o + R_L}, \quad \omega_0 = \frac{1}{(R_i \parallel R_s) C_i}$$

Voltage Amplifier

Bode magnitude plot



Voltage Amplifier

Bode phase plot

