

# *A Simplified Methodology for the Extraction of Parameters of the ACM MOST Model*

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# **ACM MODEL**

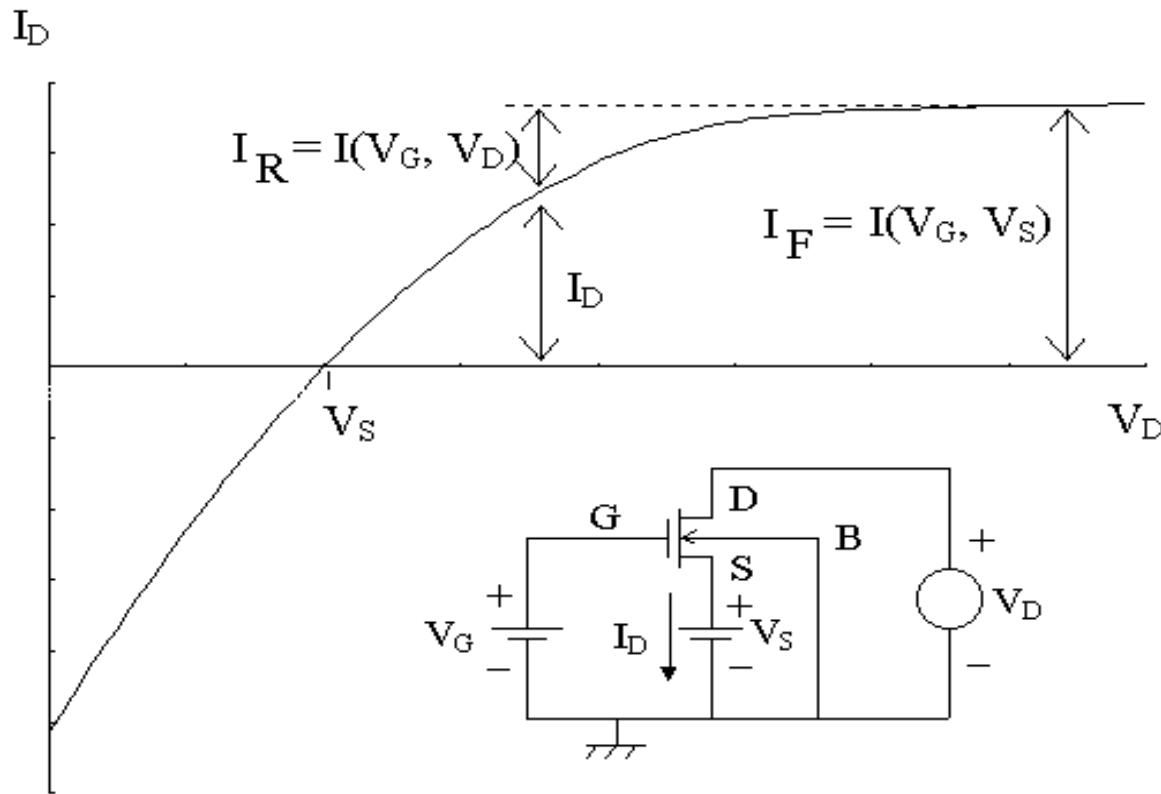
## **ADVANCED COMPACT**

### **MOSFET MODEL**

- ✓ A physically based MOSFET model
- ✓ Accurate in all regions of operation
- ✓ Source-to-drain intrinsic symmetry
- ✓ Charge conservation
- ✓ Small set of parameters

# MOS transistor modeling

Forward and reverse currents:  $I_D = I_F - I_R = I(V_G, V_S) - I(V_G, V_D)$



For large  $V_D$ ,  $I_R \rightarrow 0$ ; therefore,  $I_D = I_F - I_R \cong I_F$

**The current-based model**     $I_D = I_F - I_R$     or     $I_D = I_S(i_f - i_r)$

where:     $I_S = I_{SQ} \frac{W}{L}$      $I_{SQ} = \mu n C'_{ox} \frac{\phi_t^2}{2}$

$I_{F(R)}$ : forward (reverse) current

$i_{f(r)}$ : inversion level at source (drain)

$I_S$ : specific (normalization) current

$I_{SQ}$ : specific (normalization) sheet current is weakly dependent on  $V_G$  [ $\mu(V_G)$ ,  
 $n(V_G)$ ]  $\Rightarrow I_{SQ}$  is a technological parameter

All large- and small-signal parameters can be written in terms of  $i_f$  and  
 $i_r \Rightarrow$ current-based model, appropriate for electrical characterization,  
hand analysis and design

# The I x V relationship

$$V_P - V_{S(D)} = \phi_t \left[ \sqrt{1+i_{f(r)}} - 2 + \ln \left( \sqrt{1+i_{f(r)}} - 1 \right) \right] \quad V_P \cong \frac{V_G - V_{T0}}{n}$$

a) weak inversion:  $i_{f(r)} \ll 1$        $V_P - V_{S(D)} \cong \phi_t \left[ -1 + \ln \left( \frac{i_{f(r)}}{2} \right) \right] \Rightarrow$

$$I_D \cong 2I_S \exp \left( \frac{V_G - V_{T0} - nV_S}{n\phi_t} + 1 \right) \left[ 1 - \exp \left( -\frac{V_{DS}}{\phi_t} \right) \right]$$

b) strong inversion at source and drain:  $i_{f(r)} \gg 1$

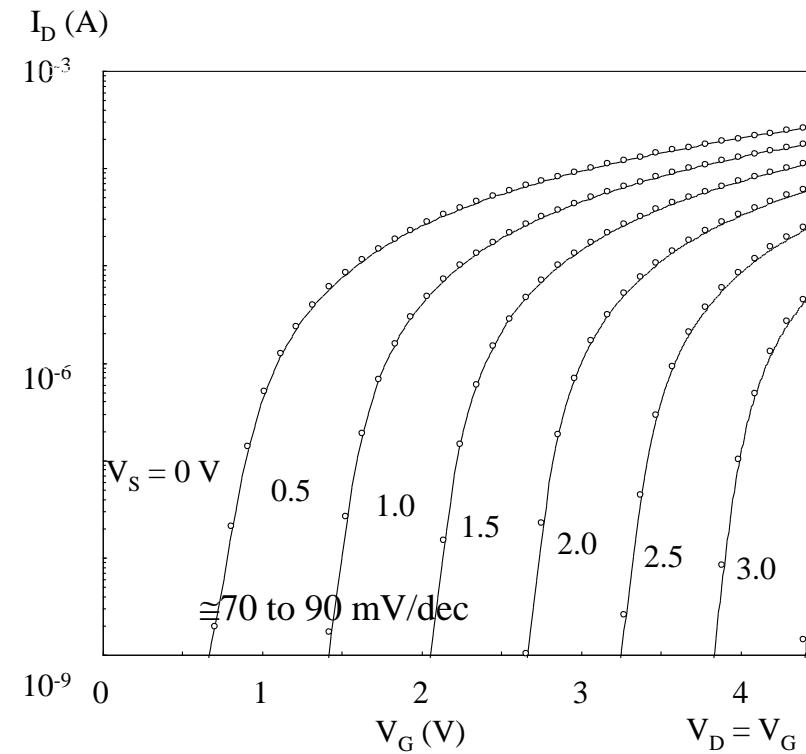
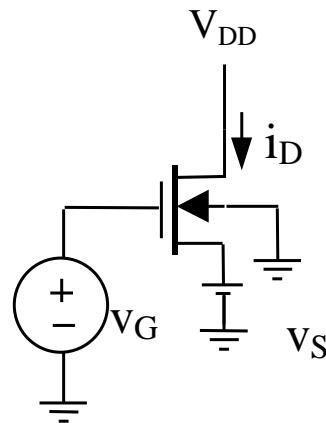
$$I_D \cong \frac{\mu n C'_ox}{2} \frac{W}{L} [(V_P - V_S)^2 - (V_P - V_D)^2]$$

c) forward saturation:  $i_f \gg i_r \Rightarrow I_D$  is (almost) independent of  $V_D$

c1) weak inversion:  $I_D \cong 2I_{SQ} \frac{W}{L} \exp \left( \frac{V_G - V_{T0} - nV_S}{n\phi_t} + 1 \right)$

c2) strong inversion  $I_D \cong \frac{\mu C'_ox}{2n} \frac{W}{L} (V_G - V_{T0} - nV_S)^2 = I_{SQ} \frac{W}{L} \left( \frac{V_G - V_{T0} - nV_S}{n\phi_t} \right)^2$

# Common-source characteristics of NMOS transistor in saturation



$t_{ox} = 280 \text{ \AA}$ ,  $W = L = 25 \mu\text{m}$ ,  $V_{DD} = 5 \text{ V}$   
— ACM model (o) experimental

## Second order effects

- Drain-induced barrier lowering  $\rightarrow V_T$  depends on both  $V_D$  and  $V_S$

$$\hat{V}_{T0} = V_{T0} - \sigma(V_S + V_D)/2 \quad \sigma = \text{SIGMA}/L_{\text{eff}}^2$$

- Channel length modulation

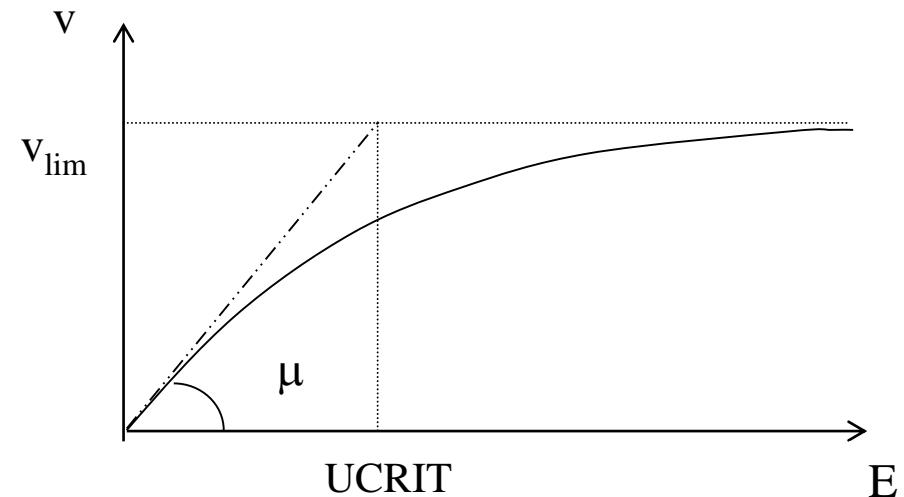
$$\Delta L = PCLM \cdot L_C \cdot \ln \left( 1 + \frac{V_{DS} - V_{DS,SAT}}{L_C UCRIT} \right)$$

- Mobility reduction due to transversal field

$$\mu = \frac{\mu_0}{1 + \theta(V_{GS} - V_{T0})}$$

- Velocity saturation

$$v_{\text{lim}} = 5 \times 10^6 \text{ to } 2 \times 10^7 \text{ cm/s}$$



# ACM Parameters

Parameter	Description	Units
VTO	Zero-bias threshold voltage	V
GAMMA	Body-effect parameter	V <sup>1/2</sup>
PHI	Surface potential	V
TOX	Gate oxide thickness	m
LD	Lateral diffusion	m
XJ	Junction depth	m
UO	Low-field mobility	cm <sup>2</sup> /Vs
VMAX	Saturation velocity	m/s
THETA	Mobility reduction parameter	V <sup>-1</sup>
SIGMA	Drain-induced barrier lowering parameter	m <sup>2</sup>
PCLM*	Channel length modulation parameter	-

\*LAMBDA in a previous version of the ACM model

# Mapping BSIM to ACM

ACM Parameter	BSIM 3V3 Parameter	Equation for determining the ACM parameter	Unit
VT0	VTH0	—	V
GAMMA	—	$\text{GAMMA} = \frac{(2 \cdot \epsilon_{\text{SI}} \cdot q \cdot N_{\text{CH}})^{1/2}}{C_{\text{ox}}}$	V <sup>1/2</sup>
PHI	—	$\text{PHI} = 2 \cdot \phi_t \cdot \ln\left(\frac{N_{\text{CH}}}{n_i}\right)$	V
TOX	TOX	—	m
LD	DLC	—	m
XJ	XJ	—	m
U0	U0	—	cm <sup>2</sup> /V·s
VMAX	VSAT	—	m/s
THETA	—	$\text{THETA} = \frac{U_A}{TOX} + \frac{U_B}{TOX^2} \cdot \left[ \frac{(V_{DD} - 2 \cdot V_{T0})}{(V_{DD} + V_{T0})^2 - (3 \cdot V_{T0})^2} \right]$	V <sup>-1</sup>
SIGMA	—	$\text{SIGMA} = \theta_{\text{DIBL}} \cdot \eta_{\text{A0}} \cdot (L_{\text{eff}})^2$	m <sup>2</sup>
PCLM	PCLM	—	—

## Strategy for parameter extraction:

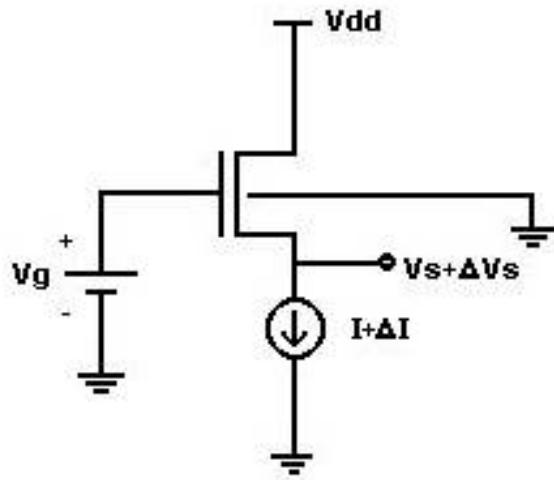
- Parameters derived from device physics
- Bias the MOSFET in a region where the parameter to be extracted has significant effects
- Avoid “optimization”

*If a parameter is difficult to extract, then its effects are not important*

- Extraction of  $I_S$  (strong inversion  $I \gg I_S$ )

Strong inversion & saturation

$$I \approx I_S \left( \frac{V_G - V_{T0} - nV_S}{n\phi_t} \right)^2$$



$$I_S \approx I \times \left( \frac{\Delta I / I}{2 \times \Delta V_S / \phi_t} \right)^2$$

$$I = 40 \mu A$$

$$\Delta I = 4 \mu A \quad \Rightarrow$$

$$\Delta V_S / \phi_t = 0.57$$

$$I_S = 310 nA$$

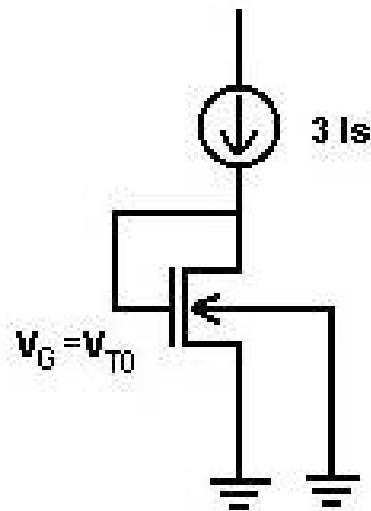
A more accurate method, based on the  $g_m/I_D$  characteristic, can be used to determine  $I_S$

- Extraction of  $V_{T0}$

ACM Model:

$$V_P - V_S = \phi_t \left[ \sqrt{1+i_f} - 2 + \ln \left( \sqrt{1+i_f} - 1 \right) \right]$$

$$V_P \approx \frac{V_G - V_{T0}}{n}$$

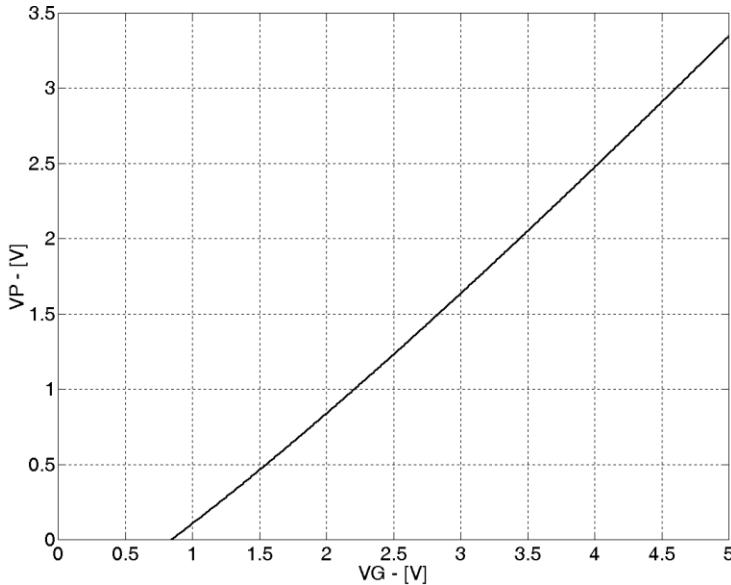


$$i_f = 3 \quad \longrightarrow \quad V_G = V_{T0}$$

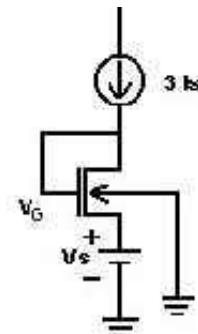
$$I = 3 \cdot I_S \quad \longrightarrow \quad V_G = V_{T0}$$

$$V_{T0} = 0.845 \text{ V}$$

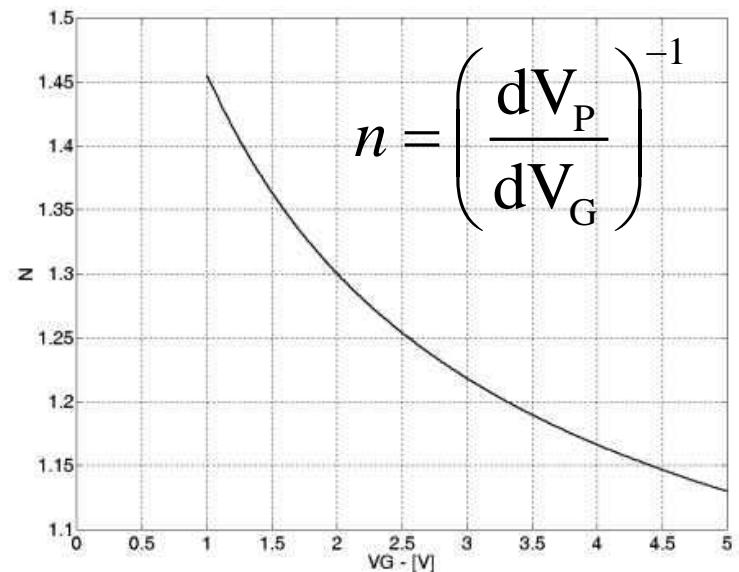
- Extraction of  $V_P$



$$I = 3I_S$$



- Extraction of  $n$



- Calculation of GAMMA ( $\gamma$ )

$$2\phi_F = 0.7, \quad V_{GB} = 2.5V, \quad n = 1.25, \quad V_P = 1.23$$

$$n = 1 + \frac{\gamma}{2\sqrt{2\phi_F + V_P}}$$

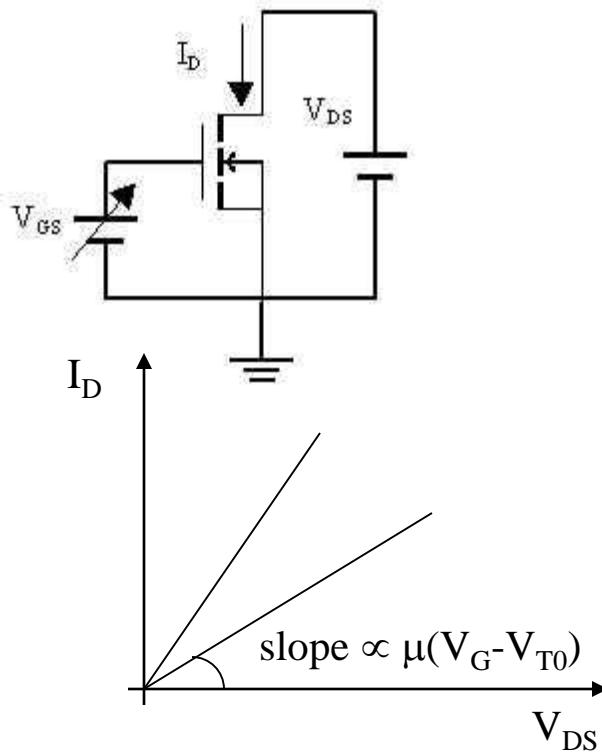
→

$\text{GAMMA} = 0.69 \text{ V}^{1/2}$

- Extraction of  $\mu_0$  (U0) and  $\theta$  (THETA)

Strong inversion, linear region     $I_D \cong \frac{\mu n C_{ox}'}{2} \frac{W}{L} [(V_P - V_S)^2 - (V_P - V_D)^2]$

$$I_D = \mu n C_{ox}' \frac{W}{L} \left( V_P - \frac{V_D + V_S}{2} \right) (V_D - V_S) ; \frac{1}{\mu C_{ox}' \frac{W}{L}} \cong \frac{(V_G - V_{T0})(V_{DS})}{I_D} \text{ for small } V_{DS}$$

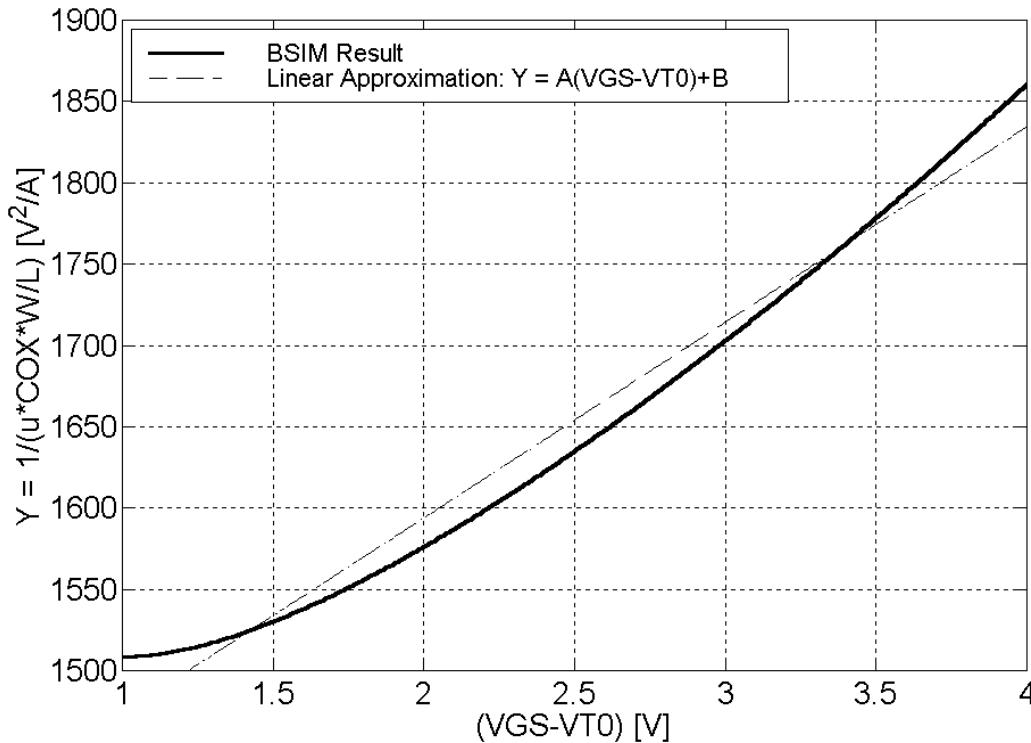


The plot

$$\frac{V_{DS}(V_G - V_{T0})}{I_D} \text{ versus } (V_G - V_{T0})$$

allows determining     $\mu C_{ox}' \frac{W}{L}$

- Extraction of  $\mu_0$  (U0) and  $\theta$  (THETA)



$$\mu = \frac{\mu_0}{1 + \theta(V_G - V_{T0})}$$

y-axis intersection  $\implies \mu_0 = \frac{1}{C_{OX} \cdot (W/L) \cdot B} = 514 \text{ cm}^2/\text{V}\cdot\text{s}$

slope A  $\implies \theta = \mu_0 \cdot C_{OX} \cdot \left(\frac{W}{L}\right) \cdot A = 0.20 \text{ V}^{-1}$

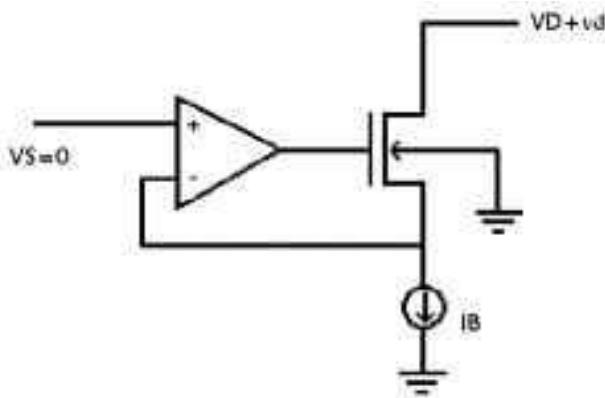
# **Short-channel effects:**

- DIBL**
- CLM**
- Weak avalanche**

Short-channel parameters are determined from either output conductance or voltage gain

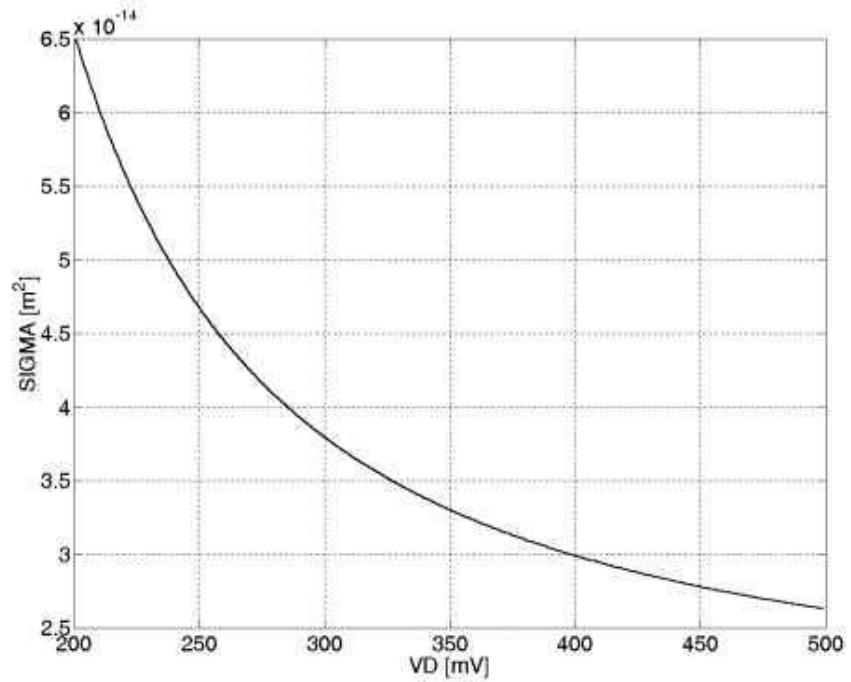
**Typically, for short channel devices, DIBL is dominant in weak inversion while CLM prevails in strong inversion**

## • Extraction of SIGMA (weak inversion)



$$\text{SIGMA} = \sigma \cdot (L_{\text{eff}})^2$$

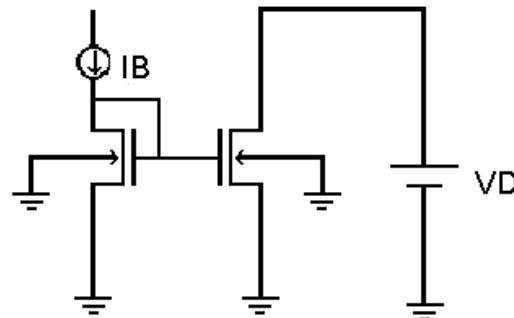
$$\sigma = -\frac{1}{\text{Gain}} = -\frac{g_m d}{g_m g}$$



$$V_T = V_{T0} - \sigma \cdot (V_D + V_S)/2$$

$\text{SIGMA} = 3.2 \times 10^{-15} \text{m}^2$

- Extraction of PCLM (strong inversion)



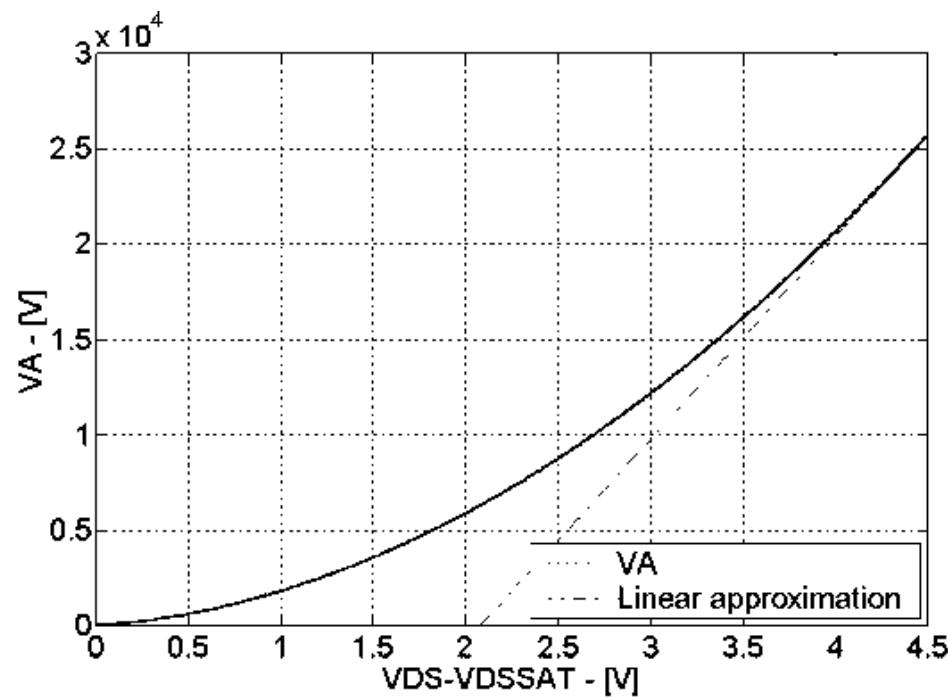
$$\Delta L = P_{CLM} \cdot L_C \cdot \ln \left[ 1 + \frac{(V_{DS} - V_{DSAT})}{L_C \cdot U_{CRIT}} \right]$$

$$U_{CRIT} = \frac{V_{MAX}}{U_0}$$

$$P_{CLM} = \frac{L_{eff}}{\frac{dV_A}{dV_{DS}} \cdot L_C} \cdot \left( \varepsilon \cdot \sqrt{1 + \frac{I_D}{I_S}} + 1 \right)$$

$$L_C = \sqrt{\varepsilon_{Si} \cdot \frac{Xj}{Cox}} \quad \varepsilon \approx \frac{\phi_t}{L_{eff} \cdot U_{CRIT}}$$

$P_{CLM} = 1.23$

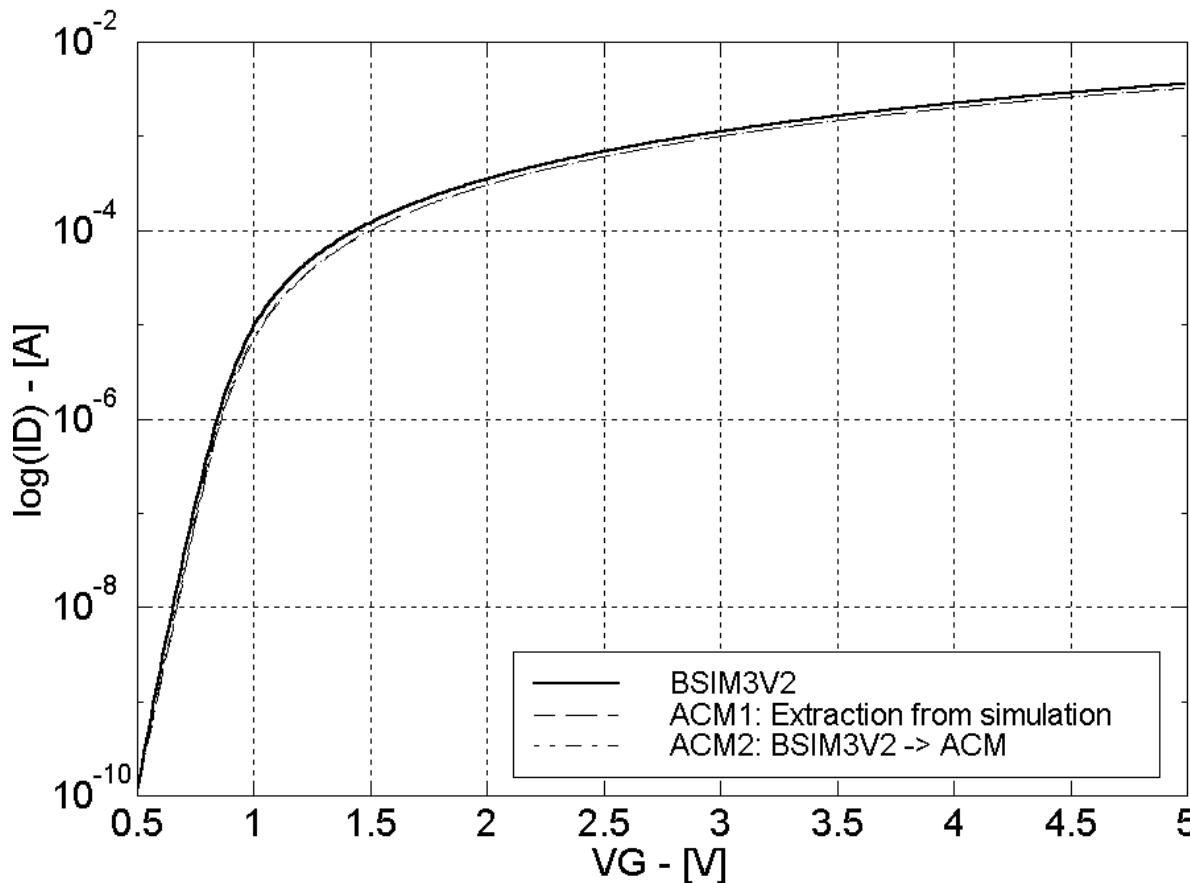


# Results

Parameter	BSIM3 → ACM	From Simulation	Unit
VT0	0.836	0.845	V
GAMMA	0.71	0.69	V <sup>1/2</sup>
PHI	0.81	0.7	V
TOX	$15.8 \cdot 10^{-9}$	$15.8 \cdot 10^{-9}$	m
LD	$209 \cdot 10^{-9}$	$209 \cdot 10^{-9}$	m
XJ	$300 \cdot 10^{-9}$	$300 \cdot 10^{-9}$	m
U0	487	514	cm <sup>2</sup> /V·s
VMAX	$9.08 \cdot 10^4$	$9.08 \cdot 10^4$	m/s
THETA	0.12	0.20	V <sup>-1</sup>
SIGMA	$4.55 \cdot 10^{-16}$	$3.2 \cdot 10^{-15}$	m <sup>2</sup>
PCLM	1.01	1.23	—

# Results

Simulation of an n-MOS transistor using  
Smash™ from Dolphin



Parameters:  
AMS 0.8 $\mu$ m  
BSIM 3V3

# Conclusions

- Advantages
  - ✓ Simple & Fast
  - ✓ Provides good results with low-cost equipment
  - ✓ Simple equations that emphasize the physical meaning of parameters
- Disadvantages
  - ✓ The extraction from simulation is dependent of the available models.

# Links

- *Integrated Circuits Laboratory*

 <http://www.eel.ufsc.br/lci/>

- *SMASH Circuit Simulator, Dolphin Integration, Meylan, France.*

 <http://www.dolphin.fr>

- *Austria Mikro Systeme International AG*

 <http://www.ams.co.at>

- *BSIM3 Homepage:*

 <http://www-device.ECCS.Berkley.EDU/~bsim3>