

**Texas A&M University  
Department of Electrical and Computer Engineering**

**ECEN 325 – Electronics**

**Spring 2021**

**Exam #1**

**Instructor: Sam Palermo**

- Please write your name in the space provided below
- Please verify that there are 6 pages in your exam
- Good Luck!

Problem	Score	Max Score
1		30
2		25
3		25
4		20
<b>Total</b>		<b>100</b>

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UIN: \_\_\_\_\_

Problem 1 (30 points)

Plot the magnitude and phase response of the following transfer function. Label key points and slopes.

$$H(s) = \frac{100s(s + 10^5)}{(s + 10^4)(s + 10^6)}$$

DC gain =  $\phi = -\infty$  dB

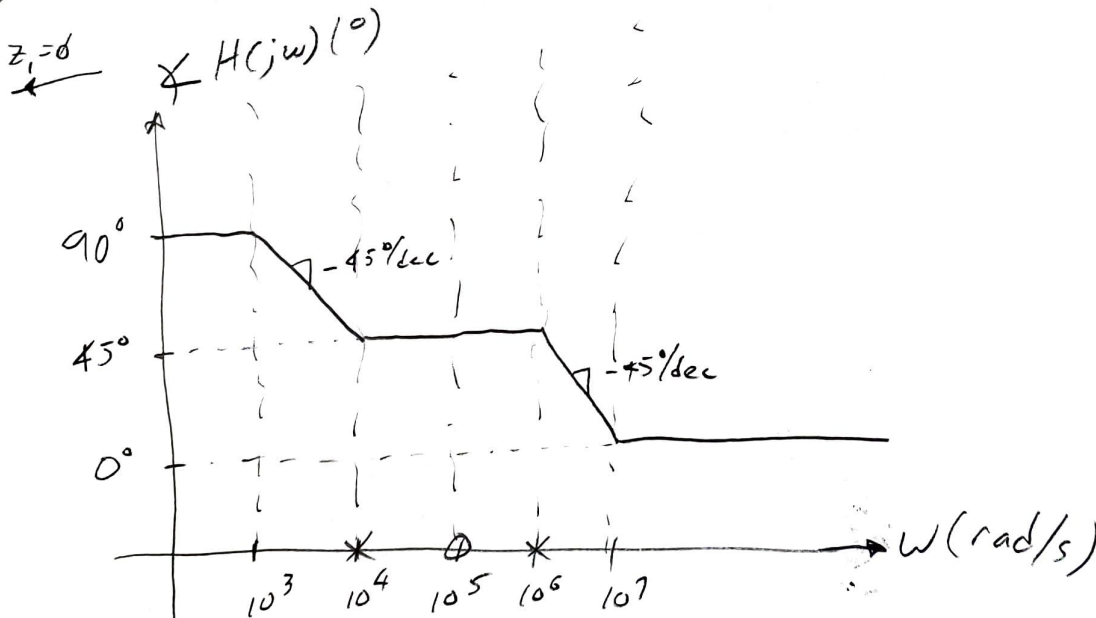
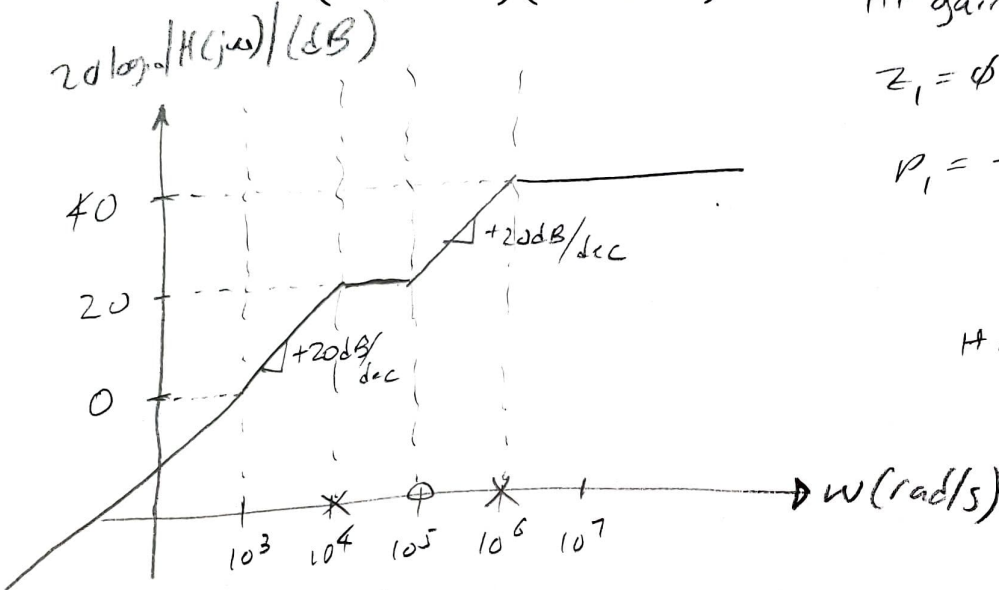
HF gain = 100 = 40 dB

$z_1 = 0, z_2 = -10^5$

$p_1 = -10^4, p_2 = -10^6$

LF Phase =  $90^\circ$

HF Phase =  $90^\circ + 1(90^\circ) + 2(-90^\circ)$   
 $= 0^\circ$



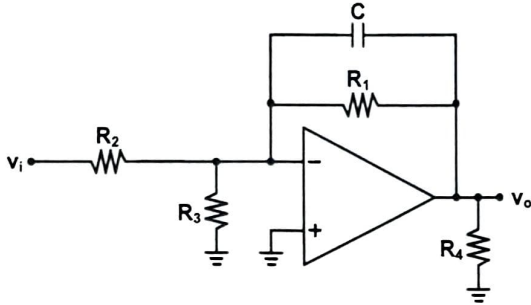
## Problem 2 (25 points)

Assume for Problem 2 circuits that all operational amplifiers are ideal.

For the following circuit:

i. Obtain the transfer function,  $v_o(s)/v_i(s)$

ii. Set the component values to achieve a  $100\Omega$  input resistance, 40dB low-frequency gain (magnitude), and a pole frequency of  $|\omega_p| = 100\text{krad/s}$ .



$$\frac{V_o}{V_i} = -\frac{Z_{R1} \parallel Z_C}{Z_{R2}} = -\frac{1}{\left(\frac{1}{R_1} + sC\right)R_2} = \frac{-\frac{R_1}{R_2}}{1 + sR_1C}$$

$$\boxed{\frac{V_o}{V_i} = \frac{-\frac{R_1}{R_2}}{1 + sR_1C}}$$

$$R_{in} = R_2 = 100\Omega$$

$$|LFGain| = 40\text{dB} = 100 \Rightarrow R_1 = 100R_2 = 100(100\Omega) = 10\text{k}\Omega$$

$$|\omega_p| = \frac{1}{R_1C} = 100\text{krad/s}$$

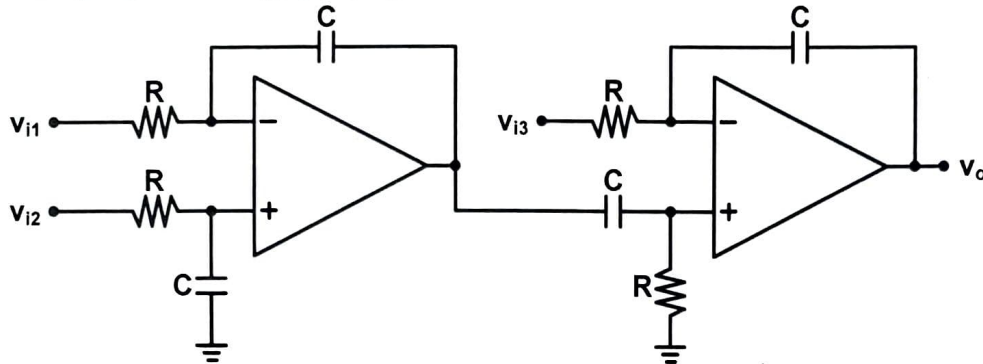
$$C = \frac{1}{R_1|\omega_p|} = \frac{1}{(10\text{k}\Omega)(100\text{krad/s})} = 1\text{nF}$$

$$\boxed{\begin{array}{l} R_1 = 10\text{k}\Omega \\ R_2 = 100\Omega \\ C = 1\text{nF} \end{array}}$$

## Problem 3 (25 points)

Assume for Problem 3 circuits that all operational amplifiers are ideal.

For the following circuit obtain the expression for  $v_o$  as a function of  $v_{i1}$ ,  $v_{i2}$ , and  $v_{i3}$ . Assume ideal opamps. Hint: apply superposition.



$$V_o = - \left( \frac{z_c}{z_R} \right) \left( \frac{z_R}{z_R + z_c} \right) \left( 1 + \frac{z_c}{z_R} \right) v_{i1}$$

$$+ \left( \frac{z_c}{z_R + z_c} \right) \left( 1 + \frac{z_c}{z_R} \right) \left( \frac{z_R}{z_c + z_R} \right) \left( 1 + \frac{z_c}{z_R} \right) v_{i2}$$

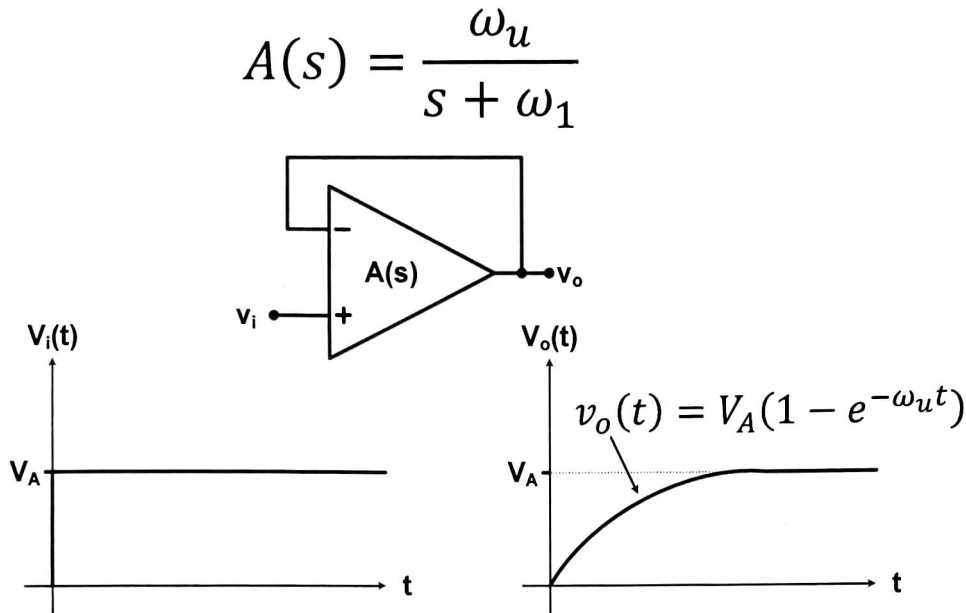
$$- \left( \frac{z_c}{z_R} \right) v_{i3}$$

$$V_o = - \left( \frac{z_c}{z_R} \right) v_{i1} + \frac{z_c}{z_R} v_{i2} - \frac{z_c}{z_R} v_{i3}$$

$$V_o = \frac{1}{sRC} \left[ -v_{i1} + v_{i2} - v_{i3} \right]$$

## Problem 4 (20 points)

The step response of a unity-gain voltage follower constructed with a single-pole opamp with unity gain frequency,  $\omega_u$ , is given below. The operational amplifier for this problem has a finite slew rate of  $10\text{V}/\mu\text{s}$ . Given an input step amplitude  $V_A=5\text{V}$ , what is the maximum opamp unity gain frequency,  $\omega_u$ , that the opamp can have and still produce an un-distorted single-pole transient step response?



$$\max \left( \left| \frac{dv_o(t)}{dt} \right| \right) \leq SR$$

$$\frac{dv_o(t)}{dt} = V_A \omega_u e^{-\omega_u t}$$

$$\max \left( \left| \frac{dv_o(t)}{dt} \right| \right) = V_A \omega_u \leq SR$$

$$\omega_u \leq \frac{SR}{V_A} = \frac{10\text{V}/\mu\text{s}}{5\text{V}} = 2\text{Mrad/s}$$

$$\text{Max } \omega_u = 2\text{Mrad/s}$$